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December 1983

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E - Traffic engineering report for
the Ringwood Borough planning board
covering develop. of 9 sites and their effect on
the roadway system.

(includes maps + exhibits)

Prepared by Traffic + Transportation engineer.

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TRAFFIC ENGINEERING REPORT

FOR THE

RINGWOOD BOROUGH PLANNING BOARD

COVERING THE DEVELOPMENT OF NINE SITES

AND THEIR

EFFECT ON THE ROADWAY SYSTEM

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PREPARED BY

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80 ORTON ROAD

WEST CALDWELL, N.J. 07006

DECEMBER 1983

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RESUME OF JOHN E. **CHRIST, P.E.**

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INTRODUCTION

This report has been prepared to determine the effects of two scenarios of site development on the roadway system in Ringwood Borough. The first scenario is the development of nine sites as currently zoned. The second scenario is the development of the same nine sites in a higher density manner, or with different types of development. The nine sites are described in the S.LZK QE.S.QRLEZLQRS. section of this report beginning on page 4- 1.

The major roadways in Ringwood Borough have been included in the study. These include:

Skyline Drive
Greenwood Lake Turnpike
Sloatsburg Road
Margaret King Avenue
West Brook Road
Stone town Road

C Other roadways are included where they intersect with the above named roadways.

Twenty-five intersections are included in the study. Obviously, there are more than 25 intersections along these roadways. The more important intersections and the study site created intersections are the only ones included in order to keep the study to a manageable size.

The possible construction of Interstate Highway 1-287 in the area was noted. Potential interchanges in the area will be at the foot of Skyline Drive in Oakland and to the south in Wanaque off Ringwood Avenue. The location of the interchange in Oakland is understood to be definite and to include the improvement of the West Oakland Avenue - Skyline Drive intersection. It is understood that an interchange in Wanaque is not definite and that if one is constructed it will be off of Ringwood Avenue near Union Avenue.

Traffic counts were conducted as part of this study. Observations of traffic flows were made. Measurements of existing roadways were made*

A computerized traffic Tableau was used to manage the traffic generation and distribution portions of the study. Computerized methods for intersection capacity were also used.

The site descriptions and site development was obtained from the Planning Board, and their planning consultant. The traffic generation factors are from ZRLE GEN.KBAZLQE, 1982, by the Institute of Transportation Engineers.

The following directions of travel were assumed on the roadways in this study:

Skyline Drive North-south except at Erskine Road and at Greenwood Lake Turnpike.

Greenwood Lake Turnpike North-south except at Sloatsburg Road.

Sloatsburg Road North-south.

Margaret King Avenue East-west

West Brook Road East-west

Greenwood Lake Turnpike North-south except at Greenwood Lake Turnpike

CONCLUSIONS

C It can be concluded that

1, With the "As Zoned" scenario

a. Skyline Drive -will need extensive widening to five lanes in width from Greenwood Lake Turnpike to the south of Site I.

b, Greenwood Lake Turnpike will need to be widened to four lanes in width for its entire length within Ringwood, except possibly between Sloatsburg Road and Stonetown Road, with wider sections at the major intersections.

c. Margaret King Avenue will need to be widened to five lanes from Greenwood Lake Turnpike to Peters Mine Road and then four lanes to Sloatsburg Road,

d, Sloatsburg Road will need to be widened to four lanes for its entire length with wider sections at some inter sections.

2, With the "Full Development" scenario

a, All of the above improvements for the "As Zoned" scenario plus the following:

b, Skyline Drive should be widened to five lanes from Knollwood Drive easterly to Countryside (Site 1) near the water tower. The center lane should be 16 to 20 feet wide with painted channelization, and reserved for left turns into and out of the side streets, in order that left turning traffic from side streets entering Skyline Drive has to contend with only one direction of through traffic at a time.

c. The same roadway treatment as described for Skyline Drive in Item 2.b. above would be needed for Margaret King Avenue from Greenwood Lake Turnpike to Peters Mine Road.

d. Some intersections would need additional improvements beyond those needed in the "As Zoned" scenario.

e. A careful analysis should be made to determine if the roadway improvements needed for either scenario can be constructed, considering the rights-of-way available, slope rights, damages to the abutting properties, and within reasonable costs.

METHOD

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This study originally started for one site off of Skyline Drive. As such, the emphasis was placed on the A.M. (morning) Peak Traffic flow liour. While data has been collected in both the A.M. and P.M. peak hours, not all inter sect ions were counted during the P.M. hours.

Traffic counts were conducted at the following locations. The counts were conducted using a hand held telly count board with 16 registers. All turning movements were counted.

- Skyline Drive at Conkl intown Road
- Skyline Drive at Fieldstone Drive
- Skyline Drive at Erskine Road
- Fieldstone Drive at the Fieldstone Shopping Center Driveway
- Greenwood Lake Turnpike at Skyline Drive
- Greenwood Lake Turnpike at Sky I ana's Road
- Greenwood Lake Turnpike at Sloatsburg Road
- Greenvjood Lake Turnpike at Stonetown Road
- Greenwood Lake Turnpike at Margaret King Avenue
- Greenwood Lake Turnpike at West Brook Road
- Ringwood Avenue at Skyline Lakes Drive
- Ringwood Avenue at Conkl intown Road
- West Brook Road at Stonetown Road
- Conkl intown R.oad at Canterbury Road
- Sloatsburg Road at Carletondcle Road
- Sloatsburg Road at Margaret King Avenue
- Partial counts at Skyline Drive and Edward Drive
- Partial counts at Skyline Drive and James Drive

In addition, machine traffic counts were conducted on Skyline Drive south of Conkl intown Road near the water tower.

The above traffic counts were adjusted to a compos ite form and are shown in the Traffic Distr ibut ion Tableaus for inter sect ions in the column labeled EXISTING GRKD CNT (Existing Ground Count) in the Appendix.

The count data was used to estimate the directional travel of the generated site traffic. The best indicator of travel desires would be the existing traffic flows as they leave the area. Care was used not to include the through traffic from the north on Greenwood Lake Turnpike which returned to the north on Sloatsburg Road with no trip end in Ringwood. Some site traffic was considered to remain within Ringwood.

A computerized three-stage traffic distribution tableau was used to manage and present the data. Nine developable sites, 11 cordon (boundary) points, and 25 intersections are included in the Tableau. With this Tableau, the size of the various developments and the percent traveling to any cordon point can be easily changed. The most lengthy part of making a change would be loading the program into the computer. After loading the program, a series of changes in site development, travel factors, and directional factors could be made in a matter of minutes. After changing the data, the program will recalculate all intersection volumes in about five minutes. Therefore, should you desire changes in the site development used in this analysis it can easily be made.

Standard trip generation rates from the Institute of Transportation (ITE) publication TRIE_GENE&i1lQN, 1975, as updated in 1979 and 1982, was used to determine the volumes of vehicle trips to and from the study sites. The reasonableness of the ITE trip generation rates for the area was verified by manual and machine traffic counts made on Fieldstone Drive. The single family homes off Fieldstone Drive have only one way in and out for everyday traffic. The ITE factors related well to the traffic counts.

The method for determining the Level of Service for an Unsignalized Intersection contained in GLRCLLLAR-Z12., a 276 page publication by the Transportation Research Board, National Academy of Science, January 1980, was used. This method has been placed into a computer program. Note that there is an impedance factor determined by the left turns from the major roadway that reduces the capacity of the left turns and through movements from the side street. This impedance factor is to account for the differences in the gap distribution of the major roadway traffic

flow caused by a vehicle waiting to turn left. In the case of all of the "JT" type intersections, a three lane configuration with a left turn stacking lane is assumed. Since left turning traffic from the major roadway will not block following through major roadway traffic, the effect of the impedance factor has been reduced by two thirds.

The critical intersections within the study area were analyzed by the Critical Movement Analysis (CMA) for Signalized Intersections as programmed for an Apple Computer by the University of Florida. This program is for signalized intersections and allows a series of different intersection geometric and operational features of an intersection to be analyzed for capacity in a moderate amount of time. The CMA method is referred to as a planning method. It approximates the Level of Service that could be obtained if the intersections were operated efficiently. It does not give details such as the signal timing.

Traffic at a traffic signal operates quite differently depending on whether or not left turn movements are protected from the opposing traffic flow. The original Florida parameters were tested at Route 46 and New Road in Parsippany with April 1983 P.M. peak hour traffic counts supplied by the New Jersey Department of Transportation. The left turns are protected at the Route 46 - New Road intersection. The traffic flow is at saturation in the P.M. peak hour. Using a peak hour factor of 1.0, the CMA program calculated a Level of Service E at 102% saturation. This concurs with the actual conditions observed at the intersection. Note that a peak hour factor of 1.0 reflects constant demand during the hour while lower factors reflect unevenness in the traffic flow.

The existing background traffic was expanded at 3% per year for ten years to 1993 to reflect growth at other sites in Ringwood not included in the study, and traffic growth caused by development of the surrounding areas. This expansion factor does not affect the volume of traffic generated by the sites included in the study.

Site I. - Block 752 Lot 1, known as Countryside Properties. This site has frontage on the east side of Skyline Drive near the water tower. The site is 66 acres in size with 81% of its area on slopes over 15%. Access is proposed by others for both an intersection with Skyline Drive (Intersection 1) and by a connection to the existing Cheshire Lane (Intersection 2). The site roadway to Skyline Drive is called Countryside. In the analysis of the "As Zoned" scenario, 20 single family homes are used. Development of 280 townhouses within this site was used in the analysis of the "Full Development" scenario.

Site 2. - Block 877 Lot 16, also known as Countryside Properties. Site 2 is on the east side of Skyline Drive immediately south of Fieldstone Drive. This site is 63 acres in area with 67% lying on slopes of over 15%. It is proposed to use the 28 acres nearest Skyline Drive for commercial development. A shopping center with 140,000 gross square feet was assumed in both scenarios. The remaining 34 acres is proposed by others for residential development, rental or condominiums, with a total of 400 to 500 units. Four hundred and fifty units were used in the analysis of the "Full Development" scenario. Thirty-four single family homes were used in the "As Zoned" scenario. Access was tested to Fieldstone Drive at Intersection 13 in order that one traffic control signal could protect traffic exiting onto Skyline Drive (intersection 4) from the new as well as the existing shopping centers in the "Full Development" scenario. In the "As Zoned" scenario access was assumed to be from a site roadway to Skyline Drive (Intersection 5) with no access to Fieldstone Drive. Dctc is given in the "Full Development" scenario for both access directly to Skyline Drive or to Fieldstone Drive.

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Site 3. - Block 80 OA Lot 3, off Alto Vista Drive. This site lies to the west of Skyline Drive. It was assumed that access would be by an extension of Fieldstone Drive to the west and to Alto Vista Drive. Alto Vista Drive was not included in the computer traffic tableau because of size limitation. The percentage of traffic to Fieldstone Drive is reduced to reflect the volume of Site 3 traffic using Also Vista Drive instead of Intersection 4 in the tableau. A shopping center with 150,000 square feet gross floor area was used in both scenarios.

Site 4. - Block 100 Lot 16. This site is off the west side of Stonetown Road south of Magee Road. It is 95 acres in size with 19% on slopes of 15% or more. A 20,000 square foot neighborhood shopping area and 95 townhouses on the site were used in the traffic analysis for the "Full Development" scenario. In the "As Zoned" scenario 83 single family homes were assumed. This site was assumed to have its own roadway to Stonetown Road.
(Intersection 11).

Site 5. - Block 201 Lot 31. This site is off the west side of Stonetown Road north of Magee Road. It is 314 acres in size with 41% lying on slopes of 15% or greater. Three hundred and fourteen townhouses were used in the traffic analysis for the "Full Development" scenario and 217 townhouses in the "As Zoned" scenario. Access was assumed to be via Magee Road to Stonetown Road (Intersection 12).

Site 6. - Block 601 Lot 12 & 13. This site is off the north side of Margaret King Avenue and is owned by Ringwood Borough. This site is 203 acres in size with 68% on 15% or greater slopes. An access roadway to Margaret King Avenue was assumed (Intersection 18). Thirty acres for industrial use and 53 two family residential units were assumed for the "Full Development" scenario. Six acres for industrial use and 53 two family residential units were assumed for the "As zoned" scenario.

Site 7. - Block 508 Lot 2. This site is off the south side of Margaret King Avenue (Intersection 19). This site is 122 acres in area with 21% being on slopes of 15% or greater. A mobile home tract is proposed by others on this site. For the "Full Development" scenario, 732 residential mobile home units (six per acre) were assumed. For the "As Zoned" scenario, industrial uses on 48 acres was assumed.

Site 3. - Block 800 Lot 2. This site has access to Skyline Drive via Knollwood Drive (Intersection 6). Lot 2 is owned by the Borough and contains 45 acres, with 59% on 15% or greater slopes. Municipal offices including a library, a Department of Public Works building, Police Headquarters, and a park-ride lot with 60 spaces were used in the analysis for both scenarios.

Site 9. - Sterling Forest. This site is on the north side of Margaret King Avenue just east of Greenwood Lake Turnpike. Site 9 contains 1300 acres of which 60% is on slopes of 15% or more. For the traffic analysis, the following development was used in the traffic analysis:

<u>U.S.K</u>	<u>"FULL DEVELOPMENT"</u>	<u>"AS ZONED"</u>
	<u>SCENARIO</u>	<u>SCENARIO</u>
Single Family Residence	193 units	453 units
Townhouse	226 units	
Apartment	300 units	
Commercial	100,000 sq. ft.	
Office Lab	250,000 sq. ft.	250,000 SQ. ft.

Two roadways to Margaret King Avenue were assumed. The one located Sterling Forest Com. (Intersection 16) is to the west of the roadway labeled Sterling Forest Res. (Intersection 17).

COMPUTER TRAFFIC TABLEAU

A traffic generation-network-distribution tableau was used to combine the facets of a traffic tableau for the study area. The Visicars (1) program for an Apple Computer was used for this purpose. The program develops a three part tableau which overlays into the Standard Visicalc (2) software program. A large capacity (192K) is needed for this program as configured for this study.

The program is limited to 9 sites with 5 uses on each site, 16 cordon points, and 30 average intersections. In this case, 25 intersections were used to prevent exceeding the capacity of the program.

The first part of the Visicars tableau is a description of the sites, the uses on each site, and the cordon points. When completed and loaded into Visicalc, the sizes of each use and generation factors are added. Therefore, the various combination of site uses, sizes, and generation factors, are easily changed.

Included in the first part of the tableau when loaded into the Visicalc is the percentage of traffic from each use on each site to/from each cordon point. This percentage is easily changed in the tableau.

The second part of the computer traffic tableau is built by describing each included intersection. Each intersection is named and also given a number followed by a decimal point. The numbers following the decimal point, from 01 through 12, refer to movements. The numbers always begin with a left turn movement, the straight through traffic and then right turns with the following sequencing of approaches: Northbound, southbound, eastbound, westbound. Once completed, no changes may be made to this part of the tableau except by editing. Editing the final tableau is difficult and time consuming.

(1) Visicars is the trade name for the computer traffic tableau developed by Garmen Associates.

(2) Visicalc is a trademark of Personal Software Inc.

Building the third part of the Visicars tableau involves routing traffic along paths through the intersections from each site to each cordon point, and then from each cordon point to each site. Multiple branching of paths is possible along with the assignment of a percentage. This decision on a percentage for a particular branch of paths is made while building the tableau. Once put in the paths tableau, a percentage may only be changed by editing the final Visicalc tableau. That editing is a lengthy process*

Once the three parts of the program are completed and loaded into Visicalc, and various combinations of site development, generation factors, percentages to/from cordon points are loaded in, the Visicalc program will calculate the volumes of traffic to and from each site as it passes through each intersection. To these site generated volumes the existing volumes, or the existing volumes expanded at an annually compounded percentage rate of your choice for the number of years desired, may be added.

The graphics included with the program allow the presentation of traffic volumes at each intersection in a diagrammatic fashion. These traffic volume diagrams are included as an Appendix of this report. The intersection numbers correspond to the intersection numbers used for the traffic tableau.

Once the tableau is completed it is used for whatever variations in time period, site development, generation factors, traffic distribution percents, and background traffic, by editing headings and inserting the desired date. The prepared tableau without site or traffic factors and data is called up into the computer from a master storage disk. The various desired data is keyed in, calculations performed, printed, and saved on a different storage disk. This process is repeated in whole or part to get the desired scenarios for the study. Print-outs of the various tableaux are included under separate cover.

> * The site development in the tableau is from data supplied to
me from the Planning Board and their Consulting Professional
Planner. The traffic generation factors are from ZRLE
GE.NEBAZLQ.bL, 198 2, by the Institute of Transportation Engineers.
The percentages of site traffic to each cordon point was
developed from the counts of existing traffic flows. The computer
program expands the existing background traffic to a future year
at a chosen percent per year rate as part of its calculctions.
In this case, 1993 was chosen at an annual growth rate of 3
percent.

When completed, the computer traffic tableau is using the
best available data to give the best estimate of future traffic
flows through the twenty-five intersections included in the
study.

UH2R&ECX1&LJCAPAGITY-MALZ&LS.

Two types of intersection capacity analyses were performed. The first was the unsignalized intersection method from Circular 212. The second was a signalized intersection method called CMA for Critical Movement Analysis based on Circular 212. The computer program for the CMA analysis was developed by the Transportation Research Institute of the University of Florida.

The unsignalized intersection analysis assumes randomness in the traffic flows arriving at the intersection. Today this assumption is valid as there are no traffic signals in the study area. In the future there will be traffic signals which will change the approach characteristics of the traffic on the major roadways. The traffic signal will form queues in the major roadway traffic flows. In most cases the Level of service will be increased by nearby signals.

There are two facets to the Level of service reported by the unsignalized intersection capacity method. The first is delay to the average vehicle making the movement reported on and the second is the demand for the movement related to the capacity for that movement. You may see a Level of service 4 (D) reported where less than 5% of the capacity is utilized. This tells you that there will be substantial average delay for each vehicle making that movement although there will not be standing lines of waiting traffic. As the percentage of capacity utilized goes up, congestion would develop and increase.

In the unsignalized intersection analysis, three traffic lanes are considered in the approaches to the intersection. The extra* lane, which for the most part does not exist today, is for left turn stacking lanes. The effect of the impedance factor has been reduced in the calculations to reflect the left turn stacking lane's beneficial effect on capacity.

« The Level of service is stated in the results of the unsignalized intersection analysis in terms of delay. As set up in the program the letter "F" has been substituted for a second letter "E" that uses a different type setting in Circular 212, The delay description is in the following chart:

LEZEL-.QE.-ZKR1LGZ

EXEZQZEQ-XRAZELG-QZLAZ _____

A	Little or no delay
B	Short traffic delays
C	Average traffic delays
D	Long traffic delays
E	Very long traffic delays
F	Failure - extreme congestion

The Critical Movement Analysis (CMA) based on Circular 212 as developed for the Apple Computer by the University of Florida was used for signalized intersections. With this program it is necessary to enter left turns from the stem of a "T" type intersection as straight through traffic for calculations, Left turns in the CMA program only relate to directly opposing through traffic in a different type of check and would not reflect the green signal time needed for the movement. Each input and calculation for an intersection variation takes about five minutes. Therefore, many variations of intersection parameters can be tested in a reasonable amount of time. This CMA method is referred to as a Planning Method, One caution to anyone using this method is to always save data before making calculations, never after, and to always call for a new problem before retrieving data. The year 1993 is used in the CMA capacity analysis.

The following descriptions of level of service has been copied from page 130 of the 1965 dLGUEAZ GAEAGLZY. MA&U.AL- This description of the interpretation of the various levels of service is appropriate for this study.

At level of service A there are no loaded cycles (ie., the load factor **is** 0.0) and few are even close to loaded. No approach phase **is** fully utilized by traffic and no vehicle waits **longer** than one red indication. Typically the approach **appears** quite open, turning movements are easily made, **and nearly** all drivers find freedom of operation, their **only** concern being the chance that the light will be **red, when** they approach.

Level of service B represents stable operation, with a load factor **of not over** 0.1; an occasional approach phase is fully utilized **and** a substantial number are approaching full use. **Many drivers** begin to feel somewhat restricted within platoons of vehicles. Under typical rural conditions this frequently will be suitable operation for rural design purposes.

In level of service C stable operation continues. Loading is still intermittent, but more frequent, with the load factor ranging from 0.1 to 0.3. Occasionally drivers may have to **wait** through more than one red signal indication, and back-ups may develop behind turning vehicles. Most drivers feel somewhat restricted, but not objectionably so. In the absence of local conditions dictating otherwise, this is the level typically associated with urban design practice.

Level of **service** D encompasses a zone of increasing restriction approaching instability in the limit when the load factor reaches 0.70. Delays to approaching vehicles may be substantial during short peaks within the peak period, but enough cycles with lower demand occur to permit periodic **clearance** of developing queues, thus preventing excessive back-ups.

t Capacity occurs at level of service E. It represents the most vehicles that any particular intersection approach can accommodate. Although theoretically a load factor of 1.0 would represent capacity, in practice full utilization of every cycle is seldom attained, no matter how great the demand, unless the street is highly friction-free. A load factor range of 0.7 to 1.0 is more realistic. In the absence of a local determination, use of 0.85 is recommended for isolated intersections. For interconnected signals a higher factor may be appropriate, as discussed in Chapter Ten. At capacity there may be long queues of vehicles waiting upstream of the intersection and delays may be great (up to several signal cycles).

Level of service F represents jammed conditions. Back-ups from locations downstream or on the cross street may restrict or prevent movement of vehicles out of the approach under consideration; hence, volumes carried are not predictable. No load factor can be established, because utilization of the approach is prevented by outside conditions.

The actual intersection capacity analyses are on the following pages.

CAPACITY ANALYSIS FOR SKYLINE DRIVE & COUNTRYSIDE
INTERSECTION 1

This intersection is south of Conkl intown Road near the water tower. It does not exist today. It will be at a poor location for a possible traffic signal because of grades and horizontal curvature of the roadway. Therefore, only an unsignalized intersection capacity analysis was performed.

During the AM. peak hour with the "As Zoned" scenario, the unsignalized intersection capacity analysis shows a Level of service A (1) for left turns into and right turns out of Countryside and a Level o'f service E for left turns out of Countryside using only 3 of the 25 vehicle capacity. This would indicate severe delay for these few vehicles making left turn exits from Site 1 at this intersection. With the "Full Development" scenario the level of service for the left turn exit from Site 1 onto Skyline drops to an F with the demand exceeding the capacity,

During the P.M. peak hour, the analysis shows a Level of service E for both right and left turns from Countryside and left turns into Countryside for the "As Zoned" scenario, The "Full Development" scenario also shows Level of service E for these movements but note that the available reserve capacity is lower, meaning that there will be greater interaction among vehicles waiting to make the same movement.

C

Unsignalized "T" Int Cap Calc
 Location Skyline Dr. ?< Countryside Intersection 1
 Count Data: Zone development of sites included in the study
 Date 1993
 Day Weekday

AM or PM Analysis?	AM			
Hourly Demand Volumes:		Table 2A		
A Through	473	180	5	
A Right	2	240	6	
B Left	1	330	6	
B Through	1891	360	5	
C Left	3	440	7	
C Right	3	480	6	
		660	6	
		880	7	
RIGHT TURN FROM C				
Conflicting Flows=	474			
Major road lanes (2 or 4)	2			
Major road spd (30 or 55)	30			
Control (stop=4, Yld=3)	4			
Critical Gap Table 2 T=	6			
Capacity, from fig 2=	560			
Shared Lane-go to L.T.				
-----		Table 3		Figure 3
No shared lane-Y=1,N=0	1	-800	6	0
Demand(C right)=	3	0	5	5
Available Reserve*	557	100	4	10
Delay ?< L.O.S. Table 3=	1	200	3	15
(A=1,B=2,C=3,D=4,E=5,F=6)		300	2	20
		400	1	25
		10000	0	30
LEFT"TURN"FROM"i				35
Conflicting Flows=	475			40
Major road lanes(2 or 4)	2	Table 2B		45
Major road spd(30 or 55)	30	60	5	50
Critical Gap Table 2 T=	5	110	5.5	55
Capacity, from fig 2=	730	120	5.5	60
Demand(B left)=	1	220	6	65
Capacity used (in %)=	.1369863			70
Impedance factor, fig 3=	1	Table 2C		75
Available reserve^	729	180	6.5	80
Delay ?< L.O.S. Table 3=	1	240	7.5	85
(A=1,B=2,C=3,D=4,E=5,F=6)		330	8	90
		360	7	95
		440	9	100
		480	8	0
LEFT TURN FROM-C		660	9	
Conflicting Flows=	2366	880	10	
Major road lanes(2 or 4)	2			
Major road spd(30 or 55)	30			
Control (stop=4, Yld=3)	4			
Critical Gap Table 2 T=	7.5			
Capacity, from fig 2=	25			
Adjustment for Impedance ²	25			
-No Shared Lane,Y=1,N=0	1			
Demand=	3			
Available Reserve ³	22			
Delay S< L.O.S. Table Z ⁴	5			
(A=1,B=2,C=3,D=4,E=5,F=6)				

G - S A

C

Unsignalized "T" Int Cap Calc
 Location..... Skyline Dr & Countryside Intersection 1
 Count Data: Full development of sites included in the study

Data..... 1993
 Day..... Weekday
 AM or PM Analysis? AM

Hourly Demand Volumes:
 A Through 506
 A Right 10
 B Left 4
 B Through 2217
 C Left 27
 C Right 27
 RIGHT TURN FROM C
 Conflicting Flows* 511
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop-4, Yld*3) 4
 Critical Sap Table 2 T= 6
 Capacity, from fig 2* 530
 Shared Lane-go to L.T.

No shared lane-Y*I,N*O 1
 Demand(C right)³ 27
 Available Reserve" 503
 Delay & L.O.S. Table 3* 1
 (A*I,B-2,C<3.D-4.E>5,F>6)

LEFT TURN FROM B
 Conflicting Flows* 516
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T* 5
 Capacity, from fig 2* 695
 Demand(B left)* 4
 Capacity used (in 5C)* .5755396
 Impedance factor, fig 3* 1
 Available reserve* 691
 Delay & L.O.S. Table 3* 1
 <A=1,B<2,C>3.D-4,E*5,F*6)

LEFT TURN FROM C
 Conflicting Flows* 2732
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop*4, Yld=3> 4
 Critical Gap Table 2 T* 7.5
 Capacity, from fig 2> 25
 Adjustment for Impedance* 25

-No Shared Lane,Y*i,N*O I
 Demand* 27
 Available Reserve* -2
 Delay ?< L.O.S. Table 3= 6
 <A=*1,B=2,C*3,D*4,E=5,,F=6)

Table 2A

190	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	a.5
240	7.5
330	8
360	7
440	9
480	8
660	9
880	10

6-5 B

Unsignalised "T" Int Cap Calc

Location Skyline Dr. Se Countryside Intersection 1
 Date 1993
 Day Weekday

Count Data: Zone development of sites included in the study

AM or PM Analysis? PM

Hourly Demand Volumes:

A Through	2364
A Right	6
B Left	3
B Through	839
C Left	2
C Right	2

Table 2A

ISO	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

RIGHT TURN FROM C

Conflicting Flows=	2367
Major road lanes (2 or 4)	2
Major road spd (30 or 55)	30
Control (stop=4, Yld=3)	4
Critical Gap Table 2 T=	6
Capacity, from fig 2=	40
Shared Lane-go to L.T.	

No shared-lane-Y=1,N=0	1
Demand(C right)=	2
Available Reserve ³	38
Delay & L.O.S. Table 3=	5
(A=1,B=2,C=3,D=4,E=5,F=6)	

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.27
SO	.27
85	.2
90	.14
95	.08
100	0

LEFT TURN FROM B

Conflicting Flows=	2370
Major road lanes(2 or 4)	2
Major road sod(30 or 55)	30
Critical Gap Table 2 T=	5
Capacity, from fig 2=	50
Demand(B left)=	3
Capacity used (in 7.)=	6
Impedance factor, fig 3=	.97
Available reserves	47
Delay ?< L.O.S. Table 3=	5
<A=1,B=2,C=3,D=4,E=5,F=6>	

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	8
360	7
440	9
480	8
660	9
880	10

LEFT TURN FROM C

Conflicting Flows=	3209
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Control <stop=4, Yld=3>	4
Critical Gap Table 2 T=	7.5
Capacity, from fig 2=	25
Adjustment for Impedances	24.75025
-No Shared Lane,Y=t.N=0	1
Demand ³	2
Available Reserve="	22.75035
Delay ?< L.O.S. Table Z=	5
(A=1,B=2.C=3,D=4.E=5.F=6)	

Unsignalized "T" Int Cap Calc

Location Skyline Dr. & Countryside Intersection 1
 Count Data: Full development of sites included in the study

Date 1993
 Day Weekday

AM or PM Analysis? PM

Hourly Demand Volumesz

A Through	2655
A Right	51
B Left	21
B Through	985
C Left	12
C Right	14
RIGHT TURN FROM C Conflicting Flows**	2680.5
Major road lanes (2 or 4)	2
Major road spd (30 or 55)	30
Control (stop=4, Yld=3)	4
Critical Gap Table 2 T= Capacity, from fig 2- Shared Lane-go to L.T.	40

Table 2A

130	5
240	6
330	6
360	5
440	7
480	6
660	6
380	7

No shared lane-Y=1,N=0	1
Demand(C right)»	14
Available Reserve*	26
Delay & L.O.S. Table 3»	5
(A=1,B=2,C=3,D=4,E=5,F=6)	

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
10	.97
15	.39
20	.85
25	.31
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
90	.27
95	.2
100	.14
	.08
	0

LEFT TURN FROM B

Conflicting Flows*	2706
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Critical Gap Table 2 T= Capacity, -from fig 2= Demand(B left)= Capacity used (in '/.)= Impedance factor, fig 3= Available reserve** Delay & L.O.S. Table Z= <A>1,B<2.C>3,D<4,E>5,F*6>	50 21 42 .69 25

Table 2B

60	5
NO	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	9
360	7
440	9
480	8
660	10
980	10

LEFT TURN FROM C

Conflicting Flows™	3686.5
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Control (stop=4. Yld=3)	4
Critical Gap Table 2 T» Capacity, from fig 2= Adjustment for Impedance ⁸	7.5 25 22.41925

-No Shared Lane.Y=1.N>0	1
Demand=	12
Available Reserve-	10.41925
Delay & L.O.S. Table 3= (A=1,B>2.C>3,D>4,E=5.F>6)	5

^CAPACITY ANALYSIS FOR SKYLINE DRIVE & CONKLINTOWN ROAD -
^INTERSECTION 2

The unsignalized intersection capacity analysis for the current traffic volumes shows a Level of service E for right turns and D for left turns from Conkl intown Road in the A.M. peak hour. The capacity for the right turn from Conkl intown Road nearly equals the capacity for that movement. Adding traffic from the sites in this study would have the effect of having the demand for the movements from Conkl intown Road both exceed the available capacity, necessitating further roadway widening and traffic signals.

The CMA analysis shows that with future development of the study sites the P.M. peak hour will be the more critical. In the 1993 "Full Development" scenario, a Level of service E with a saturation rate of 90% is indicated by the CMA analysis with Skyline Drive widened to 5 lanes and Conkl intown Road to 4 lanes. Note that the 194 vehicles turning left from Conkl intown Road are placed in the computer analysis as through traffic. With the same intersection geometry, a Level of service D at a saturation rate of 80% would result in 1993 from development of the study sites "As Zoned". In the 1993 A.M. peak hour, this geometry would give a satisfactory Level of service C at a saturation rate of 69% with the "Full Development" scenario.

The next test was to add another through lane for northbound traffic on Skyline Drive. Skyline Drive would then have 3 lanes for through northbound traffic, one lane for northbound left turns and 2 lanes for southbound traffic. As before, Conkl intown Road would have 2 lanes for left turns and one lane for right turns entering the intersection and one lane exiting the intersection. With this geometry the CMA indicates a satisfactory Level of service C at a saturation rate of 66% for the "Full Development" scenario and a Level of service B at a saturation rate of 59% for the "As Zoned" scenario.

From the above it can be seen that the "Full Development" scenario would be one Level of service below the "As Zoned" scenario. It should be noted that the added lane would have to be of a significant length to add to the capacity as indicated by the CMA analysis. A full width lane 800 feet or more long before and after the intersection would be desirable.

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SKYLINE OR ft CONKLINTOUN RO

DATE 1993 PM PEAK FULL DEVELOPMENT

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.....>>>.....
LEVEL OF SERVICE  E
SATURATION        30
CRITICAL N/S VOL  1434
CRITICAL E/W VOL  118
CRITICAL SUM      1552
*****
    
```

		LANE GEOMETRY							
LANE	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND		
	MOV WIDTH		MOV WIDTH		MOV WIDTH		MOV WIDTH		
1	T..	13.0	RT..	13.0	R..	13.0	
2	T..	14.0	T..	12.0	T..	12.0	
3	L..	12.0	T..	12.0	
4	
5	
6	

		NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT		327	0	0	0
THRU		2342	896	194	0
RIGHT		0	237	107	0

	TRUCKS <math>\%>	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.3
EASTBOUND	5	0	.9
WESTBOUND	0	0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 39 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	1434	672	118	0
LEFT	351	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	327	0	0	0
ADJUSTED VOL	351	0	0	0
CAPACITY	0	0	0	0
MOVEMENT	N/A	N/O	US OK	OK

6-6A

JOHN E- CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & CONKLINTOWN RD

DATE 1993 PM PEAK AS ZONED

*****#*****#*****
 LEVEL OF SERVICE D
 SATURATION 80
 CRITICAL N/S VOL 1262
 CRITICAL E/W VOL 109
 CRITICAL SUM 1371
 *****#*****#*****

LANE	LANE SEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T.. 13.0	RT. 13.0	R.. 13.0
2	T.. 12.3	T.. 13.0	T.. 12.0
3	L.. 12.0	T.. 12.0
4
5
6

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	305	0	0	0
THRU	2061	751	178	0
RIGHT	0	229	87	0

	TRUCKS <*	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	0	0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	1262	579	109	0
LEFT	324	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	305	0	0	0
ADJUSTED VOL	324	0	0	0
CAPACITY	0	0	109	0
MOVEMENT	N/A	N/A	OK	OK

6-6 B

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & CONKLINTOWN RD

DATE 1993 AM PEAK FULL DEVELOPMENT

*****#*****

LEVEL OF SERVICE C
 SATURATION 69
 CRITICAL N/S VOL 1134
 CRITICAL E/W VOL 50
 CRITICAL SUM 1184

*****HHHHUHHHHHHHHMUHI*****

LANE	LANE GEOMETRY							
	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	T..	13.0	RT.	13.0	R..	13.0
2	T..	12.0	T..	12.0	T..	12.0
3	L..	12.0	T..	12.0
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	32	0	0	0
THRU	480	1769	33	0
RIGHT	0	70	452	0

	TRUCKS	LOCAL BUSES	(#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0		.9
SOUTHBOUND	5	0		.9
EASTBOUND	0	0		.9
WESTBOUND	0	0		1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W il. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY i I. 0 - 99 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	293	1120	50	3
LEFT	14	0	12	13

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	52	0	0	0
ADJUSTED VOL	14	0	0	0
CAPACITY	0	0	50	13
MOVEMENT	N/A	N/A	OK	OK

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & CONKLINTOWN RD

DATE 1993 PM PEAK FULL DEVELOPMENT

LEVEL OF SERVICE C
SATURATION 66
CRITICAL N/S VOL 1023
CRITICAL E/W VOL 118
CRITICAL SUM 1141

LANE GEOMETRY								
LANE	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	T.	13.0	RT.	13.0	R.	13.0
2	T.	12.0	T.	12.0	T.	12.0
3	T.	12.0			T.	12.0
4	L.	12.0				
5						
©						

TRAFFIC VOLUMES				
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	327	0	0	0
THRU	2342	896	194	0
RIGHT	0	237	107	0

	TRUCKS <*>	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	0	0	1

PHASING N/S : 4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W : 1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU*-RIGHT	1001	672	118	0
LEFT	351	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	327	0	0	0
ADJUSTED VOL	351	0	0	2
CAPACITY	0	0	118	0
MOVEMENT	N/A	N/A	OK	OK

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & CONKLINTOWN RO

DATE 1993 PM PEAK AS ZONED

.....>>>.....>>>.....>>>.....>>>.....>>>.....
 LEVEL OF SERVICE B
 SATURATION 39
 CRITICAL N/S VOL 903
 CRITICAL E/W VOL 109
 CRITICAL SUM 1012
>>>.....>>>.....>>>.....>>>.....>>>.....

LANE	LANE GEOMETRY							
	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	T..	13.0	RT.	13.0	R..	13.0
2	T..	12.0	T..	12.0	T..	12.0
3	T..	12.0	T..	12.0
4	L..	12.0
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	305	0	0	0
THRU	2061	731	178	0
RIGHT	0	229	87	0

	TRUCKS (%)	LOCAL BUSES	<#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5		0	.3
SOUTHBOUND	5		0	.9
EASTBOUND	5		0	.3
WESTBOUND	0		0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	881	579	109	0
LEFT	324	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	305	0	0	0
ADJUSTED VOL	324	0	13	13
CAPACITY	0	0	109	0
MOVEMENT	N/A	N/A	OK	OK

6-6 E

Unsignalised "T" Int Cap Calc

Location Skyline Dr & Conklintown Rd Intersection 2

Count Data: Existing Ground Count

Date 1983

Day Weekday

AM or PM Analysis? AM

Hourly Demand Volumes:

A Through	900
A Right	25
B Left	25
B Through	100
C Left	35
C Right	300

Table 2A

ISO	5
240	6
330	6
360	5
440	7
480	6
660	6
SSO	7

RIGHT TURN FROM C

Conflicting Flows=	912.5
Major road lanes <2 or 4)	2
Major road spd (30 or 55)	30
Control (stop<4, Yld=3)	4
Critical Gap Table 2 T=	6
Capacity, from fig 2=	305
Shared Lane-go to L.T.	

Table 3

-300	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure

0	1
5	.93
10	.93
15	.89
20	.35
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

No shared lane-Y=77N=0

Demand(C right)=	300
Available Reserve ³	5
Delay at L.O.S. Table 3=	5
<A=1,B=2,C=3,D=4,E=5,F=6)	

LEFT-TURN-FROM-i

Conflicting Flows=	925
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Critical Gap Table 2 T=	5
Capacity, from fig 2=	440
Demand (B left)=	25
Capacity used (in %)=	5.6S1818
Impedance factor, fig 3=	.97
Available reserve=	415
Delay & L.O.S. Table 3=	1
(A=1,B=2,C=3,D=4,E=5,F=6)	

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	3
360	7
440	9
660	9
880	10

LEFT TURN FROM C

Conflicting Flows=	1037.5
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Control <stop=4, Yld=3)	4
Critical Gap Table 2 T=	7.5
Capacity, from fig 2=	150
Adjustment for Impedance=	148.5015

-No Shared Lane,Y=1,N=0

Demand ⁵⁵	35
Available Reserve=	113.5015
Delay ?< L.O.S. Table 3=	4
(A=1,B=2,C=3,D=4,E=5,F=6)	

6-6F

Unsignalized 'T' Int Cap Calc
 Location Skyline Dr * Conklintown Rd Intersection 2

Count Data: Existing Ground Count
 Date 1983
 Day Weekday
 AM~or~PM*Anafysis? PM

Hourly Demand Volumes:
 A Through 200
 A Right 70
 B Left 200
 B Through 1250
 C Left 40
 C Right 50
 RIGHT TURN FROM C
 Conflicting Flows* 235
 Major road lanes (2 or 4) 2
 Major road sod (30 or 55) 30
 Control (»top«4, Yld»3) 4
 Critical Gap Table 2 T» 6
 Capacity. from fig 2^s 760
 Shared Lane-go to L.T.

 ~No shared Lane-Y*17N=0 1
 Demand(C right)³ 50
 Available Reserve* 710
 Delay & L.O.S. Table 3« 1
 (A»1.B»2,C*3,D»4,E»5.F«6>

 LEFT-TURN"FROM-B
 Conflicting Flows" 270
 Major road lanes<2 or 4) 2
 Major road sod(30 or 55) 30
 Critical Gap Table 2 T= 5
 Capacity, from fig 2= 920
 Demand(B left)* 200
 Capacity used (in *'.)* 21.73913
 Imoedance factor, fig 3» .85
 Available reserve* 720
 Delay & L.O.S. Table 3» 1
 (A»1.B»2,C»3,D»4,E=5.F*6)

 LEFT TURN FROM C
 Conflicting Flows* 1685
 Major road lanes(2 or 4) 2
 Major road spd<30 or 55) 30
 Control (stop»4. Yld=3) 4
 Critical Gap Table 2 T= 7.5
 Capacity, from fig 2= 50
 Adjustment for Impedance* 47.5025

 -No Shared Lane.Y=1,N=0 1
 Demand³ 40
 Available Reserve^ 7.5025
 Delay ?< L.O.S. Table 3= 5
 (A=1.B=2.C=3.D=4.E=5.F=6)

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

Table 3

-800	6	0	1
0	5	5	.91 ^F
100	4	10	.93
200	4	15	.89
300	2	20	.35
400	1	25	.81
10000	0	30	.77

Table 2B

60	5	40	.69
110	5.5	45	.64
120	5.5	50	.6
220	6	55	.55
		60	.5
		65	.45
		70	.39
180	6.5	75	.33
240	7.5	80	.27
330	3	85	.2
360	7	90	.14
440	9	95	.08
480	8	100	0
660	0		
880	10		

6-6 G

Unsignalised "T" Int Cap Calc
 Location Skyline Dr & Conklintown Rd Intersection 2
 Count Data: Zone development of sites included in the study

Date 1983
 Day Weekday

AM or PM Analysis? AM

Hourly Demand Volumes:
 A Through 1141
 A Right 42
 B Left 36
 B Through 397
 C Left 68
 C Right 338
 RIGHT TURN FROM C
 Conflicting Flows= 1162
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop'4, Yld=3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2= 200
 Shared Lane-go to L.T.

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

 No"shared~lane-Y=17N=0 1
 Demand(C right)= 338
 Available Reserve* -138
 Delay it L.O.S. Table 3= 6
 (A=1,B=2,C=3,D=»4,E=5,F=6)

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

LEFT~TURN~FROM~B
 Conflicting Flows- 1183
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T= 5
 Capacity, from fig 2= 320
 Demand(B left)= 36
 Capacity used (in !).= 11.25
 Impedance factor, fig 3= .93
 Available reserve* 284
 Delay ?< L.O.S. Table 3= 3
 <A=1,B=2,C=3,D=4,E=5,F=6)

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	8
360	7
440	?
480	8
660	9
380	10

LEFT~TURN~FROM~C
 Conflicting Flows* 1595
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop=4. Yld=3) 4
 Critical Gap Table 2 T= 7.5
 Capacity, from fig 2= 50
 Adjustment for Impedance*¹ 48.8345

-No Shared Lane, Y=»1, N=0 1
 Demand* 68
 Available Reserve- -19.1655
 Delay & L.Q.S. Table 3= 6
 (A=1,B=2.C=3,D=4.E=5,F=6)

6-6H

Unsignalized "T" Int Cap Calc

Location _____ Skyline Dr S< Conklintown Rd Intersection 2
 Count "Data" Zone development of sites included in the study

Date* _____ 1983
 Day _____ Weekday

AM or PM Analysis?	Hourly Demand Volumes
AM	
PM	
	A Through 682
	A Right 205
	B Left 236
	B Through 1631
	C Left 164
	C Right 70

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

RIGHT TURN FROM C

Conflicting Flows*	784.5
Major road lanes (2 or 4)	2
Major road spd (30 or 55)	30
Control (stop-4, Yld*3)	4
Critical Gap Table 2 T=	6
Capacity, from fig 2 ^s	380
Shared Lane-go to L.T.	

Table 2
Figure 3

-800	6	0	1
0	5	5	.97
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77
		35	.72
		40	.69

No shared Lane-Y*77N*O

Demand(C right) ³	70
Available Reserve*	310
Delay & L.O.S. Table 3*	2
(A-1, B-2, C*3, D*4, E*5, F*6)	

Table 2B
Table 2C

60	5	45	.64
110	5.5	50	.6
120	5.5	55	.55
220	6	60	.5
		65	.45
		70	.39
180	6.5	75	.33
240	7.5	80	.27
330	8	85	.2
360	9	90	.14
440	9	95	.08
480	10	100	0
660	?		
880	10		

LEFT TURN FROM B

Conflicting Flows*	887
Major road lanes(2 or 4)	2
Major road spd(30 or 35)	30
Critical Gap Table 2 T»	5
Capacity, from fig 2*	460
Demand(8 left)*	236
Capacity used (in %)=	51.,30435
Impedance factor, fig 3*	.6
Available reserve*	224
Delay Si L.O.S. Table 3*	3
(A*i, B-2, C-3, D»4, E*5, F«6)	

LEFT TURN FROM C

Conflicting Flows*	2651.5
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Control (stop*4, Yld»3)	4
Critical Gap Table 2 T=	7.5
Capacity, from fig 2*	25
Adjustment for Impedance*	21.67

-No Shared Lane, Y*1, N*0

Demand*	164
Available Reserve*	-142.33
Delay & L.O.S. Table 3*	6
(A*1, B«2, C*3, D*4, E«5, F»6)	

k

Unsignalised "T" Int Cap Calc

Location Skyline Dr & Conklintown Rd Intersection 2
Count Data: Full development of sites included in the study

Date 1983

Day Weekday

AM or PM-Analysis? AM

Hourly Demand Volumes:	
A Through	1459
A Right	61
B Left	44
B Through	446
C Left	71
C Right	349

Table 2A	
ISO	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

RIGHT TURN FROM C	
Conflicting Flows-	1489.5
Major road lanes (2 or 4)	4
Major road spd (30 or 55)	30
Control <stop=4, Yld=3>	4
Critical Gap Table 2 T=	6
Capacity, -from fig 2=	130
Shared Lane-go to L.T.	

No shared lane-Y=1,N=0	1
Demand(C right)=	349
Available Reserve-	-219
Delay & L.O.S. Table 3-	6
(A=1,B=2,C=3,D=4,E=5,F=6)	

Table 3		Figure 3	
-800	6	0	1
0	5	5	.97
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77
		35	.72

LIFT~TURN~FROM~i	
Conflicting Flows=	1520
Major road lanes(2 or 4)	4
Major road spd(30 or 55)	30
Critical Gap Table 2 T=	5.5
Capacity, from fig 2=	150
Demand(B left)=	44
Capacity used (in'/.+)	29.33333
Impedance factor, fig 3=	.81
Available reserve*	106
Delay ?< L.O.S. Table 3=	4
<A=1,B=2,C=3,D=4,E=5,F=6)	

Table 2B		Table 2C	
60	5	180	6.5
110	5.5	240	7.5
120	5.5	330	8
220	6	360	7
		440	9
		480	8
		660	9
		880	10
			70
			75
			80
			85
			90
			95
			100
			0

LEFT~TURN~FROM C	
Conflicting Flows=	1979.5
Major road lanes(2 or 4)	4
Major road spd(30 or 55)	30
Control (stop=4, Yld<3>	4
Critical Gap Table 2 T=	8
Capacity, from fig 2=	20
Adjustment for Impedance-	18.7346

-No Shared Lane,Y=1,N=0	1
Demand ² *	71
Available Reserve=	-52.2654
Delay !< L.O.S. Table 3=>	6
(A=i,B=2.C=3,D=4,E=5,F<6)	

6-6 J

Unsignalized "T" Int Cap Calc

Location Skyline Dr & Conklintown Rd Intersection 2
 Count Data Full development of sites included in the study

Data 1983
 Day Weekday
 AM or PM Analysis? PM

Hourly Demand Volumes:
 A Through 827
 A Right 213
 B Left 258
 B Through 1912
 C Left 180
 C Right 89
 RIGHT TURN FROM C
 Conflicting Flows* 933.5
 Major road lanes (2 or 4) 4
 Major road spd (30 or 55) 30
 Control (stop-4. Yld*3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2» 290
 Shared Lane-go to L.T.

No shared lane-Y-i.N=0 1
 Demand<Cright)=* 89
 Available Reserve* 201
 Delay & L.O.S. Table 3* 3
 <A>1,B*2.C-3,D»4,E-5,F-6)

LEFT TURN FROM B
 Conflicting Flow** 1040
 Major road lanes(2 or 4) 4
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T* 5.5
 Capacity* from fig 2* 310
 Demand(B left)* 258
 Capacity used (in X)* 83.22581
 Impedance factor, fig 3= .27
 Available reserve* 52
 Delay & L.O.S. Table 3* 5
 <A>1,B-2,C*3,D*4,E-5.F«6)

LEFT TURN FROM C
 Conflicting Flows* 3103.5
 Major road lanes(2 or 4) 4
 Major road spd(30 or 55) 30
 Control (stop»4, Yld*3) 4
 Critical Gap Table 2 T» 8
 Capacity, from fig 2* 20
 Adjustment for Impedance* 15.1382

-No Shared Lane.Y»1,N»0 1
 Demand* 180
 Available Reserve- -164.862
 Delay & L.O.S. Table Z=* 6
 <A*1,B«2.C-3,D»4,E»5,F»6)

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

Table 3

-800	6
0	5
100	4
200	2
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.39
20	.85
25	.81
30	.77
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

Table 2B

60	5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
360	8
440	9
480	8
660	9
880	10

CAPACITY ANALYSIS FOR SKYLINE DRIVE & CHESHIRE LANE -
INTERSECTION 3

This currently existing intersection is a short distance north of Conklintown Road. It is proposed by others that Site 1 have part of their access by this intersection. Because of this intersection's location with respect to Conklintown Road, a traffic signal capacity analysis was not done.

During the A.M. peak hour, the unsignalized intersection analysis for the "As Zoned" scenario shows a Level of service A for vehicles making right turns out of and left turns into Cheshire Lane, and a Level of service E for vehicles making left * turns from Cheshire Lane. The left turns from Cheshire Lane onto Skyline Drive use 17 of the 25 vehicle available capacity indicating interaction between vehicles waiting to make that movement. With the "Full Development" scenario during the A.M. peak hour, the Level of service for the left turn from Cheshire Lane falls to an F with the demand (44) exceeding the capacity (20) by 24 vehicles, indicating extremely long delays.

During the P.M. peak hour, the unsignalized intersection capacity analysis shows a Level of service E for both left and right turns out of Cheshire Lane and for left turns into Cheshire Lane for the "As Zoned" scenario. In the "Full Development" scenario the Level of service for left turns from Cheshire Lane fails to an F with the capacity exceeded.

f

Unsignalized "T" Int Cap Calc
 Location Skyline Dr & Cheshire La. Intersection 3
 Count Data*Zone development of sites included in the study
 Data 1993
 Day Weekday

AM or PM Analysis?	AM
Hourly Demand Volumes:	
A Through	504
A Right	7
B Left	8
B Through	1484
C Left	17
C Right	15
RIGHT TURN FROM C	
Conflicting Flows-	507.5
Major road lanes (2 or 4)	30
Major road spd (30 or 55)	30
Control (stop-4, Yld»3)	4
Critical Sap Table 2 T«	6
Capacity, from fig 2-	530
Shared Lane-go to L. T.	

No shared lane-Y-1,N«0	1
Demand(C right)-	15
Available Reserve-	515
Delay & L.O.S. Table 3-	1
(A-1,B-2,C»Z,D-4,f-5,F-6)	

LEFT TURN FROM I	
Conflicting Flows*	511
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Critical Gap Table 2 T»	5
Capacity, from fig 2-	695
Demand(B left)"	8
Capacity used (in /f)*	1.151079
Impedance factor, fig 3*	1
Available reserve-	687
Delay it L.O.S. Table 3*	1
(A»1,B«2,C«3,D«4,E»5,F*6)	

LEFT TURN FROM C	
Conflicting Flows-	1999.5
Major road lanes<2 or 4)	-
Major road spd(30 or 55)	30
Control (stop»4, Yld»3)	4
Critical Gap Table 2 T»	7.5
Capacity, from fig 2*	25
Adjustment for Impedance-	25

-No Shared Lane,Y=1.N»0	i
Demand ⁹	17
Available Reserve-	8
Delay ?< L.O.S. Table 3=	5
(A=1, 8-2, C=Z,D-4.E-5,F-6)	

Table 2A

ISO	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

Table 3		Figure 3	
-800	6	0	1
0	5	5	.97
100	4	10	.93
200	Y.	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77
		35	.72
		40	.69
Table 2B		45	.64
60	5	50	.6
110	5.5	55	.55
120	5.5	60	.5
220	6	65	.45
		70	.39
Table 2C		75	.33
180	6.5	80	.27
240	7.5	85	.2
330	3	90	.14
360	7	95	.08
440	9	100	0
480	8		
660	9		
880	10		

Unsignalised "T" Int Cap Calc

Location Skyline Dr ?< Cheshire La. Intersection 3
 Count Data: Full development of sites included in the study

Date 1993
 Day Weekday

AM or PM AnaFysFs? AM
 Hourly Demand Volumes:

		Table 2A	
A Through	556	180	5
A Right	8	240	6
B Left	11	330	6
B Through	1795	360	5
C Left	44	440	7
C Right	33	480	6
		660	6
		880	7
RIGHT TURN FROM C			
Conflicting Flows=	560		
Major road lanes (2 or 4)	4		
Major road spd (30 or 55)	30		
Control <stop=>4, Yld=3)	4		
Critical Gap Table 2 T=	6		
Capacity, from fig 2=	500		
Shared Lane-go to L.T.			

		Table 3		Figure ->	
-No-shared-lane-Y=T7N=0	1	-800	6	0	1
Demand(C right)=	33	0	5	5	.97
Available Reserve*	467	100	4	10	.93
Delay & L.O.S. Table 3=	1	200	3	15	.89
(A=1,B=2,C=3,D=4,E=5,F=6)		300	2	20	.85
		400	1	25	.81
		10000	0	30	.77
				35	.72
				40	*69

		Table 2B		Table 2C	
LEFT~TURN~FROM i					
Conflicting Flows=	564	60	5	45	.64
Major road lanes(2 or 4)	4	110	5.5	50	.6
Major road spd(30 or 55)	30	120	5.5	60	.5
Critical Gap Table 2 T=	5.5	220	6	65	.45
Capacity, from fig 2=	575			70	.39
Demand(B left)=	11			75	.Z-Z
Capacity used (in '/.)=	1.913043	180	6.5	80	.27
Impedance factor, fig 3=	1	240	7.5	95	.2
Available reserve*	564	330	8	90	.14
Delay ?< L.O.S. Table 3=	1	360	7	95	.08
<A=1,B=2,C=3,D=4,E=5,F=6>		440	9	100	0

		Table 2C	
LEFT~TURN"FROM C		480	8
Conflicting Flows=	2366	660	?
Major road lanes(2 or 4)	4	880	10
Major road spd(30 or 55)	30		
Control (stop=4, Yld=3)	4		
Critical Gap Table 2 T=	8		
CaQacity, from fig 2=	20		
Adjustment for Impedance=	20		
-No Shared Lane,Y=1.N=0	1		
Demand=	44		
Available Reserve=	-24		
Delay !< L.O.S. Table Z=	6		
(A=1.B=2.C=3,D=4.E=5,F=6)			

Unsignalized "T" Int Cap Calc

Location Skyline Dr it Cheshire La. Intersection 3
 Count Data; Zone development of sites included in the study

Date 1993
 Day Weekday
 AM or PM Analysis? PM

Hourly Demand Volumes:		Table 2A	
A Through	2191	180	5
A Right	21	240	6
B Left	17	330	6
B Through	972	360	5
C Left	9	440	7
C Right	8	480	6
		660	6
		880	7
RIGHT TURN FROM C			
Conflicting Flows-	2201.5		
Major road lanes (2 or 4)	2		
Major road spd (30 or 55)	30		
Control (stop»4. Yld»3>	4		
Critical Gap Table 2 T-	6		
Capacity, from fig 2-	40		
Shared Lane-go to L.T.			

No shared lane-Y=1.N=0	1
Demand (C right)-	8
Available Reserves	32
Delay & L.O.S. Table 3=	5
(A-i,B-2,C-3.D-4,E-5.F-6)	

LiFT~TURN~FROM~i	
Conflicting Flows-	2212
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Critical Gap Table 2 T»	5
Capacity, from fig 2=	50
Demand(B left)-	17
Capacity used (in %)	34
Impedance factor, fig 3*	.77
Available reserve-	33
Delay % L.O.S. Table 3*	5
.A«1.B-2,C-3,D-4,E-5,F-6)	

LEFT~TURN~*FROM~'C	
Conflicting Flows-	3190.5
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Control (stop»4. Yld-3)	4
Critical Gap Table 2 T=	7.5
Capacity, from -fig 2-	25
Adjustment for Impedance-	23.08525
-No Shared Lane.Y-1.N-0	1
Demand-	9
Available Reserve-	14.08525
Delay ?< L.O.S. Table 3-	5
(A-1,B-2,C-3,D-4,E-5,F-6)	

Table 2		Figure 1	
-800	6	0	1
0	5	5	.37
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77
		35	.72
		40	.69
		45	.64
		50	.6
		55	.55
		60	.5
		65	.45
		70	.39
		75	.33
		80	.27
		85	.2
		90	.14
		95	.08
		100	0

6-7" C

Unsignalized "T" Int Cap Calc
 Location Skyline Dr & Cheshire La. Intersection 3
 Count Data: Full development of sites included in the study

Date 1993
 Day Weekday

AM-or-FM-AnaTysi"s? PM

Hourly Demand Volumes:
 A Through 2485
 A Right 24
 B Left 42
 B Through 1112
 C Left 20
 C Right 17
 RIGHT TURN FROM C
 Conflicting Flows= 2497
 Major road lanes (2 or 4) 4
 Major road spd (30 or 55) 30
 Control <stop=4, Yld=3) 4
 Critical Gap Table 2 T=> 6
 Capacity, from fig 2= 40
 Shared Lane-go to L.T.

Table 2A
 180 5
 240 6
 330 6
 360 5
 440 7
 480 6
 660 6
 880 7

No "shared-Tane-Y=17N=0 1
 Demand(C right)= 17
 Available Reserve* 23
 Delay & L.O.S. Table 3= 5
 (A=1,B=2,C=3,D=4,E=5,F=6)

Table 3
 -800 6
 0 5
 100 4
 200 3
 300 2
 400 1
 10000 0

Figure 3
 0 1
 5 .97
 10 .93
 15 .89
 20 .85
 25 .81
 30 .77
 35 .72
 40 .69
 45 .64
 50 .6
 55 .55
 60 .5
 65 .45
 70 .39
 75 .33
 80 .27
 85 .2
 90 .14
 95 .08
 100 0

LEFT TURN FROM B
 Conflicting Flows=> 2509
 Major road lanes(2 or 4) 4
 Major road sod(30 or 55) 30
 Critical Gap Table 2 T= 5.5
 Capacity, from fig 2= 45
 Demand(B left)= 42
 Capacity used (in "%)= 9Z.ZZZZZ
 Impedance factor, fig 3= .14
 Available reserve* 3
 Delay ?< L.O.S. Table 3= 5
 (A=t,B=2,C=3,D=4,E=5,F=6)

Table 2B
 60 5
 HO 5.5
 120 5.5
 220 6
 Table 2C
 180 6.5
 240 7.5
 330 8
 360 7
 440 9
 480 8
 660 9
 880 " 10

LEFT"TURN FROM~C
 Conflicting Flows= 3651
 Major road lanes(2 or 4) 4
 Major road spd(30 or 55) 30
 Control (stop=4. Yld=3) 4
 Critical Gap*Table 2 T= 8
 Capacity, from fig 2= 20
 Adjustment for Impedance³ 14.2724
 -No Shared Lane.Y=1.N=0 1
 Demand= 20
 Available Reserve⁸ -5.7276
 Delay ?< L.O.S. Table 3= 6
 (A=1,B=2.C=Z,D=4,E=5,F=6)

6-7 D

CAPACITY ANALYSIS FOR SKYLINE DRIVE & FIELDSTONE DRIVE -
INTERSECTION 4

Intersection 4 is one of the two right angle four approach intersections in the study, and the only one existing today. The basic analysis assumes that Site 2 will have its own access road to Skyline Drive at Intersection 5. A CMA analysis was also calculated assuming Site 2 having its access to Fieldstone Drive at Intersection 13 instead of at Intersection 5. The P.M. peak hour will be the critical peak hour because three major shopping areas will use Intersection 4 as part of their access system. Therefore, the P.M. peak hour is the only time period tested.

The first test with CMA was for an intersection with Skyline Drive 5 lanes (62 feet) wide and Fieldstone Drive also 5 lanes wide. In the "Full Development" scenario the CMA analysis indicates a poor Level of service D at a saturation rate of 82%. The CMA indicates a Level of service C at saturation rate of 75% for the "As Zoned" scenario with the same geometry.

The second test was to add a lane for northbound traffic resulting in Skyline Drive being 6 lanes (74 feet) wide. Then the CMA analysis indicates a Level of service C at a saturation rate of 76% for the "Full Development" scenario. With this geometry the "As Zoned" scenario also has a Level of service C but at a saturation rate of 69%. Note that Level of service C ranges from a saturation rate of 66% to 79%.

The third test was to add a lane for southbound Skyline Drive to make the intersection symmetrical. Then Skyline Drive would be 7 lanes (86 feet) wide. The CMA indicates a Level of service B at a saturation rate of 65% for the "Full Development" scenario, and also a Level of service B but at 57% saturation for the "As Zoned" scenario. Note that Level of service B ranges from a saturation rate of 55% to 65%.

The fourth test was to eliminate Intersection 5 from the tableau, assuming access to Site 2 to be via Intersection 13 on Fieldstone Drive. This changes the volumes of traffic for the various movements at Intersection 4. The test was only for the "Full Development" scenario with Skyline Drive 7 lanes (86 feet) wide. The CMA analysis indicates a Level of service E at a saturation level of 105%. Therefore, it can be seen that if Site 2 is to be developed as in the "Full Development" scenario, having its only access to Fieldstone Drive would not be successful from a traffic standpoint.

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & FIELDSTONE DR (INT#A)W»5

DATE 1993 PM PEAK FULL DEVELOPMENT

.....<<.....>>.....
 LEVEL OF SERVICE D
 SATURATION SS
 CRITICAL N/S VOL 1120
 CRITICAL E/W VOL 2B7
 CRITICAL SUM 1487

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 12.0	RT. 13.0	RT. 13.0	RT. 13.0
2	T.. 12.0	T.. 12.0	L.. 12.0	L.. 12.0
3	L.. 12.0	L.. 12.0	L.. 12.0	L.. 12.0
4
5
&

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	196	43	339	130
THRU	1759	1044	22	31
RIGHT	77	251	198	59

	TRUCKS (S>	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	5	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 PEDESTRIAN ACTIVITY : 1. 0 - 9 9 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	1117	770	230	33
LEFT	191	-3	192	57

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	196	43	333	130
ADJUSTED VOL	191	3	366	110
CAPACITY	0	0	0	0
MOVEMENT	N/A	N/A	N/A	N/A

6-3A

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SKYLINE OR * FIELOSTONE DR <INT#4)W#5
DATE 1993 PM PEAK FULL DEVELOPMENT

LEVEL OF SERVICE C
SATURATION 76
CRITICAL N/S VOL 961
CRITICAL E/W VOL 287
CRITICAL SUM 1248

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	RT. 13.0	RT. 13.0	RT. 13.0
2	T.. 12.0	T.. 12.0	L.. 12.0	L.. 12.0
3	T.. 12.0	L.. 12.0	L.. 12.0	L.. 12.0
4	L.. 12.0
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	196	43	333	130
THRU	1739	1044	22	31
RIGHT	77	231	138	59

	TRUCKS $\lt; \gg$	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	5	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :4. BOTH TURNS PROTECTED (WITH OVERLAP)
PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	779	770	£30	93
LEFT	191	3	132	57

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	196	43	339	130
ADJUSTED VOL	191	3	366	110
CAPACITY	0	0	0	0
MOVEMENT	N/A	N/A	N/A	N/A

6-f>r

JOHN F. CHRIST
CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & FIELDSTONE DR (INT#4)W#5

DATE PM PEAK AS ZONED

#**»*****.....

LEVEL OF SERVICE C
SATURATION 69
CRITICAL N/S VOL 858
CRITICAL E/W VOL 274
CRITICAL SUM 1132

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	RT. 13.0	RT. 13.13	RT. 13.0
2	T.. 12.0	T.. 12.0	L. . 12.3	L.. 12.0
3	T.. 12.0	L.. 12.0	L. . 12.3	L.. 12.0
4	<u>1</u> 12.0
5
6

	NORTHBOUND	TRAFFIC VOLUMES SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	196	43	323	121
THRU	1507	876	22	31
RIGHT	76	249	189	59

	TRUCKS (%)	LOCAL BUSES (<#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	5	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :4. BOTH TURNS PROTECTED (WITH OVERLAP)
PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	670	667	221	33
LEFT	191	3	181	51

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	196	43	323	12*
ADJUSTED VOL	191	3	346	39
CAPACITY	0	0 -	0	0
MOVEMENT	N/A	N/A	N/A	N/A

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & FIELDSTONE DR <INT#4>W#5

DATE 1993 PM PEAK AS ZONED

LEVEL OF SERVICE B
 SATURATION 57
 CRITICAL N/S VOL S73
 CRITICAL E/W VOL 274
 CRITICAL SUM 947

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	RT. 13.0	RT. 13.0	RT. 13.0
2	T.. 12.0	T.. 12.0	L.. 12.0	L.. 12.0
3	T.. 12.0	T.. 12.0	L.. 12.0	L.. 12.0
4	L.. 12.0	L.. 12.0
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	196	43	323	121
THRU	1507	S76	22	31
RIGHT	76	249	189	59

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	5	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	670	461	221	93
LEFT	191	3	iai	51

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	196	43	323	121
ADJUSTED VOL	191	3	346	99
CAPACITY	0	0	0	0
MOVEMENT	N/A	N/A	N/A	N/A

6-8 F

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SKYLINE DRIVE4FIELDSTONE WITHOUT INT#5

DATE 1992 PM PEAK FULL DEVELOPMENT

LEVEL OF SERVICE E
SATURATION 105
CRITICAL N/S VOL 1116
CRITICAL E/W VOL 609
CRITICAL SUM 1725

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 12.0	RT. 12.0	RT. 13.0	RT. 13.13
2	T. . 12.0	T. . 12.0	L. . 12.0	L. . 12.3
3	T.. 12.0	T. . 12.0	L. . 12.0	L. . 12.3
4	L.. 12.0	L. . 12.0
5
W

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	193	361	339	301
THRU	1453	726	28	34
RIGHT	£92	251	191	364

	TRUCKS <X>	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	3	0	.9
EASTBOUND	5	0	.9
WESTBOUND	5	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :4. BOTH TURNS PROTECTED (WITH OVERLAP)
PEDESTRIAN ACTIVITY : 1. 0 - 9 9 <#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	723	398	229	417
LEFT	187	393	192	167

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	193	361	339	301
ADJUSTED VOL	187	393	366	319
CAPACITY	0	0	0	0
MOVEMENT	N/A	N/A	N/A	N/A

CAPACITY ANALYSIS FOR SKYLINE DRIVE & SITE 2 DRIVEWAY -
INTERSECTION 5.

Intersection 5 does not currently exist, A quick perusal of the traffic data shows that when developed the intersection volumes will far exceed those that can successfully be handled by STOP sign control. The P.M. peak hour will be the critical peak hour.

The CMA analysis indicates a Level of service D with a saturation rate of 80% with 6 lanes in Skyline Drive and 2 lanes available for left turns from Site 2 during the P.M. peak hour with the "Full Development" scenario. The six lanes in Skyline Drive would be divided evenly with 3 lanes for southbound traffic and 3 lanes for northbound traffic. With the same geometry the CMA yields a Level of service B at a saturation rate of 65% for the "As Zoned" scenario.

Constructing Skyline Drive to a six lane width with a cartway 72 feet wide plus shoulders and a graded utility strip would be difficult because of the ruggedness of the terrain. It is doubtful that a greater roadway width in Skyline Drive could be practically constructed to achieve a better level of service. Therefore, if the "Full Development" scenario is allowed, more complex solutions such as an additional access point to Fieldstone Drive or an English style intersection, using a large access width and interchange area within the site should be investigated.

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & SITE 2 DR <INT#3>

DATE 1393 PM PEAK FULL DEVELOPMENT

LEVEL OF SERVICE D
SATURATION 80
CRITICAL N/S VOL 1168
CRITICAL E/W VOL 206
CRITICAL SUM 1374

###>>>.....>>>###>>>.....>>>

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	T.. 13.0	RT. 12.0
2	T.. 12.0	T.. 12.0	T.. 12.0
3	T.. 12.0	L.. 12.0
4
5
6

	NORTHBOUND	TRAFFIC VOLUMES SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	332	0	0
THRU	1721	1037	0	177
RIGHT	216	0	0	311

	TRUCKS <>	LOCAL BUSES <#/HR>	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.9
EASTBOUND	0	0	1
WESTBOUND	3	0	.3

PHASING N/S :14. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY i 1. 0 - 9 9 <#PDS/HR>
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	811	635	0	006
LEFT	0	357	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	332	0	0
ADJUSTED VOL	0	357	0	0
CAPACITY	0	0	0	206
MOVEMENT	N/A	N/A	OK	OK

G-10 A

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & SITE 2 DR (INT#5)

DATE 1993 PM PEAK AS ZONED

*****-*****-*****-*****-*****

LEVEL OF SERVICE B
SATURATION 65
CRITICAL N/S VOL 965
CRITICAL E/W VOL 156
CRITICAL SUM 1121

*****-*****-*****-*****-*****

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	T. 13.0	RT. 13.0
2	T. 12.0	T. 12.13	T. 12.0
3	T. 12.0	L. 12.0
4
5
6

	NORTHBOUND	TRAFFIC VOLUMES SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	266	0	0
THRU	1505	919	0	134
RIGHT	130	0	0	269

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	0	0	1
WESTBOUND	5	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	689	562	0	156
LEFT	0	276	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	266	0	0
ADJUSTED VOL	0	276	0	0
CAPACITY	0	0	0	156
MOVEMENT	N/A	N/A	OK	OK

6-10B

CAPACITY ANALYSIS FOR SKYLINE DRIVE & KNOLLWOOD DRIVE -
INTERSECTION 6

The unsignalized intersection shows that with either the "As Zoned" scenario or "Full Development" scenario with 1983 background traffic during the P.M. peak hour the demand for left turns from Knollwood Drive will exceed the capacity. Therefore, the capacity of a traffic signal was investigated.

For the CMA analysis five lanes were assumed in Skyline Drive with the middle lane a left turn stacking lane for northbound traffic. Knollwood Drive was assumed to be three lanes wide. With these geometries the CMA analysis shows a Level of service A at a saturation rate of 47% for the "As Zoned" scenario and a Level of service B at a saturation rate of 56% during the A.M. peak hour. During the P.M. peak hour the CMA analysis shows a Level of service B at a saturation rate of 65% for the "As Zoned" scenario and a Level of service C at a saturation rate of 75% for the "Full Development" scenario.

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & KNOLLWOOD DR

DATE 1993 AM PEAK AS ZONED

.....*.....
 LEVEL OF SERVICE A
 SATURATION 47
 CRITICAL N/S VOL 787
 CRITICAL E/W VOL 21
 CRITICAL SUM 808
»»».....».....».....*.....».....

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T. . 13.0	RT. 13.0	RT. 12.3
2	T. . 12.0	T.. 12.0	T.. 12.0
3	L. . 12.0
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	34	0	0	0
THRU	180	1237	23	0
RIGHT	0	57	14	0

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.3
EASTBOUND	5	0	.9
WESTBOUND	0	0	1

PHASING N/S ::4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W ::1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY :: 1. 0 - 9 9 (#PDS/HR)
 CYCLE LENGTH : 30 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	416	787	21	0
LEFT	0	0	0,	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	34	0	0	0
ADJUSTED VOL	0	0	0	0
CAPACITY	0	0	2.X	0
MOVEMENT	N/A	N/A	OK	OK

G-11 A

C

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & KNOLLWOOD DR

DATE 1333 AM PEAK FULL DEVELOPMENT

#.....*.....*.....*.....*.....*.....*.....*.....*.....*.....*

LEVEL OF SERVICE B
 SATURATION 56
 CRITICAL N/S VOL 333
 CRITICAL E/W VOL 23
 CRITICAL SUM 362

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T. . 13.0	RT. 13.0	RT. 13.0	...
2	T. . 12.0	T. . 12.0	T. . 12.0	...
3	L. . 12.0
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	41	0	0	0
THRU	775	1473	23	0
RIGHT	0	70	15	0

	TRUCKS (*>)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.3
EASTBOUND	5	0	.3
WESTBOUND	0	0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 33 <#PEDS/HR>
 CYCLE LENGTH : 30 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	474	338	23	0
LEFT	1	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	41	0	0	0
ADJUSTED VOL	1	0	0	0
CRPGCITY	0	0	23	0
MOVEMENT	N/A	N/A	OK	OK

6-11B

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR 4 KNOLLWOOD DR

DATE 1993 PM PEAK AS ZONED

```
#.....#.....>>>.....*.....
LEVEL OF SERVICE B
SATURATION 65
CRITICAL N/S VOL 1024
CRITICAL E/W VOL 87
CRITICAL SUM 1111
.....<->.....>>>.....>>>.....
```

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T. . 13.0	RT. 13.0	RT. 13.0
£	T. . 12.0	T. . 12.0	T. . 12.0
3	L. . 12.0
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	47	0	0	(3
THRU	1673	1267	91	0
RIGHT	0	67	61	0

	TRUCKS (54)	LOCAL BUSES	C#/HR>	PEAK HOUR FACTOR
NORTHBOUND	5	0	0	.3
SOUTHBOUND	5	0	0	.3
EASTBOUND	5	0	0	.3
WESTBOUND	0	0	0	.1

PHASING N/S s 4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W ; 1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY s 1. 0 - 39 <#PEDS/HR>
 CYCLE LENGTH s 30 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	1024	a11	37	0
LEFT	a	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	47	0	0	0
ADJUSTED VOL	a	0	0	0
CAPACITY	0	0	a7	0
MOVEMENT	N/A	N/A	OK	OK

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & KNOLLWOOD DR

DATE 1393 PM PEAK FULL DEVELOPMENT

*****#*****
 LEVEL OF SERVICE C
 SATURATION 75
 CRITICAL N/S VOL 1139
 CRITICAL E/W VOL 36
 CRITICAL SUM 1235
 *****#*****

LANE	LANE BEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T.. 13.13	RT. 13.13	RT. 13.0
2	T.. 12.0	T.. 12.13	T.. 12.13
3	L.. 12.a
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	51	13	0	a
THRU	1359	1456	93	a
RIGHT	0	70	68	a

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	1	0	.3
SOUTHBOUND	5	0	.3
EASTBOUND	5	0	.3
WESTBOUND	0	0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 39 (#PEDS/HR)
 CYCLE LENGTH : 30 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	1133	328	36	0
LEFT	13	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	51	0	0	0
ADJUSTED VOL	13	0	0	0
CAPACITY	0	13	36	0
MOVEMENT	N/A	N/A	OK	OK

6-11 D

C

Unsignalized "T" Int Cap Calc
 Location Skyline Dr & Knollwood Dr. Intersection 6
 Date 1983
 Day Weekday
 AM or PM Analysis? AM
 Count Data Zone development of sites included in the study

Hourly Demand Volumes:

A Through	1003
A Right	57
B Left	34
B Through	583
C Left	23
C Right	14

RIGHT TURN FROM C

Conflicting Flows	1031.5
Major road lanes (2 or 4)	2
Major road spd (30 or 55)	30
Control (stop-4, Yld-3)	4
Critical Gap Table 2 T*	6
Capacity, from fig 2*	260
Shared Lane-go to L.T.	

No shared lane-Y>1,N<=0	1
Demand<C right"	14
Available Reserve*	266
Delay & L.O.S. Table 3*	3
(A*1,B-2,C-3,D-4,E-5,F*6)	

LEFT-TURN"FR6M~B

Conflicting Flows*	1060
Major road lanes(2 or 4)	4
Major road spd(30 or 55)	30
Critical Gap Table 2 T*	5.5
Capacity, from fig 2 ^s	300
Demand(B left)*	34
Capacity used (in %) *	11.3
Impedance factor, fig 3*	.93
Available reserve*	266
Delay & L.O.S. Table 3*	3
(A=1,B-2,C*3,D-4,E-5,F-6)	

LEFT-TURN-FROM~C

Conflicting Flows*	1648.5
Major road lanes(2 or 4)	4
Major road spd(30 or 55)	20
Control (stop*4, Yld=3)	4
Critical Gap Table 2 T=	3
Capacity, from fig 2=*	40
Adjustment for Impedance*	39.0676

No Shared Lane.Y*1,N=0	1
Demand*	23
Available Reserve*	16.0676
Delay & L.O.S. Table 3 *	5
(A*1,B*2,C*3,D*4,E*5,F*6)	

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

Table 3

-800	6	0	1
0	5	5	.97
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77
		35	.72
		40	.69

Table 2B

60	5	45	.64
110	5.5	50	.6
120	5.5	55	.55
220	6	60	.5
		65	.45
		70	.39

Table 2C

180	6.5	75	.33
240	7.5	30	.27
330	8	85	.2
360	7	90	.14
440	9	95	.08
480	8	100	0
660	9		
880	10		

G-11 E

Unsignalised "T" Int Cap Calc

Location Skyline Dr ?< Knollwood Dr. Intersection 6
 Count Data: Full development of sites included in the study

Date 1983

Day Weekday

~AM" or ~PM Analysts? AM

Hourly Demand Volumes:

A Through	1239
A Right	70
B Left	41
B Through	678
C Left	26
C Right	15

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

RIGHT TURN FROM C

Con-flicting Flows=	1274
Major road lanes (2 or 4)	4
Major road spd (30 or 55)	30
Control (stop=>4, Yld=3)	4
Critical Gap Table 2 T=	6
Capacity, -from -fig 2=	180
Shared Lane-go to L.T.	

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.Z^
80	.27
85	.2
90	.14
95	.08
100	0

No shared lane-Y=1,N=0	1
Demand (C right)=>	15
Available Reserve=	165
Delay ?< L.O.S. Table 3=	4
(A=1,B=2,C=3,D*4,E=5,F=6>	

LEFT~TURN FROM~B

Conflicting Flows-	1309
Major road lanes(2 or 4)	4
Major road spd<30 or 55)	30
Critical Gap Table 2 T=	5.5
Capacity, from fig 2=	210
Demand(B left)=	41
Capacity used (in %)=	19.52381
Impedance factor, fig 3=	.89
Available reserve=	169
Delay S< L.O.S. Table 3=	4
(A=1,B=2,C=3,D=4,E=5.F=6)	

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	8
360	7
440	9
480	8
660	9
880	10

LEFT~TURN FROM~C

Conflicting Flows-	1993
Major road lanes(2 or 4)	4
Major road spd(30 or 55)	30
Control (stop=4, Yld=3)	4
Critical Gap Table 2 T=	3
Capacity, from fig 2=	20
Adjustment for Impedance ³	19.2674

-f*4 Shared Lane, Y=1, N=0	1
Demand=	26
Available Reserve=	-6.7326
Delay !< L.O.S. Table 3=	6
(A=1,B=2.C=3,D=4,E=5,F=6)	

Unsignalized "T" Int Cap Calc

Location Skyline Dr at Knollwood Dr. Intersection 6

Count Data Zone development of sites included in the study

Data _____ 1983

Day _____ TTTT Weekday

AM or PM Analysis? PM

Hourly Demand Volumes:
 A Through 1163
 A Right 67
 B Left 47
 B Through 1443
 C Left 91
 C Right 61

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

RIGHT TURN FROM C
 Conflicting Flows- 1196.5
 Major road lanes (2 or 4) 2
 Major road spd (30 or 35) 30
 Control (stop-4, Yld»3> 4
 Critical Gap Table 2 T- 6
 Capacity, from fig 2= 195
 Shared Lane-go to L.T.

Table 3

-800	6	Figure 1	0	1
0	5		5	.97
100	4		10	.93
200	3		15	.89
300	2		20	.85
400	1		25	.81
10000	0		30	.77
			35	.72
			40	.69

No shared lane-Y«1,N»0 1
 Demand(C right)" 61
 Available Reserve- 134
 Delay & L.O.S. Table 3= 4
 <A-1.B«2,C«3,D«4,E-5.F-6)

LEFT TURN FROM B
 Conflicting Flows* 1230
 Major road lanes(2 or 4) 4
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T- 3.5
 Capacity, from fig 2= 240
 Demand (B left)- 47
 Capacity used (in %>= 19.58333
 Impedance factor, fig 3* .89
 Available reserve* 193
 Delay it L.O.S. Table 3= 4
 (A-1,B-2,C»3,D*4,E-5,F-6)

Table 2B

60	5	45	.64
110	5.5	50	.6
120	5.5	55	.55
220	6	60	.5
		65	.45
		70	.39
180	6.2	75	.33
240	7.5	80	.27
330	3	85	.2
360	7	90	.14
440	9	95	.08
480	8	100	0
660	9		
880	10		

Table 2C

180	6.2	75	.33
240	7.5	80	.27
330	3	85	.2
360	7	90	.14
440	9	95	.08
480	8	100	0
660	9		
880	10		

LEFT TURN FROM C
 Conflicting Flows- 2686.5
 Major road lanes(2 or 4) 4
 Major road spd(30 or 55) 30
 Control (stop»4, Yld-3) 4
 Critical Gap Table 2 T= 8
 Capacity, -from fig 2= 20
 Adjustment -for Impedance³ 19.2674

-No Shared Lane,Y»1.N«0 1
 Demand³ 91
 Available Reserve- -71.7326
 Delay & L.O.S. Table 3= 6
 <A-1.B-2.C=Z,D-4,E«5,F»6)

Unsignalized "T" Int Cap Calc

Location Skyline Dr & Knollwood Dr. Intersection 6
 Count Data: Full development of sites included in the study

Date 1983

Day Weekday

AM~or~PM~Ana7ys7s? PM

Hourly Demand Volumes:

A Through	1352
A Right	70
3 Left	51
B Through	1729
C Left	99
C Right	68
RIGHT TURN FROM C	
Conflicting Flows*	1337
Major road lanes (2 or 4)	4
Major road spd <30 or 55>	30
Control (stop*4, Yld=3>	4
Critical Gap Table 2 T=	6
Capacity, -from fig 2=	150
Shared Lane-go to L.T.	

Table 2A

ISO	5
240	6
330	6
360	5
440	7
480	6
660	6
380	7

No shared Lane-Y*7,N=0	1
Demand(C right)=	68
Available Reserve*	82
Delay it L.O.S. Table 3=	5
(A=1,B=2.C=3.D=4,E=5.F=6)	

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

u	1
5	.97
10	.93
15	.89
20	.85
25	.91
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.3^
80	.27
85	.2
90	.14
95	.08
100	0

LiFT~TURN"FROM~i	
Conflicting Flows*	1422
Major road lanes(2 or 4)	4
Major road spd(30 or 55)	30
Critical Gap Table 2 T=	5.5
Capacity, from fig 2=	180
Demand(B left)=	51
Capacity used (in "/.) * 23.ZZZZ	
Impedance factor, fig 3=	.81
Available reserve*	129
Delay ?< L.O.S. Table 3=	4
(A=1.B=2.C=3,D=>4.E=5.F=6)	

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	8
360	7
440	9
480	8
660	9
880	10

LEFT~TURN FROM~C	
Conflicting Flows*	3167
Major road lanes(2 or 4)	4
Major road spd<30 or 55)	30
Control (stop=4, Yld=3)	4
Critical GaD Table 2 T=	8
Capacity, from fig 2=	20
Adjustment for Impedance*	18.7346

-No Shared Lane,Y=1.N=0	1
Demand*	99
Available Reserve*	-80.2654
Delay ?< L.O.S. Table 3=	6
(A=1.B=2,C=3,D=4.E=5.F=6)	

CAPACITY ANALYSIS FOR SKYLINE DRIVE AND ERSKINE ROAD -
INTERSECTION 7

This intersection exists with the west approach of Skyline Drive and the Eskine Road approach being the "thru" approaches with a STOP sign facing westbound Skyline Drive traffic. For this study the STOP sign is assumed to face southbound Erskine Road traffic, with the eastbound and westbound Skyline Drive approach the "through street". In the CMA analysis Erskine Road is again considered to be the stem of the "T" type intersection.

The unsignalized intersection analysis indicates that the demand for left turns from Erskine Road to Skyline Drive will exceed the capacity to make that movement in either the "As Zoned" or "Full Development" scenarios even with 1983 background. Therefore, roadway improvements and a traffic control signal will become necessary as the area develops.

Skyline Drive was assumed to be 5 lanes wide and Erskine Road 3 lanes wide for the CMA signalized intersection analysis. The five lanes in Skyline Drive would be divided into 3 lanes eastbound and 2 lanes westbound. The middle lane in the roadway would be a left turn stacking lane for eastbound traffic on Skyline Drive. Erskine Road would have two lanes turning left into Skyline Drive. The right turn from Erskine Road would be a free right turn and not enter the analysis.

The CMA analysis indicates that with this geometry a Level of service A at a saturation rate of 51% for the "As Zoned" scenario and a Level of service B at 60% saturation for the "Full Development" scenario during the A.M. peak hour. During the P.M. peak hour, the CMA analysis indicates that there would be a Level of service C at a saturation rate of 73% for the "As Zoned" scenario and a Level of service D at a saturation rate of 83% for the "Full Development" scenario. An additional westbound through lane would be needed to raise the Level of service to a C level for the "Full Development" scenario.

C

Unsignalized "T" Int Cap Calc
 Location Skyline Dr ?< Erskine Road Intersection 7
 Count Data: Zone development of sites included in the study

Date 1983
 Day Weekday
 ~AM~or~PM~AnaFys7s? AM

Hourly Demand Volumes:
 A Through 536
 A Right 65
 B Left 35
 B Through 790
 C Left 200
 C Right 80
 RIGHT TURN FROM C
 Conflicting Flows=> 568.5
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2= 490
 Shared Lane-go to L.T.

 No shared lane-Y=i,N=0 1
 Demand<C right)= 80
 Available Reserve* 410
 Delay it L.Q.S. Table 3= 1
 (A=1,B=2,C=Z,D=4,E=5,F=*6)

 LEFT TURN FROM B
 Conflicting Flows* 601
 Major road lanes(2 or 4) 4
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T= 5.5
 Capacity, from fig 2= 550
 Demand(B left)= 35
 Capacity used (in '/.)= 6.363636
 Impedance factor, fig 3= .97
 Available reserve* -515
 Delay ?< L.O.S. Table 3= 1
 (A=1,8=2,C=3.D=4,E=5,F=6)

 LEFT~TURN~FROM~C
 Conflicting Flows= 1393.5
 Major road lanes(2 or 4) 4
 Major road spd(30 or 55) 30
 Control <stop=4, Yld=3) 4
 Critical Gap Table 2 T= 8
 Capacity, from fig 2= 60
 Adjustment for Impedance⁵* 59.4006

 -No Shared Lane,Y=1,N=0 1
 Demand* 200
 Available Reserve² -140.599
 Delay S< L.O.S. Table 3= 6
 (A=1,B=2,C=3,D=4,E=5,F=6)

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

Table 3	Figure 3
-800	0
~	1
100	.97
200	.93
300	.89
400	.81
10000	.77
	.75
	.69
	.64
	.6
	.55
	.5
	.45
	.39
	.33
	.27
	.2
	.14
	.08
	0

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	3
360	7
440	9
480	3
660	9
380	10

G-12. A

Unsignalized "T" Int Cap Calc
 Location _____ Skyline Dr it Erskine Road Intersection 7
 Count Data Tzone development of sites included in the study
 Date _____ 1983

Day _____ * Weekday
 AH or PM Analysis? PM

Hourly Demand Volumes:
 A Through 1322
 A Right 212
 B Left 59
 B Through 1133
 C Left 97
 C Right 40
 RIGHT TURN FROM C
 Conflicting Flows- 142B
 Major road lanes (2 or 4) 2
 Major road spd (30 or S3) 30
 Control (stop-4, Yld»3) 4
 Critical Gap Table 2 T» 6
 Capacity, from fig 2* 140
 Shared Lane-go to L.T.

Table 2A

180	5
240	6
330	4
360	5
440	7
480	6
660	6
880	7

 ~No snared Lane-Y»1^N»O 1
 Demand(C right)- 40
 Available Reserve* 100
 Delay & L.O.S. Table 3- 4
 (A<1,B>2,C»3,D<4,E»5,F-6)

Table 2
 Figure 3

-800	6	0	1
0	5	5	.97
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77
		35	.72
		40	.69
		45	.64
		50	.6
		55	.55
		60	.5
		65	.45
		70	.39
		75	.33
		80	.27
		85	.2
		90	.14
		95	.08
		100	0

 LEFT TURN-FROM~i
 Conflicting Flows* 1534
 Major road lanes(2 or 4) 4
 Major road spd(30 or 35) 30
 Critical Gap Table 2 T= 5.5
 Capacity, from fig 2^s 250
 Demand(B left)* 59
 Capacity used (in 7.)- 23.6
 Impedance factor, fig 3* .85
 Available reserve- 191
 Delay & L.O.S. Table 3* 4
 (A<t.B»2,C»3,D<4,E»5,F-6)

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	8
360	7
440	6
480	8
660	8
880	10

 LEff-fURN~FR6fi~C
 Conflicting Flows- 2620
 Major road lanes(2 or 4) 4
 Major road spd(30 or 55) 30
 Control (stop»4, Yld-3) 4
 Critical Gap Table 2 T- 8
 Capacity, -from fig 2= 20
 Adjustment for Impedance- 19.001

 -No Shared Lane.Y»t,N«O 1
 Demand- 97
 Available Reserve- -77.999
 Delay ?< L.O.S. Table 3- 6
 (A<1,B»2,C=3,D=4,E»5.F»6)

6-12 B

f

Unsignalised "T" Int Cap Calc
 Location Skyline Dr & Erskine Road Intersection 7
 Count Data: Full development of sites included in the study

Date 1983
 Day Weekday
 AM oV~PM~AnaTysTs? AM

Hourly Demand Volumes:

A Through	635
A Right	65
B Left	35
B Through	1039
C Left	200
C Right	80

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

RIGHT TURN FROM C
 Conflicting Flows= 667.5
 Major road lanes (2 or 4) 4
 Major road spd (30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2= 430
 Shared Lane-go to L.T.

 No shared lane-Y=1,N=0 1
 Demand(C right)= 80
 Available Reserve= 350
 Delay S< L.O.S. Table 3= 2
 (A=1,B=2,C=3,D=4,E=5,F=6)

Table 3		Figure 3	
-800	6	0	1
0	5	5	.97
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77
		35	.72

 LEFT~TURN~FROM~B
 Conflicting Flows= 700
 Major road lanes(2 or 4) 4
 Major road spd<30 or 55) 30
 Critical Gap Table 2 T= 5.5
 Capacity, from fig 2= 490
 Demand(B left)= 35
 Capacity used (in 7.)= 7.142857
 Impedance factor, fig 3= .97
 Available reserve⁸ 455
 Delay & L.O.S. Table 3= 1
 (A=1,B=2,C=3,D=4,E=5,F=6>)

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

130	6.5	75	.32-
240	7.5	80	.27
330	8	85	.2
360	7	90	.14
440	9	95	.08
480	8	100	0
660	8		
880	10		

 LEFT~fuRN~FROM~C
 Conflicting Flows= 1741.5
 Major road lanes(2 or 4) 4
 Major road spd(30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T= 8
 Capacity, from fig 2= 20
 Adjustment for Impedance* 19.8002

-No Shared Lane,Y=1,N=0 1
 Demand= 200
 Available Reserve* -180.200
 Delay * L.O.S. Table 3= 6
 (A=1,B=2.C=3,D=4,E=5,F=6~)

6-12 C

C

Unsignalised "T" Int Cap Calc

Location Skyline Dr 5c Erskine Road Intersection 7
 Count Data: Full development of sites included in the study

Oats 1983

Day Weekday

AM or PM Analysts? PM

Hourly Demand Volumes:

A Through	1615
A Right	212
B Left	59
B Through	1325
C Left	97
C Right	40
RIGHT TURN FROM C	
Conflicting Flows*	1721
Major road lanes (2 or 4)	4
Major road spd (30 or 55)	30
Control (stop=4. Yld=3)	4
Critical Gap Table 2 T»	6
Capacity, from fig 2 ^s	40
Shared Lane-go to L.T.	

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

No-shared Lane-Y»T7N*0

Demand(C right)*	40
Available Reserve*	0
Delay % L.O.S. Table 3*	5
(A=1.B*2,C*3,D-4,E»5.F»6)	

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

LEFT TURN FROM B

Conflicting Flows-	1827
Major road lanes(2 or 4)	4
Major road sod(30 or 55)	30
Critical Gao Table 2 T*	5.5
CaDacity, from fig 2 ^s *	45
Demand(B left)*	59
Capacity used (in %)*	131.1111
Impedance factor, fig 3=	0
Available reserve*	-14
Delay % L.O.S. Table 3*	6
(A»1.8«2.C»3,D-4.E*5,F-6>	

Table 2B

60	5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	9
360	7
440	9
480	8
660	9
880	10

LEFT "TURN" *FR6M-C

Conflicting Flows*	3105
Major road lanes(2 or 4)	4
Major road spd(30 or 55)	30
Control (stop=4. Yld=3)	4
Critical Gap Table 2 T»	8
Capacity, from fig 2=	20
Adjustment for Impedance*	13.34

-No Shared Lane.Y»1,N*0

Demand ³	97
Available Reserve*	-83.66
Delay it L.O.S. Table 3*	6
<A*I.B-2.C=3,D*4.E-5.F-6)	

6-12 D

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & ERSKINE RD (INT.7)

DATE 1993 AM PEAK AS ZONED

*****#*****#*****#
 LEVEL OF SERVICE A
 SATURATION 51
 CRITICAL N/S VOL 313
 CRITICAL E/W VOL 570
 CRITICAL SUM 883
 *****#*****#*****#

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T.. 13.0	T.. 13.0	RT. 13.ft
2	T.. 12.0	T.. 12.0	T.. 12.0
3	L.. 12.0
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	0	47	0
THRU	0	269	931	609
RIGHT	0	103	0	37

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	0	0	1
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	5	0	.9

PHASING N/S : 1. NEITHER TURN PROTECTED
 E/W : 4. BOTH TURNS PROTECTED (WITH OVERLAP)
 PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	0	313	570	418
LEFT	0	0	a	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	0	47	0
ADJUSTED VOL	0	0	8	0
CAPACITY	0	313	0	156
MOVEMENT	OK	OK	N/A	N/A

6-12L F

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & ERSKINE RO (INT. 7)

DATE 1993 AM PEAK FULL DEVELOPMENT

*****><<>>>>>>>>>>>>>>>>>>>>>>>>>*****

LEVEL OF SERVICE B
SATURATION 60
CRITICAL N/S VOL 313
CRITICAL E/W VOL 722
CRITICAL SUM 1035

LANE	NORTHBOUND		LANE GEOMETRY		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	T..	13.0	T..	13.13	RT..	13.0		
3	T..	12.0	T..	12.0				
4	L..	12.0				
S				
S				

	NORTHBOUND		TRAFFIC VOLUMES		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
LEFT	0		0		47		0	
THRU	0		269		1180		707	
RIGHT	0		108		0		87	

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	0	0	1
SOUTHBOUND	5	0	.3
EASTBOUND	5	0	.3
WESTBOUND	5	0	.3

PHASING N/S :1. NEITHER TURN PROTECTED
E/W :4. BOTH TURNS PROTECTED (WITH OVERLAP)
PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PEPS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	0	313	722	478
LEFT	0	0	a	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	0	47	0
ADJUSTED VOL	0	0	a	0
CAPACITY	0	313	0	156
MOVEMENT	OK	OK	N/A	N/A

6-12F

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SKYLINE DR & ERSKINE RD (INT. 7)

DATE 1993 PM PEAK FULL DEVELOPMENT

 LEVEL OF SERVICE D
 SATURATION 83
 CRITICAL N/S VOL 151
 CRITICAL E/W VOL 1282
 CRITICAL SUM 1433

LANE	NORTHBOUND		LANE GEOMETRY		EASTBOUND		WESTBOUND	
	MOV	WIDTH	SOUTHBOUND	MOV WIDTH	MOV	WIDTH	MOV	WIDTH
1	T.	13.13	T.	13.0	RT.	13.0
2	T.	12.0	T.	12.0	T.	12.0
3	L.	12.0
4
5
6

	NORTHBOUND		TRAFFIC VOLUMES		EASTBOUND		WESTBOUND	
	LEFT	THRU	SOUTHBOUND	THRU	RIGHT	LEFT	THRU	RIGHT
	0	0	0	130	54	79	139S	0
								1773
								285

	TRUCKS (%)	LOCAL BUSES	<#/HR)	PEAK HOUR	FACTOR
NORTHBOUND	0		0		1
SOUTHBOUND	5		0		.9
EASTBOUND	5		0		.9
WESTBOUND	5		0		.9

PHASING N/S :1. NEITHER TURN PROTECTED
 E/W :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 PEDESTRIAN ACTIVITY : 1. 0 - 9 9 <#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	0	151	855	1235
LEFT	0	0	47	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	0	79	0
ADJUSTED VOL	0	0	47	0
CAPACITY	0	151	0	156
MOVEMENT	OK	OK	N/A	N/A

CAPACITY ANALYSIS FOR GREENWOOD LAKE TURNPIKE AND SKYLINE DRIVE -
INTERSECTION 8

A quick perusal of the traffic data shows that a traffic signal will be necessary at this intersection. Therefore, only the CMA signalized intersection analysis is presented. Greenwood Lake Turnpike is assumed to be five lanes wide, with one lane for through southbound traffic and two lanes for southbound left turns for the first test. Skyline Drive was considered to have two westbound lanes, one for left turns and one for right turns. For the "Full Development" scenario during the P.M. peak hour, the CMA analysis indicates a Level of service E at a saturation rate of 109%. An additional northbound through lane and an additional westbound left turn lane was added for the second test. Then the CMA indicates a Level of service D at a saturation rate of 82% for the "Full Development" scenario during the P.M. peak hour.

Using the latter geometry as described above, the CMA analysis indicates a Level of service C at a saturation rate of 72% during the P.M. peak hour with the "As Zoned" scenario.

The A.M. peak hour is less critical than the P.M. peak hour. Whereas the six lane Skyline Drive configuration shows an 82% saturation in the P.M. peak, the CMA analysis shows a Level of service B at a saturation rate of 66% for the "Full Development" scenario during the A.M. peak hour. Dropping a lane so that Skyline Drive has 5 lanes still yields an acceptable level of service during the A.M. peak hour; Level of service C at a saturation rate of 74% for the "Full Development" scenario and Level of service B at a saturation rate of 65% for the "As Zoned" scenario.

6-13-7

MO 96S	MO 0 0 0	0/N 313 1380 Z.9TI	tf/N 0 0 0	1N3W3A0W A113ftdJ3 HOA asisnraw awmoA mdNi
WESTBOUND 2	ai\inoaisb3	aNnoaHinos	ONnoaHidON	

M33H3 TURN ±3-I

WESTBOUND 898	0 0	724 0Z9	0	LEFT iH9ia- naHi
WESTBOUND	aNnoaisws	aNnoaHinos	ONnoaHidON	

1N3W3A0W AS S3WmOA 3NW1 -1W3I1IM3

SON033S 06 ' . H19N3H 3H3A3
 (HH/Sa3d#) 6 6 - 0 'I s A11A113W N<Id1S3Q3d
 Q31D310ad M3HJ.I3N M/3
 a31D310dd 808 HJ.08 S/N SNISWHD
 (dW"LM3A0 HUM)

PEAK HOUR FACTOR	0 0 0 0	0 0 0 0	5 0 5 5	awnoaissM EASTBOUND aNnoaHinos ONnoSHLHON
1303 513 0	0 0 0	0 600 1167	543 426 0	IHSI THRU 1J31

WESTBOUND	arvinoaisb3	SOUTHBOUND	QNnoaHlUON	
-----------	-------------	------------	------------	--

TRAFFIC AOWmas

.....	6
.....	5
.....	2
13.0	1.1	13.0	13.0	I

WESTBOUND HiaiM AOW	EASTBOUND HIDIM AOW	aNnoaHinos HiaiM AOW	NORTHBOUND HIOifi AOW	3Ntn
------------------------	------------------------	-------------------------	--------------------------	------

Af13W039 3NW1

Z99T wnS -1W3I1IM3
 B6S IDA M/3 -1W3I1IH3
 693T HOA S/N -1W3I1IM3
 SATURDAY 109
 3 33IAM3S JO "I5A31

±N3WdO13A3a FULL PEAK 1993 Wd 310<0 (#1NI)da SNIAMS ? dl 3<<n a00MN33d9

CRITICAL AOW3A0W ANALYSIS
 1S18H3 '3 NHOF

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SKYLINE DR (INT#S)

DATE 1993 PM PEAK FULL DEVELOPMENT

LEVEL OF SERVICE D
SATURATION 32
CRITICAL N/S VOL 1096
CRITICAL E/W VOL 314
CRITICAL SUM 1410

*****#*****#*****#*****<*****

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	RT. 13.0	R.. 13.0
2	T.. 12.0	L.. 12.0	T.. 12.0
3	T.. 12.0	L.. 12.0	T.. 12.2
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	1167	0	0
THRU	426	600	0	513
RIGHT	543	0	0	1303

	TRUCKS C/.)	LOCAL BUSES <#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	0	0	1
WESTBOUND	5	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 9 9 <#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	372	630	0	31*
LEFT	0	724	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	1167	0	0
ADJUSTED VOL	0	1380	0	0
CAPACITY	0	313	0	314
MOVEMENT	N/A	N/A	OK	OK

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SKYLINE DR(INT#8)

DATE 1993 PM PEAK AS ZONED

LEVEL OF SERVICE C
 SATURATION 72
 CRITICAL N/S VOL 948
 CRITICAL E/W VOL £90
 CRITICAL SUM 1238

.....

LANE	NORTHBOUND		LANE GEOMETRY		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	RT.	12.0	RT.	12.0	R..	13.0
2	T..	12.0	L..	12.0	T..	12.0
3	T..	12.0	L..	12.0	T..	12.0
4
5
6

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	1018	0	(3
THRU	342	632	0	475
RIGHT	499	0	0	1046

	TRUCKS (5L)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.3
EASTBOUND	0	0	.1
WESTBOUND	5	0	.3

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVEFUAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PEDS/HR>
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	320	663	0	
LEFT	0	£28	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	1018	0	0
ADJUSTED VOL	0	1198	0	0
CAPACITY	0	0	0	£90
MOVEMENT	N/A	N/A	OK	OK

£-'3c

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SKYLINE DR<INT#8)

DATE 1993 AM PEAK FULL DEVELOPMENT

LEVEL OF SERVICE B
SATURATION 66
CRITICAL N/S VOL 989
CRITICAL E/W VOL 143
CRITICAL SUM 1132
*****#*****

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	RT. 13.0	R. . 13.0
2	T. . 12.0	L. . 12.0	T. . 12.0
3	T. . 12.0	L. . 12.0	T. . 12.0
4
5
6

	NORTHBOUND	TRAFFIC VOLUMES SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	1117	0	0
THRU	437	380	0	235
RIGHT	318	0	0	599

	TRUCKS (%)	LOCAL BUSES <#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	0	0	1
WESTBOUND	5	0	.9

PHASING N/S =A. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	297	399	0	143
LEFT	0	692	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	1117	0	0
ADJUSTED VOL	0	1319	0	0
CAPACITY	0	0	0	143
MOVEMENT	N/A	N/A	OK	OK

6-13 D

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SKYLINE DR<INT#8)

DATE 1993 AM PEAK FULL DEVELOPMENT

«-»*.....«.....*.....*.....*

LEVEL OF SERVICE C
SATURATION 74
CRITICAL N/S VOL 1126
CRITICAL E/W VOL 143
CRITICAL SUM 1269

.....#.....».....».....».....».....».....».....».....».....».....».....».....».....».....».....».....».....*.....

LANE	LANE GEOMETRY							
	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	RT.	13.0	RT.	13.0	R..	13.0
2	T..	12.0	L..	12.0	T..	12.0
3	L..	12.0	T..	12.0
4
3
6

	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
LEFT	0		1117		0		0	
THRU	437		380		0		235	
RIGHT	318		0		0		599	

	TRUCKS <»	LOCAL BUSES (* / HR >	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.9
EASTBOUND	0	0	1
WESTBOUND	5	0	.9

PHASING N/S : 4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W : 1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	434	399	0	143
LEFT	0	692	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	1117	0	0
ADJUSTED VOL	0	1319	0	0
CAPACITY	0		0	143
MOVEMENT	N/A	N/A	OK	OK

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SKYLINE DR(INT#8>

DATE 1383 AM PEAK AS ZONED

*****#*****#*****#*****#*****#

LEVEL OF SERVICE B
SATURATION 65
CRITICAL N/S VOL 936
CRITICAL E/W VOL 129
CRITICAL SUM 1125

*****#*****#*****#*****#*****#

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	RT. 13.0	R. 13.0
2	T. 12.0	L. 12.0	T. 12.0
3	L. 12.0	T. 12.0
4
5
6

	NORTHBOUND	TRAFFIC VOLUMES SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	362	0	0
THRU	484	312	0	211
RIGHT	304	0	0	525

	TRUCKS <+/->	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.9
EASTBOUND	0	0	1
WESTBOUND	5	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :1. NEITHER TURN PROTECTED.
PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	455	327	0	123
LEFT	0	541	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	382	0	0
ADJUSTED VOL	0	1031	0	0
CAPACITY	0	0	0	129
MOVEMENT	N/A	N/A	OK	OK

6-13F

CAPACITY ANALYSIS FOR GREENWOOD LAKE TURNPIKE & WEST BROOK ROAD -
INTERSECTION 9

The A.M. peak hour will be the critical peak hour at this location. The **unsignalized intersection** capacity analysis shows that the **capacity for left turns from West Brook Road** will be exceeded in both the **"As Zoned"** and **"Full Development"** scenarios. Therefore, a CMA analysis was run.

A **three lane configuration** was assumed in both Greenwood Lake Turnpike and West Brook Road. The CMA analysis indicates a Level of service A for both the **"As Zoned"** and **"Full Development"** scenarios.

Unsignalised "T" Int Cap Calc Intersection 9
 Location Greenwood Lk. Toe. & West Brook Road
 Count Data: Full development of sites included in the study

Date 1993
 Day Weekday

AM or FM Analysis? AM
 Hourly Demand Volumes:
 A Through 552
 A Right 43
 B Left 45
 B Through 495
 C Left 193
 C Right 239

RIGHT TURN FROM C
 Conflicting Flows- 573.5
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control <stop=4, Yld=3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2= 390
 Shared Lane-go to L.T.

No shared lane-Y=1,N=0 1
 Demand(C right)- 239
 Available Reserve³ 151
 Delay & L.O.S. Table 3= 4
 (A=1,B=2,C=3,D=4.E=5,F=6)

LEFT TURN FROM B
 Conflicting Flows- 595
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T= 5
 Capacity, from fig 2= 640
 Demand(B left)= 45
 Capacity used (in %)= 7.03125
 Imoedance factor, fig 3= .97
 Available reserve- 595
 Delay ?< L.O.S. Table 3= 1
 <A=1.B=2.C=3,D=4.E=5,F=6)

LEFT~TURN~FROM~C
 Conflicting Flows- 1113.5
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stap=4, Yld=3) 4
 Critical Gap Table 2 T= 7.5
 Capacity, from flg 2= 130
 Adjustment for Impedance- 12S.7013

-No Shared Lane,Y=1.N=0 1
 Demand- 193
 Available Reserve= -64.2987
 Delay ?< L.O.S. Table Z= 6
 (A=1.B=2,C=Z,D=4.E=5.F=6)

Table 2A

130	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

Table 3

-800	6	0	1
0	5	5	.97
100	4	10	.93
200	3	15	.89
300	^	20	.85
400	1	25	.81
10000	0	30	.77

Table 2B

60	5	40	.69
110	5.5	45	.64
120	5.5	50	.6
220	6	55	.55
		60	.5
		65	.45
		70	.39

Table 2C

180	6.5	75	.33
240	7.5	30	.27
330	8	85	.2
360	7	90	.14
440	9	95	.08
480	8	100	0
660	9		
380	10		

G-17A

Unsignalized "T" Int Cap Calc	Intersection 9		
Location _____	Greenwood Lk. Tpe. & West Brook Drive		
Count Data: Zone development of sites included in the study			
Date _____	1993		
Day _____	Weekday		
AH or PM Analysis?	All		
Hourly Demand Volumes:	Table 2A		
A Through	464	180	5
A Right	38	240	6
B Left	43	330	6
B Through	339	360	5
C Left	182	440	7
C Right	223	480	6
		660	6
		880	7
RIGHT TURN FROM C Conflicting Flows"	483		
Major road lanes (2 or 4)			
Major road spd (30 or 55)	Z0		
Control <stop*4, Yld-3)	4		
Critical Gao Table 2 T*	6		
Capacity, from fig 2= Shared Lane-go to L.T.	560		

No shared lane-Y>1.N*0	1		
Demand(C right)*	223		
Available Reserve*	337		
Delay & L.O.S. Table 3*	2		
(A=1,B*2,C*3.D*4,E-5.F*6)			

LEFT TURN FROM B			
Conflicting Flows*	502		
Major road lanes(2 or 4)	2		
Major road sod(30 or 55)	30		
Critical Gao Table 2 T*	5		
Capacity, from fig 2*	705		
Demand(B left)*	43		
Capacity used (in 7.)*	6.099291		
Impedance factor, fig 3*	.97		
Available reserve*	662		
Delay & L.O.S. Table 3*	1		
(A=1,B*2.C-3.D*4,E*5,F*6)			

^LEFT~TURN~FROM~C			
Conflicting Flows*	1065		
Major road lanes(2 or 4)	2		
Major road sod(30 or 55)	30		
Control (stop*4, Yld*3)	4		
Critical Gao Table 2 T*	7.5		
Capacity, from -fig 2*	140		
Adjustment for Impedance*	138.6014		

-No Shared Lane.Y*1.N*0	1		
Demand*	182		
Available Reserve*	-43.3986		
Delay fc L.O.S. Table 3*	6		
(A*1,B*2.C*3.D*4.E=5,F*6)			

	Table 3	Figure 3
-800	6	0
0	5	5
100	4	10
200	Y	15
300	2	20
400	1	25
10000	0	30
		35
	Table 2B	40
60	5	45
110	5.5	50
120	5.5	55
220	6	60
		65
	Table 2C	70
180	6.5	75
240	7.5	80
330	3	85
360	7	90
44.0	0	95
480	8	100
660	0	
880	10	

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & WEST BROOK RD

DATE 1993 AM PEAK FULL DEVELOPMENT

.....
 LEVEL OF SERVICE A
 SATURATION 47
 CRITICAL N/S VOL 593
 CRITICAL E/W VOL 212
 CRITICAL SUM 805
 *****#*****

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T. . 14.0	RT. 14.0	R. . 13.0
2	L. . 12.0	T. . 12.0
3
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	45	0	0	0
THRU	495	552	193	0
RIGHT	0	43	239	0

	TRUCKS (%)	LOCAL BUSES <#/HR>	PEAK HOUR FACTOR
NORTHBOUND	10	0	1
SOUTHBOUND	10	0	1
EASTBOUND	10	0	1
WESTBOUND	10	0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 (ttPEDS/HR)
 CYCLE LENGTH : 30 seconds

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	490	588	212	0
LEFT	5	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	45	0	0	0
ADJUSTED VOL	5	0	0	0
CAPACITY	0	0	212	0
MOVEMENT	N/A	N/A	OK	OK

6-14C

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & WEST BROOK RD

DATE 1993 flm PEAK AS ZONED

LEVEL OF SERVICE A
SATURATION 63
CRITICAL N/S VOL 533
CRITICAL E/W VOL 0
CRITICAL SUM 733

LANE	LANE GEOMETRY							
	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	T.k	14.13	RT.	14.0	R..	13.a
2	L..	12.0	T..	12-13
3
4
5
6

	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
LEFT		43		0		0		13
THRU		539		464		182		0
RIGHT		0		38		223		

	TRUCKS (%)	LOCAL BUSES	<#/HR>	PEAK HOUR FACTOR
NORTHBOUND	10		0	1
SOUTHBOUND	10		0	1
EASTBOUND	10		0	1
WESTBOUND	10		0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :i. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 9 9 <#PDS/HR>
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	533	496	2013	0
LEFT	3	0	13	3

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	43	0	13	0
ADJUSTED VOL	3	0	0	0
CAPACITY	0	0	200	0
MOVEMENT	N/A	N/A	OK	OK

6-14D

CAPACITY ANALYSIS FOR GREENWOODLAKE TURNPIKE &. STONETOWN ROAD -
INTERSECTION 14

The critical peak hour at this location will be the A.M. peak. The unsignalized intersection capacity analysis shows a Level of service E for westbound traffic on Stonetown Road turning left onto Greenwood Lake Turnpike.

A three lane configuration in Greenwood Lake Turnpike was used in the CMA analysis. It gave a Level of service A for both the "As Zoned" and "Full Development" scenarios. A three or four lane configuration in Greenwood Lake Turnpike and a three lane configuration in Stonetown Road should prove adequate.

Unsignalized "T" Int Cap Calc Intersection 14
 Location..... Greenwood Lk Trk & Stonetown Rd
 Count Data: Full development of sites included in the study

Date _____ 1993
 Day _____ Weekday

AM~or~PM Analysis? AM

Hourly Demand Volumes:

A Through	577
A Right	37
B Left	7
B Through	399
C Left	143
C Right	54

RIGHT TURN FROM C
 Conflicting Flows' 595.5
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop*4, Yld*3) 4
 Critical Gap Table 2 T- 6
 Capacity, from fig 2^s 470
 Shared Lane-go to L.T.

Table 2A

180	5
240	6
330	6
360	5
440	7
430	6
660	6
880	7

 No shared Lane-Y»i7N*O 1
 Demand<C right)³ 54
 Available Reserve- 416
 Delay it L.O.S. Table 3= 1
 (A-1,B-2,C«3,D«4,E*5.F-6)

Table 3

-800	6	0	1
0	5	5	.97
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77

Figure 3

 LEFT TURN FROM B
 Conflicting Flows** 614
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T= 5
 Capacity, from fig 2* 620
 Demand(B left)" 7
 Capacityused(in'/.)* 1.129032
 Impedance factor, fig 3^s 1
 Available reserve* 613
 Delay & L.O.S. Table 3= 1
 <A*1,B«2,C-3,D-4,f«5,F-6)

Table 2B

60	5	45	.64
110	5.5	50	.6
120	5.5	55	.55
220	5	60	.5
		65	.45
		70	.39
180	6.5	75	.3^
240	7.5	80	.27
330	8	35	.2
360	7	90	.14
440	9	95	.08
480	8	100	0

 LEFT~TURN~FROM~C
 Conflicting Flows= 1001.5
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop*4, Yld»3) 4
 Critical Gap Table 2 T= 7.5
 Capacity, from fig 2= 160
 Adjustment for Impedance³ 160

 -No Shared Lane,Y»1,N«0 1
 Demand³ 143
 Available Reserve* 17
 Delay !« L.O.S. Table 3= 5
 (A»1.8=2.C*3,D*4.E=5.F»6)

G-15 A

Unsignalized "T" Int Cap Calc Intersection 14
 Location Greenwood Lk Tpk & Stonetown Rd
 Count Data: Zone development of sites included in the study
 Date 1993
 Day Weekday

AM or ~PM~Analysis? AM
 -Hourly Demand Volumes:
 A Through 511
 A Right 29
 B Left 7
 B Through 399
 C Left 149
 C Right 54

RIGHT TURN FROM C
 Conflicting Flows³ 525.5
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T=
 Capacity, from fig 2= 6
 520
 Shared Lane-go to L.T.

 No shared lane-Y=1,N=0 1
 Demand(C right)³ 54
 Available Reserve³ 466
 Delay ?< L.O.S. Table 3=
 (A=1,B=2.C=3,D=4,E=5,F=6) 1

 LEFT TURN FROM B
 Conflicting Flows³ 540
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T=
 Capacity, from fig 2= 680
 Demand(B left)³ 7
 Capacity used (in V.) = 1.029412
 Impedance factor, fig 3= 1
 Available reserve³ 673
 Delay & L.O.S. Table 3³ 1
 (A=1.B=2.C=3,D=4,E=5,F=6)

 LEFT~TURN~FROM~C
 Conflicting Flows³ 931.5
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop=4, Yld³3) 4
 Critical Gap Table 2 T³ 7.5
 Capacity, from fig 2=
 Adjustment for Impedance³ 180
 180

 -No Shared Lane.Y=1.N=0 1
 Demand³ 149
 Available Reserve=
 Delay ?< L.O.S. Table 3=
 (A=1,B=2.C=3.D=4,E=5,F=6) 5

Table 2A

1	8	0	5
2	4	0	6
3	3	0	6
3	6	0	5
4	4	0	7
4	8	0	6
6	6	0	6
8	8	0	7

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	8
360	7
440	9
480	8
660	9
880	10

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE IP & STONETOWN RD

DATE 1993 AM PEAK AS ZONED

LEVEL OF SERVICE A
SATURATION 41
CRITICAL N/S VOL 533
CRITICAL E/W VOL 163
CRITICAL SUM 696

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T.. 14.0	RT. 14.0	R.. 13.0
2	L.. 12.0	...	T.. 12.0
3
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	7	0	0	0
THRU	399	511	149	0
RIGHT	0	29	54	0

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	10	0	1
SOUTHBOUND	10	0	1
EASTBOUND	10	0	1
WESTBOUND	10	0	1

PHASING N/S :4. . BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	395	533	163	0
LEFT	0	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	7	0	0	0
ADJUSTED VOL	0	0	0	0
CAPACITY	0	0	163	0
MOVEMENT	N/A	N/A	OK	OK

6-15 D

CAPACITY ANALYSIS FOR GREENWOOD LAKE TURNPIKE & MARGARET KING AV£.
INTERSECTION 15

i
v
A four lane configuration in Greenwood Lake Turnpike was assumed for the first OAA test. With the "As Zoned" scenario it indicates a Level of service B at a saturation rate of 66% during the P.M. peak hour. The "Full Development" scenario shows a Level of service D at a saturation rate of 79%. Widening Greenwood Lake Turnpike to five lanes with two lanes for southbound left turns would improve the P.M. peak hour flow for the "Full Development" scenario to a Level of service C at a saturation rate of 12%.

The morning peak hour would be less critical as can be seen from the attached calculation sheets.

f

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & MAR. KING AVE

DATE 1993 PM PEAK FULL DEVELOPMENT

.....#.....
 LEVEL OF SERVICE C
 SATURATION 72
 CRITICAL N/S VOL 760
 CRITICAL E/W VOL 481
 CRITICAL SUM 1241
#.....

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	RT. 13.0	...	R. 13.0
2	T. 12.0	L. 12.0	...	T. 12.0
3	L. 12.0
4
5
6

	NORTHBOUND	TRAFFIC VOLUMES SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	230	0	0
THRU	652	229	0	413
RIGHT	459	0	0	652

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.3
EASTBOUND	0	0	1
WESTBOUND	5	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU - RIGHT	639	240	0	481
LEFT	0	121	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	230	0	0
ADJUSTED VOL	0	232	0	0
CAPACITY	0	0	0	4ai
MOVEMENT	N/A	N/A	OK	OK

6-16 C

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP ft MAR. KING AVE

DATE 1393 AM PEAK FULL DEVELOPMENT

.....

LEVEL OF SERVICE C
 SATURATION 76
 CRITICAL N/S VOL 1053
 CRITICAL E/W VOL 254
 CRITICAL SUM 1307

LANE	NORTHBOUND		LANE GEOMETRY				WESTBOUND	
	MOV	WIDTH	SOUTHBOUND	MOV WIDTH	EASTBOUND	MOV WIDTH	MOV	WIDTH
1	RT.	13.0	RT.	13.0				13.0
2	T..	12.0	L..	12.0			T..	12.3
3
4
5
6

LEFT THRU RIGHT	NORTHBOUND		TRAFFIC VOLUMES		WESTBOUND	
			SOUTHBOUND	EASTBOUND		
	0	644	0	0	0	0
	146	477	0	0	218	218
	429	0	0	0	93	93

	TRUCKS (%)	LOCAL BUSES	<#/HR)	PEAK HOUR	FACTOR
NORTHBOUND	5		0	.3	
SOUTHBOUND	5		0	.3	
EASTBOUND	0		0	1	
WESTBOUND	5		0	.3	

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

THRU -RIGHT LEFT	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
	314	500	254	254
	0	739	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	644	0	0
ADJUSTED VOL	0	733	0	0
CAPACITY	0	0	254	254
MOVEMENT	N/A	N/A	OK	OK

6-16D

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & MAR. KING AVE

DATE 1993 AM PEAK AS ZONED

LEVEL OF SERVICE C
SATURATION 7S
CRITICAL N/S VOL 1071
CRITICAL E/W VOL 172
CRITICAL SUM 1243

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	RT. 13.0	R.. 13.0
2	T.. 12.0	L.. 12.0	T.. 12.0
3
4
5
&

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	656	0	0
THRU	136	473	0	148
RIGHT	446	0	0	82

	TRUCKS	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.3
EASTBOUND	0	0	1
WESTBOUND	5	0	.3

PHASING N/S = 4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W = 1. NEITHER TURN PROTECTED.
PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	317	496	0	172
LEFT	0	754	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	656	0	0
ADJUSTED VOL	0	754	0	0
CAPACITY	0	0	0	172
MOVEMENT	N/A	N/A	OK	OK

6-16E

CAPACITY ANALYSIS FOR MARGARET KING AVENUE & THE STERLING FOREST TRACT

INTERSECTIONS 16 & 17

Two roadways were included in the computer traffic tableau to provide access for the Sterling Forest Tract. One was labeled Sterling Forest Commercial and the other Sterling Forest Residential. Both intersections were tested individually with the unsignal ized intersection capacity program. The results can be looked at individually or collectively.

The test for the "As Zoned" scenario in the 1993 A.M. peak i hour shows Levels of service A at both Intersections 16 and 17 for traffic turning left into the site and turning right out of the site* However, the tests show a Level of service E at Intersection 16 and a Level of service F at Intersection 17 for left turns exiting the site. Collectively the capacity of the left turn exit is 30 vehicles less than the demand. With the "Full Development" scenario the capacity for the left turn exit is exceeded by 140 vehicles.

During the P.M. peak hour conditions would be worse. Collectively the capacity for left turn exits from the site would be exceeded by 166 vehicles with the "As Zoned" scenario and 384 vehicles with the "Full Development" scenar io.

Clearly, the two unsignal ized intersections of site roadways forming Intersections 16 & 17 would be inadequate for site access .

Unsignalized "T" Int Cap Calc Intersection 16
 Location Margaret King Ave. & Sterling Forrest Commercial
 Count Data: Zone development of sites included in the study
 Date 1993
 Day Weekday

AM or PM Analysis?	AM				
Hourly Demand Volumes:			Table 2A		
A Through	199	180	5		
A Right	50	240	6		
B Left	154	330	6		
B Through	987	360	5		
C Left	60	440	7		
C Right	61	480	6		
		660	6		
		880	7		
RIGHT TURN FROM C					
Conflicting Flows=	229				
Major road lanes (2 or 4)	2				
Major road spd (30 or 55)	30				
Control (stop=4, Yld=3)	4				
Critical Gap Table 2 T=	6				
Capacity, from fig 2=	775				
Shared Lane-go to L.T.					
			Table 3		Figure 3
-----		-800	6	0	1
No shared Lane-Y=1,N=0	1	0	5	5	.97
Demand<C right)=	61	100	4	10	.93
Available Reserve=	714	200	3	15	.99
Delay * L.O.S. Table 3=	1	300	2	20	.35
<A=1,B=2,C=3,D=4,E=5,F=6>		400	1	25	.31
		10000	0	30	.77
				35	.69
"LEFT"TURN"FROM"B				40	.64
Conflicting Flows=	269		Table 2B	45	.6
Major road lanes(2 or 4)	2	60	5	50	.55
Major road spd(30 or 55)	30	110	5.5	55	.5
Critical Gap Table 2 T=	5	120	5.5	60	.45
Capacity, from fig 2=	920	220	6	65	.39
Demand(B left)=	154			70	.33
Capacity used <in %>=	16.73913		Table 2C	75	.27
Impedance factor, fig 3=	.89	ISO	6.5	80	.2
Available reserve ³	766	240	7.5	85	.14
Delay Z< L.O.S. Table 3=	1	330	8	90	.08
(A=1,B=2,C=3,D=4,E=5,F=6)		360	7	95	0
		44-0	9	100	

LEFT~fuRN~FROM~C		480	3		
Conflicting Flows=	1370	660	9		
Major road lanes(2 or 4)	2	880	10		
Major road spd(30 or 55)	30				
Control (stop=4, Yld=3)	4				
Critical Gap Table 2 T=	7.5				
Capacity, from fig 2=	80				
Adjustment for Impedance=	77.0696				
-No Shared Lane,Y=1,N=0	1				
Demand=	60				
Available Reserve"	17.0696				
Delay ?< L.O.S. Table 3=	5				
<A=1,B=2,C=3,D=4,E=5,F=6)					

6-17 A

Unsignalized "T" Int Cap Calc Intersection 17
 Location Margaret King Ave. 3< Sterling Forrest residential
 Count Data? Zone development of sites included in the study

Date 1993
 Day Weekday

AM or PM Analysis? AM
 Hourly Demand Volumes:
 A Through 215
 A Right 101
 B Left 88
 B Through 960
 C Left 135
 C Right 55

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

RIGHT TURN FROM C
 Conflicting Flows** 265.5
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop«4, Yld»3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2^a 740
 Shared Lane-go to L.T.

No-shared-lane-y»77N«0 1
 Demand(C right)• 55
 Available Reserve* 685
 Delay «e L.Q.S. Table 3- (A«1,B«2,C«3,D«4,E«5,F«6) 1

Table 3

-800	6
0	5
100	4
200	Y
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.39
20	.35
25	.31
30	.77
35	.7^A
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.ZZ'
80	.27
85	, 2
90	.14
95	.08
100	0

LEFT TURN FROM B
 Conflicting Flows" 316
 Major road lanes(2 or 4) ~
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T= 5
 Capacity, from fig 2^s 880
 Demand<B left)" 88
 Capacity used (in 5i)» 10
 Impedance factor, fig 3^s .93
 Available reserve** 792
 Delay & L.O.S. Table 3- (A=1,B*2,C«3,D»4,E-5,F-6> 1

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

130	6.5
240	7.5
330	3
360	7
44.0	9
480	8
660	9
880	10

LEFT TURN FROM C
 Conflicting Flows= 1313.5
 Major road lanes(2 or 4) ~
 Major road spd(30 or 55) 10
 Control (stop»4, Yld»3) 4
 Critical Sap Table 2 T= 7.5
 Capacity, from fig 2= 90
 Adjustment for Impedance** 37.9021

-No Shared Lane, Y»1, N»0 1
 Demand³ 135
 Available Reserve- -47.0979
 Delay ?« L.O.S. Table 3=* 6
 (A»1, B=2, C»3, D»4, E=5, F=6)

Unsignalized "T" Int Cap Calc Intersection 16
 Location Margaret KingAve. & Sterling Forrest Commercial
 Count Data: Full development of sites included in the study

Date 1993
 Day Weekday

AM~or~PM AnaFysTs? AM

Hourly Demand Volumes:

A Through 242
 A Right 99
 B Left 172
 B Through 941
 C Left 91
 C Right 89

Table 2A
 180 5
 240 6
 330 6
 360 5
 440 7
 480 6
 660 6
 880 7

RIGHT TURN FROM C
 Conflicting Flows= 291.5
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control <stop=4, Yld=3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2= 705
 Shared Lane-go to L.T.

 No shared lane-Y=1,N=0 1
 Demand(C right)= 89
 Available Reserve* 616
 Delay & L.O.S. Table 3= 1
 (A=1.B=2,C=3,D=4,E=5,F=6)

Table 3
 -800 6 0
 0 5 1
 100 4 10 .93
 200 3 15 .89
 300 2 20 .85
 400 1 25 .81
 10000 0 30 .77

 LEFT~TURN"FROM~i
 Conflicting Flows= 341
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T= 5
 Capacity, from fig 2= 850
 Demand<B left)= 172
 Capacity used (in %)= 20.23529
 Impedance factor, fig 3= .85
 Available reserve* 678
 Delay ?< L.O.S. Table 3= 1
 (A=1.B=2.C=3.D=4,E=5.F=6)

Table 2B
 60 5 45 .64
 110 5.5 50 .6
 120 5.5 55 .55
 220 6 60 .5
 65 .45
 70 .39
 Table 2C
 180 6.5 75 .33
 240 7.5 80 .27
 330 8 35 .2
 360 7 90 .14
 440 9 95 .08
 480 8 100 0

 "LEFT"TURN"FROM~C
 Conflicting Flows= 1404.5
 Major road lanes<2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T= 7.5
 Capacity, from fig 2= 75
 Adjustment for Impedance³ 71.25375

 -No Shared Lane,Y=1,N=0 I
 Demand³ 91
 Available Reserve⁰ -19.7463
 Delay ?< L.O.S. Table 3= 6
 (A=1,B=2.C=3,D=4,E=5,F=6)

Unsignalized "T" Int Cap Calc

Intersection 17

Location Margaret King Ave. & Sterling Forrest Residential

Count Data: Full development of sites included in the study

Date 1993

Day Weekday

All or PFI Analysis? All

Hourly Demand Volumes:

A Through	271
A Right	111
B Left	99
B Through	933
C Left	198
C Right	71

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
380	7

RIGHT TURN FROM C

Conflicting Flows*	326.5
Major road lanes (2 or 4)	2
Major road spd (30 or 55)	30
Control (stop*4, Yld*3)	4
Critical Gap Table 2 T=	6
Capacity, from fig 2 ^s	680
Shared Lane-go to L.T.	

No shared lane-Y<1,N-0	1
Demand(C right)*	71
Available Reserve*	609
Delay & L.O.S. Table 3=	1
<A*1,B-2,C<3,D>4,E*5,F*6)	

Table 3

-800	6
O	5
100	4
200	2
300	1
400	0
10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.31
30	.77
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

LEFT TURN FROM B

Conflicting Flows*	382
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Critical Gap Table 2 T=	5
Capacity, from fig 2=	805
Demand(B left)-	*?*
Capacity used (in %)=	12.29814
Impedance factor, fig 3*	.93
Available reserve*	706
Delay & L.O.S. Table 3*	1
(A*1.B*2.C*3,D*4,E-5,F*6)	

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	8
360	.j
440	o
480	8
660	o
880	10

LEFT TURN FROM C

Conflicting Flows*	1358.5
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Control (stop*4, Yld*3)	4
Critical Gap Table 2 T*	7.5
Capacity, -from fig 2 ^s *	80
Adjustment for Impedance*	78.1352

-No Shared Lane,Y=1,N*0	1
Demand*	198
Available Reserve*	-119.865
Delay * L.O.S. Table 3*	6
(A*1.8*2.C*3,D*4.E*5.F*6)	

Unsignalized "T" Int Cap Calc Intersection 16
 Location Margaret King Ave. & Sterling Forrest Commercial
 Count Data: Zone development of sites included in the study

Date 1.993
 Day Weekday

AM or PM Analysis? PM

Hourly Demand Volumes:

A Through	361
A Right	78
B Left	86
B Through	377
C Left	138
C Right	130

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
380	7

RIGHT TURN FROM C
 Conflicting Flows= 900
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T= 6
 Capacity, -from fig 2= 310
 Shared Lane-go to L.T.

No shared lane-Y=1,N=0 1
 Demand(C right)= 130
 Available Reserve* 180
 Delay & L.O.S. Table 3= 4
 <A=1,B=2,C=3,D=4,E=5,F=6)

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.81
30	.77
40	.72
45	.69
50	.64
55	.6
60	.55
65	.5
70	.45
75	.39
80	.33
85	.27
90	.2
95	.14
100	.08
	0

LEFT TURN FROM B

Conflicting Flows* 93?
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T= 5
 Capacity, from fig 2= 440
 Demand(B left)= 86
 CaDacity used (in %)= 19.54545
 Impedance factor, fig 3= .39
 Available reserve* 354
 Delay ?< L.O.S. Table 3= 2
 (A=1,B=2,C=3,D=4,E=5,F=6)

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	8
360	7
440	9
480	8
660	9
880	10

LEFT TURN~FROM C
 Conflicting Flows* 1363
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T= 7.5
 Capacity, from fig 2= 50
 Adjustment for Impedance⁸ 77.0696
 -No Shared Lane,Y=1,N=0 1
 Demand= 138
 Available Reserve* -60.9304
 Delay ?< L.O.S. Table 3= " 6
 (A=1,B=2,C=3,D=4,E=5,F=6)

V

Unsignalized "T" Int Cap Calc Intersection 17
 Location Margaret King Ave. St Sterling Forrest residential

Date 1993
 Day Weekday.

AM or PM Analysis? PM
 Hourly Demand Volumes:
 A Through 313
 A Right 82
 B Left 120
 B Through 396
 C Left 180
 C Right 126
 RIGHT TURN FROM C
 Conflicting Flows- 854
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop<4. Yld-3) 4
 Critical Gap Table 2 T- 6
 Capacity, from fig 2- 340
 Shared Lane-go to L.T.

 No-shared*lane-Y-T.N<<0 1
 Demand(C right)- 126
 Available Reserve- 214
 Delay & L.O.S. Table 3= 3
 (A-1.B-2,C<3,D-4,E-5,F-6)

 LiFT~TURN*"FROM~i
 Conflicting Flows- 895
 Major road lanes(2 or 4) 2
 Major road sod(30 or 55) 30
 Critical Gap Table 2 T- 5
 Capacity, from fig 2- 450
 Demand(B left)- 120
 Capacity used (in %)= 26.66667
 Impedance factor, fig 3- .31
 Available reserve- 330
 Delay & L.O.S. Table 3- 2
 (A-1.B-2.C-3.D-4.E-5.F-6)

 LEFFTURN' FROFrC
 Conflicting Flows- 1370
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop-4. Yld-3> 4
 Critical Gap Table 2 T= 7.5
 Capacity, from fig 2= 80
 Adjustment for Impedance- 74.9384

 -No Shared Lane.Y-1,N-O 1
 Demand- 180
 Available Reserve* -105.062
 Delay & L.O.S. Table 3- 6
 (A=1,B-2.C=3.D=4,E=5,F-6)

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

Table 3

-800	6	0	1
O	5	5	.97
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77
		35	.72
		40	.69

Table 2B

60	5	45	.64
110	3.5	50	.6
120	5.5	55	.55
220	6	60	.5
		65	.45
		70	.39

Table 2C

180	6.5	75	.33
240	7.5	90	.27
330	9	85	.2
36.0	7	90	.14
440	9	95	.08
480	3	100	0
660	9		
880	10		

6-17-15

I

Unsignalred "T" Int Cap Calc Intersection 16
 Location Margaret King Ave. & Sterling Forrest Commercial

"*" Count Data! Full development of sites included in the study

Date 1993

Day Weekday

~AM~or~PM~AnaTysis? PM

Hourly Demand Volumes:

Table 2A

A Through	864	180	5
A Right	124	240	6
B Left	155	330	6
B Through	534	360	5
C Left	220	440	7
C Right	201	480	6
		660	6
		880	7

RIGHT TURN FROM C

Conflicting Flows-

926

Major road lanes (2 or 4)

2

Major road spd (30 or 55)

30

Control <stop=4, Yld=3>

4

Critical Gap Table 2 T=

6

Capacity, from fig 2=

300

Shared Lane-go to L.T.

Table 3

Figure 3

		-800	6	0	1
No shared lane-Y=1,N=0	1	0	5	5	.97
Demand(C right)=	201	100	4	10	.93
Available Reserve=	99	200	3	15	.89
Delay Sc L.O.S. Table 3=	5	300	2	20	.85
<A=1.B=2.C=3.D=4.E=5.F=6>		400	1	25	.81
		10000	0	30	.77

LEFT TURN~FROM B

Conflicting Flows-

988

Major road lanes(2 or 4)

2

Major road spd (30 or 55)

30

Critical Gap Table 2 T=

5

Capacity, from fig 2=

400

Demand(B left)-

155

Capacity used (in %)=

38.75

Impedance factor, fig 3=

.72

Available reserve-

245

Delay 2< L.O.S. Table 3=

3

<A=1.B=2.C=3.D=4.E=5.F=6>

LEFT TURN FROM C

Conflicting Flows-

1615

Major road lanes(2 or 4)

2

Major road spd(30 or 55)

30

Control (stop=4, Yld=3)

4

Critical Gap Table 2 T=

7.5

Capacity, from fig 2=

50

Adjustment for Impedance-

45.338

-No Shared Lane.Y=1,N=0

1

Demand-

220

Available Reserve-

-174.662

Delay ?< L.O.S. Table 3=

6

(A=1.B=2.C=3.D=4.E=5.F=6)

Unsignalised "T" Int Cap Calc Intersection 17
Location Margarat King Ave. * Sterling Forrest Residential
Count Data Full development of sites included in the study

Data 1993
Day Weekday
AM or PH Analysis? PM

Hourly Demand Volumes:

A Through	855	ISO	5
A Right	165	240	6
B Left	195	330	6
B Through	559	360	5
C Left	253	440	7
C Right	132	480	6
		660	6
		880	7

Table 2A

RIGHT TURN FROM C
Conflicting Flows" 937.5
Major road lanes (2 or 4) 2
Major road spd (30 or 55) 30
Control (»top»4, Yld»3) 4
Critical Gap Table 2 T=
Capacity, from fig 2^s 295
Shared Lane-go to L.T.

Nctshared"1ane^Y»77N=O 1
Demand(C right)= 132
Available Reserve" 163
Delay & L.O.S. Table 3» 4
(A«1,B«2,C«3,D«4,E*5,F»6)

LEFT"*TURN~FROM~I
Conflicting Flows* 1020
Major road lanes(2 or 4) 2
Major road spd(30 or 55) 30
Critical Gap Table 2 T* 5
Capacity, from fig 2= 380
Demand (B left)** 195
Capacity used (in *C» 51.31579
Impedance factor, fig 3= .6
Available reserve** 185
Delay Sc L.O.S. Table 3= 4
(A=1,B«2,C»3,D»4,E-5,F-6)

LEFT TURN FROM C
Conflicting Flows= 1691.5
Major road lanes(2 or 4) 2
Major road spd(30 or 55) 30
Control (stop»4, Yld*3) 4
Critical Sap Table 2 T= 7.5
Capacity, from fig 2= 50
Adjustment for Impedance= 43.34

-No Shared Lane,Y=1.N»0 1
Demand* 253
Available Reserve* -209.66
Delay ?< L.O.S. Table 3= 6
(A=1,B=2,C=5,0=4,E=5.F=6)

Table 3		Figure 3	
-800	6	0	1
O	5	5	.97
100	4	10	.93
200	3	15	.8?
300	2	20	.85
400	1	25	.81
10000	O	30	.77
		35	.7^1
		40	.69
Table 2B			
60	5	45	.64
110	5.5	50	.6
120	5.5	55	.55
220	6	60	.5
		65	.45
		70	.39
Table 2C			
180	6.5	75	.37
240	7.5	80	.27
330	8	85	.2
360	7	90	.14
440	9	95	.08
480	8	100	0
660	9		
880	10		

**CAPACITY ANALYSIS FOR MARGARET KING AVENUE & SITE 6 -
INTERSECTION 18**

The unsignal ized intersection capacity analysis for the 1993 AM* peak hour shows a Level of service A for traffic making left turns into the site and traffic making right turns from the site for both the "As Zoned" and "Full Development" scenarios, and a Level of service E for left turns exiting the site. The left turn exit for the "As Zoned" scenario used 19 of the 80 vehicle capacity while in the "Full Development" scenario 36 of the 59 vehicle capacity is used. Thus while there will be long delays for left turn exits from Site 6 for both scenarios, the delays in "Full Development" scenario would be significantly greater.

During the 1993 P.M. peak hour the only similarity between the two scenarios would be the left turn entering the site which would be a Level of service A in both cases. The right turn exit from the site would be a Level of service C for the "As Zoned" scenario and a Level of service D for the "Full Development" scenario. The left turn exit from the site would be a Level of service E using 41 of the 75 vehicle capacity for the "As Zoned" scenario while for the "Full Development" scenario the demand for left turns from the site would exceed the capacity by 151 vehicles.

Unsignalized "T" Int Cap Calc Intersection 18
 Location: Margaret King Ave. & B601L12 & 13 Site 6
 Count Data: Zone development of sites included in the study

D<t<----- 1993
 D*V----- Weekday
 All or PM Analysis? AM

Hourly Demand Volumes:

A Through	305
A Right	28
B Left	25
B Through	1070
C Left	19
C Right	10

Table 2A

iao	5
240	6
330	6
360	5
440	7
480	6
660	6
830	7

RTRM TURN FROM R

Conflicting Flows*	319
Major road lanes (2 or 4)	2
Major road spd (30 or 55)	30
Control (stop*4, Yld*3)	4
Critical Gap Table 2 T*	6
Capacity, from fig 2 ^s	680
Shared Lane-go to L. T.	

NoTMshared lane-Y*77N-O

Demand(C right)*	10
Available Reserve*	670
Delay & L.O.S. Table 3*	1
(A*1,B<2,C>3,D-4,E<5,F*<b)	

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.39
20	.85
25	.31
30	.77
35	.72
40	.69

LEFT TURN FROM B

Conflicting Flows*	333
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Critical Gap Table 2 T*	5
Capacity, from fig 2=	860
Demand<8 left)*	25
Capacity used (in '/.)»	2.906977
Impedance factor, fig 3*	1
Available reserve*	835
Delay & L.O.S. Table 3*	1
(A*UB>2.C*3,D-4,E-5,F*6)	

Table 2B

60	5
NO	5.5
120	5.5
220	6

45	.64
50	.6
55	.59
60	.5
65	.43
70	.39
75	.33
80	.27
85	.22
90	.14
95	.08
100	0

LEFT TURN FROM C

Conflicting Flows*	1414
Major road lanes<2 or 4)	-
Major road spd(30 or 55)	30
Control (stop-4, Yld*3)	4
Critical Gap Table 2 T=	7.5
Capacity, from fig 2 ^s	80
Adjustment for Impedance*	80

Table 2C

180	6.5
240	7.5
330	8
360	7
440	9
480	8
660	9
880	10

-No Shared Lane,Y*1,N*0

Demand*	19
Available Reserve*	61
Delay ?< L.O.S. Table 3*	5
(A>1,B=2.C*3,D=4,E=5,F=6)	

r

Unsignalized "T" Int Cap Calc Intersection 13
 Location Margaret King Ave. ?< B601L12 & 13
 Count Data: Full development of sites included in the study
 Date 1993
 Day Weekday
 AM or PM Analysis? AM

Hourly Demand Volumes:
 A Through 360
 A Right 129
 B Left 104
 B Through 1026
 C Left 36
 C Right 22
 RIGHT TURN FROM C
 Conflicting Flows- 424.5
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Sap Table 2 T= 6
 Capacity, from fig 2= 595
 Shared Lane-go to L.T.

Table 2A

ISO	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

 ~No shared~7ane-Y=77N=0 1
 Demand(C right)- 22
 Available Reserve= 573
 Delay .* L.d.S. Table 3= 1
 (A=1,B=2,C=3,D=4,E=5,F=6)

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.99
20	.95
25	.81
30	.72

 LEFT TURN FROM B
 Conflicting Flows- 489
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T= 5
 Capacity, from fig 2= 720
 Demand(B left)- 104
 Capacity used (in %)= 14.44444
 Impedance factor, fig 3= .93
 Available reserve- 616
 Delay 2< L.O.S. Table 3= 1
 (A=1,B=2,C=3,D=4,E=5,F=6)

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	3
360	7
440	9
480	8
660	9
880	10

40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

 LEFT TURN FROM C
 Conflicting Flows- 1554.5
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T= 7.5
 Capacity, from fig 2= 60
 Adjustment for Impedance- 58.6014

-No Shared Lane, Y=1, N=0 1
 Demand- 36
 Available Reserve- 22.6014
 Delay *< L.O.S. Table 3= 5
 (A=1,B=2,C=3,D=4,E=5,F=6)

Unsignalized "T" Int Cap Calc Intersection IS
 Location Margaret King Ave. !< B601L12 & 13 Site 6
 Count Data: Zone development of sites included in the study

Date 1993
 Day Weekday

AM or PM Analysis? PM
 Hourly Demand Volumes:
 A Through 865
 A Right 18
 B Left 15
 B Through 560
 C Left 41
 C Right 30

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
380	7

RIGHT TURN FROM C
 Conflicting Flows" 874
 Major road lanes <2 or 4)
 Major road spd (30 or 55) 30
 Control <stop«4. Yld»3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2^s 320
 Shared Lane-go to L.T.

Table 3

-800	6	Figure 1	0	1
(j)	5		5	.97
100	4		10	.93
200	3		15	.89
300	2		20	.85
400	1		25	.81
10000	0		30	.77
			35	.72
			40	.69
			45	.64
			50	.6
			55	.55
			60	.5
			65	.45
			70	.39
			75	.33
			80	.*27
			85	.2->
			90	.14
			95	.08
			100	0

Table 2B

60	5
110	5.5
120	5.5
220	6

Table 2C

180	6.5
240	7.5
330	8
360	7
440	9
480	8
660	9
880	10

No shared Lane-Y-ITN-O 1
 Demand(C right)= 30
 Available Reserve" 290
 Delay k L.O.S. Table 3= 3
 (A-1.B»2.C*3,D»4.E»5.F»6)

LEFT TURN FROM B
 Conflicting Flows= 883
 Major road lanes(2 or 4) 2
 Major road sod(30 or 55) 30
 Critical Gap Table 2 T= 8
 Capacity, from fig 2= 460
 Demand(B left)» 15
 Capacity used (in '/.)= 3.260870
 Impedance factor, fig 3= 1
 Available reserve" 445
 Delay St L.O.S. Table 3» 1
 (A-t,B»2,C»3,D»4.E»3.F=6»

LEFT-TURN-FROM-C
 Conflicting Flows= 1449
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop-4, Yld»3) 4
 Critical Gap Table 2 T= 7.5
 Capacity, from fig 2= 75
 Adjustment for Impedance*³ 75

-No Shared Lane.Y»1,N»0 1
 Demand⁹ 41
 Available Reserve⁸ 34
 Delay it L.O.S. Table 3= 5
 (A"t.B=2.C=3,D=4.E=5.F=6)

f

Unsignalised "T" Int Cap Calc	Intersection IS	
Location	Margaret King Ave. i< B601L12 & 13 Site 6	
	Count Data: Full development of sites included in the study	
Date	1993	
Day	Weekday	
	AM~or~PM~Anaysrs?	PM
Hourly Demand Volumes:		Table 2A
A Through	886	180 5
A Right	43	240 6
B Left	33	330 6
B Through	774	360 5
C Left	176	440 7
C Right	135	480 6
		660 6
		880 7
RIGHT TURN FROM C		
Conflicting Flows=	907.5	
Major road lanes (2 or 4)	2	
Major road spd (30 or 55)	30	
Control <stop=4, Yld*3>	4	
Critical Gap Table 2 T=	6	
Capacity, from fig 2=	305	
Shared Lane-go to L.T.		
-----k-----		Table 3
No shared 7ane-Y=1,N=0	1	-800 6
Demand(C right)=	135	0 5
Available Reserve*	170	100 4
Delay ?< L.Q.S. Table 3=	4	200 3
(A=1,B=2,C=3,D=4,f=5,F=6)		300 2
		400 1
		10000 0

LIFT TURN~FROM~B		
Conflicting Flows*	929	
Major road lanes(2 or 4)	2	Table 2B
Major road spd(30 or 55)	30	60 5
Critical Gap Table 2 T>	5	110 5.5
Capacity, from fig 2=	440	120 5.5
Demand(B left)*	38	220 6
Capacity used (in %)=	8.636364	
Impedance factor, fig 3=	.97	Table 2C
Available reserve*	402	180 6.5
Delay ?< L.O.S. Table 3=	1	240 7.5
(A=1,B=2,C=3,D=4,E=5,F=6)		330 8
		360 7
		440 9
		480 8
		660 9
		880 10
LEFT"TURN~FROM~C		
Conflicting Flows*	1719.5	
Major road lanes(2 or 4)	2	
Major road spd(30 or 55)	30	
Control (stop=4, Yld=3>	4	
Critical Gap Table 2 T*	7.5	
Capacity, from fig 2*	25	
Adjustment for Impedance*	24.75025	
-No Shared Lane,Y=1,N=0	1	
Demand*	176	
Available Reserve*	-151.250	
Delay S< L.O.S. Table 3=	6	
(A=1,B=2,C=3,D=4,E=5,F=6)		

Figure 3

0	1
5	.97
10	.93
15	.39
20	.85
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.37
80	.27
85	.2
90	.14
95	.08
100	0

CAPACITY ANALYSIS FOR MARGARET KING AVENUE & SITE 7 -
INTERSECTION 19

The "As Zoned" and "Full Development" scenarios are quite different as industrial development is used in the former and mobile homes in the latter. In the 1993 A.M. peak hour the unsignalized intersection capacity analysis shows C Level of service C for right turns from the site, D for left turns into the site, and E for left turns from the site for the "As Zoned" scenario, where 19 of the 51 vehicle capacity is used by left turns exiting the site. With the "Full Development" scenario the Levels of service would be E for the right turn exit, 3 for the left turn entry movement, and E using 50 of the 54 vehicle available capacity for the left turn exit.

During the 1993 P.Af. peak hour the "As Zoned" scenario would have a Level of service D for right turns exiting the site, A for vehicles turning left into the site, and F for the left turn exiting the site with the capacity exceeded by 65 vehicles. With the "Full Development" scenario the Levels of service would be D for the right turn exit, B for the left turn entry, and E for the left turn exit with 20 of the 23 vehicle capacity used.

f

Unsignalized "T" Int Cap Calc Intersection 19
 Location Margaret King Ave. ?< B508L2 Site 7
 Count Data: Zone development of sites included in the study

Date 1993
 Day Weekday

AM-or PM Analysis? AM
 Hourly Demand Volumes:

A Through	906
A Right	182
B Left	202
B Through	315
C Left	19
C Right	44

Table 2A

ISO	5
240	6
330	6
360	5
440	7
480	6
660	6
380	7

RIGHT TURN FROM C
 Conflicting Flows* 997
 Major road lanes <2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T=
 Capacity, from fig 2=
 Shared Lane-go to L.T. 275

 No shared Lane-Y=1,N=0 1
 Demand(C right)= 44
 Available Reserve* 231
 Delay * L.Q.S. Table 3= 3
 (A=1,B=2.C*3,D=4,E=5,F=6)

Table 3

-800	6
0	5
100	4
200	3
300	2
400	1
10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

LEFT TURN FROM B
 Conflicting Flows* 1088
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Critical Gap Table 2 T=
 Capacity, from fig 2=
 Demand(B left)* 202
 Capacity used (in 7.)= 56.11111
 Impedance factor, fig 3=
 Available reserve* 158
 Delay Z< L.O.S. Table 3=
 (A=1.B=2.C=3,D=4,E=5,F=6)

Table 2B

60	5
HO	5<5
120	5.5
220	6

Table 2C^

180	6.5
240	7.5
330	3
360	7
440	9
480	3
660	9
880	10

LEFT~TURN~FROM~C
 Conflicting Flows* 1514
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control <stop=4, Yld=3) 4
 Critical Gap Table 2 T=
 Capacity, from fig 2=
 Adjustment for Impedance* 51.009
 -No Shared Lane,Y=1.N=0 1
 Demand* 19
 Available Reserve* 32.009
 Delay !< L.D.S. Table 3=
 (A=1.B=2.C=3,D=»4,E=5,F=6> 5

G-19A

Unsignalised ^HT^M Int Cap Calc Intersection 19
 Location Margaret King Ave. * B508L2 Site 7
 Count Data; Full development of sites included in the study

Date 1993
 Day Weekday
 AM-or-PM Analysis? AM

Hourly Demand Volumes:
 A Through 1021
 A Right 42
 B Left 53
 B Through 439
 C Left 50
 C Right 228

Table 2A

180	5
240	6
330	6
360	7
440	7
480	6
660	6
880	7

RIGHT TURN FROM C
 Conflicting Flows³ 1042
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control <stop>4. Yld>3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2= 260
 Shared Lane-go to L.T.

Table 3

-800	5	0	1
0	5	5	.97
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77

Figure 3

40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.34
80	.27
85	.2
90	.14
95	.08
100	0

No shared lane-Y=1.N=0 1
 Demand(C right)³ 228
 Available Reserve* 2
 Delay & L.O.S. Table 3= 5
 (A>1.B<2.C-3.D-4.E>5.F*6)

Table 2B

60	5
UO	5.5
120	5.5
220	5

Table 2C

180	6.5
240	7.5
330	9
360	7
440	9
480	8
660	9
880	10

LEFT TURN FROM 8
 Conflicting Flows- 1063
 Major road lanes(2 or 4) 2
 Major road sod(30 or 55) 30
 Critical Gao Table 2 T= 5
 Capacity, from fig 2= 375
 Demand(B left)= 53
 Capacity used (in'/.)= 14.13ZZZ
 Impedance factor, fig 3=> .93
 Available reserve³* 222
 Delay & L.O.S. Table 3= 2
 <A=t.8<2.C-3,D>4.E<5.F>6>

LEFT TURN FROM C
 Conflicting Flows* 1534
 Major road lanes(2 or 4) 2
 Major road spd(30 or 55) 30
 Control (stop*4, Yld=3) 4
 Critical Gap Table 2 T* 7.5
 Capacity, from fig 2= 55
 Adjustment for Impedance* 53.71795

-No Shared Lane.Y=1.N*0 1
 Demand³ 50
 Available Reserve* 3.71795
 Delay !< L.O.S. Table 3= 2
 (A=1.B*2.C*3,D>4.E=5,F=6J)

6-19 B

Unsignalised "T" Int Cap Calc Intersection 19
 Location _____; Margaret King Ave. & B508L2 Site 7
 Count Data: Zone development of sites included in the study
 Date _____ 1993
 Day _____ Weekday

AM or PM Analysis?	PM		
Hourly Demand Volumes:		Table 2A	
A Through	556	180	5
A Right	46	240	6
B Left	50	330	6
B Through	739	360	5
C Left	144	440	7
C Right	336	480	6
		660	6
		880	7

RIGHT TURN FROM C
 Conflicting Flows* 579
 Major road lanes (2 or 4) 2
 Major road spd (30 or 55) 30
 Control (stop=4, Yld=3) 4
 Critical Gap Table 2 T= 6
 Capacity, from fig 2= 485
 Shared Lane-go to L.T.

		Table 3	
-----		-800	6
No shared lane-Y*7,N=0	1	0	5
Demand(C right)*	336	100	4
Available Reserve*	149	200	3
Delav & L.O.S. Table 3=	4	300	2
<A=1.B=2,C=3,D=4,E=5,F=6>		400	1
		10000	0

Figure 3

0	1
5	.97
10	.93
15	.89
20	.85
25	.81
30	.77
35	.72
40	.69
45	.64
50	.6
55	.55
60	.5
65	.45
70	.39
75	.33
80	.27
85	.2
90	.14
95	.08
100	0

LEFT TURN~FROM B			
Conflicting Flows*	602		
Major road lanes(2 or 4)	2	60	5
Major road sod(30 or 55)	30	110	5.5
Critical Gao Table 2 T=	5	120	5.5
Capacity, from fig 2=	640	220	6
Demand(B left)=	50		
Capacity used (in %)=	7.8125		

		Table 2C	
Impedance factor, fig 3=	.97	180	6.5
Available reserve*	590	240	7.5
Delay ?< L.O.S. Table 3*	1	330	8
(A=1.B=2,C=3,D=4,E=5,F=6)		360	7
		440	9

LEFT TURN~FROM C			
Conflicting Flows*	1368	490	8
Major road lanes(2 or 4)	2	660	9
Major road spd(30 or 55)	30	880	10
Control (stop=4, Yld=3)	4		
Critical Gap Table 2 T=	7.5		
Capacity, from fig 2=	80		
Adjustment for Impedance*	79.2008		

-No Shared Lane.Y=1,N*0 1
 Demand* 144
 Available Reserve* -64.7992
 Delav ?< L.O.S. Table 3* 6
 (A=i,B=2,C=Z,D=4.E=5,F=6>

Unsignalized "T^H Int Cap Calc Intersection 1?
 Location _____ Maraaret Kino Ave. * B508L2 Site 7
 Count Data Full development of sites included in the study

Date _____ 1993

Day _____ Weekday

AM or PM Analysis? PM

Hourly Demand Volumes:

A Through	857
A Right	92
B Left	120
B Through	909
C Left	20
C Right	112

Table 2A

180	5
240	6
330	6
360	5
440	7
480	6
660	6
880	7

RIGHT TURN FROM C

Conflicting Flows-	903
Major road lanes (2 or 4)	2
Major road spd (30 or 55)	30
Control <stop-4, Yld-3)	4
Critical Gap Table 2 T»	6
Capacity, from fig 2-	310
Shared Lane-go to L.T.	

Table 3		Figure 3	
-800	6	0	1
0	5	5	.97
100	4	10	.93
200	3	15	.89
300	2	20	.85
400	1	25	.81
10000	0	30	.77
		35	.72
		40	.69

No-shared" Tane-Y»T7N-0	1
Demand(C right)«	112
Available Reserve"	198
Delay & L.O.S. Table 3=	4
(A-1,B-2,C»3,D-4,E»5,F»6>	

LiFT-TURN-FROM-i

Conflicting Flows-	949
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Critical Gao Table 2 T-	5
Capacity, from fig 2=	430
Demand(B left)-	120
Caoacity used (in %).»	27.90698
Impedance factor, fig 3»	.81
Available reserve-	310
Delay Si L.O.S. Table 3=	2
(A-1,B-2,C-3,D-4,E-5,F-6)	

Table 2B

60	5	45	.64
110	5.5	50	.6
120	5.5	55	.55
220	6	60	.5
		65	.45
		70	.39
		75	.33
		30	.27
		85	.2
		90	.14
		95	.08
		100	0

Table 2C

180	6.5	75	.33
240	7.5	30	.27
330	8	85	.2
360	7	90	.14
440	6	95	.08
480	8	100	0
660	9		
880	10		

LEFT TURN FROM C

Conflicting Flows-	1932
Major road lanes(2 or 4)	2
Major road spd(30 or 55)	30
Control (stop-4, Yld=3)	4
Critical Gap Table 2 T=	7.5
Capacity, from fig 2=	25
Adjustment for Impedance-	23.41825

-No Shared Lane,Y=1,N«0	1
Demand=	20
Available Reserve"	3.41825
Delay «e L.O.S. Table 3=	5
CA«1.B»»2.C=3,D»4,E=5,F=6)	

CAPACITY ANALYSIS FOR SLOATSBURG ROAD & MARGARET KING AVENUE -
INTERSECTION 21

The first tests for this intersection were done with all approaches three lanes wide. During the 1993 A.M. peak hour the CMA analysis shows a Level of service D at 83% saturation for the "As Zoned" scenario and Level of service D at 87% saturation for the "Full Development" scenario. Perusal of the CRITICAL LANE VOLUMES BY MOVEMENT section on the attached sheets shows that the most to be gained would be by having two eastbound lanes to turn left instead of one. To accomplish this there must be two lanes plus widening for the turning movement in the northbound exit lanes .

To accommodate the two eastbound left turn lanes the second CMA tests assumed Sloatsburg Road to be five lanes wide at the intersection. Then the CMA analysis for the 1993 A.M. peak hour indicates a Level of service A for both scenarios. During the P.M. peak hour the CMA shows a Level of service A at a saturation rate of 54% for the "As Zoned" scenario and a Level of service C at a saturation rate of 70% for the "Full Development" scenario.

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SLOATSBURG RD & MAR. KING AVE

DATE 1993 AM PEAK AS ZONED

```

  .....».....*.....
  LEVEL OF SERVICE D
  SATURATION 83
  CRITICAL N/S VOL 609
  CRITICAL E/U VOL 824
  CRITICAL SUM 1433
  .....+.....».....*.....-».....*.....+
  
```

LANE	LANE GEOMETRY							
	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	T..	14.0	RT.	14.0	R..	13.0
2	L..	12.0	T..	12.0
3
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	287	0	0	0
THRU	492	63	707	0
RIGHT	0	230	250	0

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.3
EASTBOUND	5	0	.3
WESTBOUND	10	0	1

```

PHASING           N/S :4.   BOTH TURNS PROTECTED (WITH OVERLAP)
                  E/W :1.   NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1.   0 - 39 <#PDS/HR>
CYCLE LENGTH       : 90 SECONDS
  
```

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	S16	307	824	0
LEFT	302	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	287	0	0	0
ADJUSTED VOL	302	0	0	0
CAPACITY	0	0	824	0
MOVEMENT	N/A	N/A	OK	OK

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SLOATSBURG RD 4 MAR. KING AVE

DATE 1993 AM PEAK AS ZONED

*****#**
 LEVEL OF SERVICE A
 SATURATION 52
 CRITICAL N/S VOL 457
 CRITICAL E/W VOL 433
 CRITICAL SUM 390

LANE GEOMETRY												
LANE	NORTHBOUND MOV WIDTH		SOUTHBOUND MOV WIDTH		EASTBOUND MOV WIDTH		WESTBOUND MOV WIDTH					
1	T..	14.0	RT.	14.0	R..	13.0				
2	T..	12.0	T..	12.0	T..	12.0				
3	L..	12.0	...	***	T..	12.0				
4				
5				
6	...	****				

TRAFFIC VOLUMES				
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	287	0	0	0
THRU	492	S3	707	0
RIGHT	0	230	250	0

	TRUCKS (:4)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.3
EASTBOUND	5	0	.9
WESTBOUND	10	0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED.
 PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PEDS/HR>
 CYCLE LENGTH : 30 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	271	155	433	0
LEFT	302	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	287	0	0	0
ADJUSTED VOL	302	0	0	0
CAPACITY	0	0	433	0
-MOVEMENT	N/A	N/A	OK	OK

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SLOATSBURG RD & MAR. KING AVE

DATE 1993 AM PEAK AS ZONED

.....*-->
LEVEL OF SERVICE C
SATURATION 75
CRITICAL N/S VOL 457
CRITICAL E/W VOL 824
CRITICAL SUM 1281
.....*

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T. . 14.0	RT. 14.0	R. . 13.0
2	T. . 12.0	T. . 12.0	T. . 12.0
3	L.. 12.0
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	287	0	0	0
THRU	492	63	707	0
RIGHT	0	230	250	0

	TRUCKS	OO	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5		0	.3
SOUTHBOUND	5		0	.3
EASTBOUND	5		0	.3
WESTBOUND	10		0	1

PHASING N/S 4 BOTH TURNS PROTECTED (WITH OVERLAP)
E/W li! NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PEDS/HR>
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	E71	155	8E4	0
LEFT	302	0	3	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	287	0	0	0
ADJUSTED VOL	302	0	0	0
CAPACITY	0	0	824	0
MOVEMENT	N/A	N/A	OK	OK

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SLOATSBURG RD & MAR. KING AVE

DATE 1393 AM PEAK FULL DEVELOPMENT

*****#*****>***

LEVEL OF SERVICE D
SATURATION 37
CRITICAL N/S VOL 5S7
CRITICAL E/W VOL 904
CRITICAL SUM 1491

*-...>***>##*...>*****>...>...>***>*****

LANE	LANE GEOMETRY							
	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	T.	14.0	RT.	14.0	R.	13.0
2	L.	12.0	T.	12.0
3
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	275	0	0	0
THRU	530	70	775	0
RIGHT	0	217	481	0

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	10	0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W :1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0-99 (#PEDS/HR)
CYCLE LENGTH : 30 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	556	300	904	0
LEFT	EB7	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	£75	0	0	0
ADJUSTED VOL	287	0	0	0
CAPACITY	0	0	304	0
MOVEMENT	N/A	N/A	OK	OK

6-20 D

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

SLOATSBURG RD. & MAR. KING AVE

DATE 1993 PM PEAK AS ZONED

LEVEL OF SERVICE A
SATURATION 54
CRITICAL N/S VOL 768
CRITICAL E/W VOL 164
CRITICAL SUM 932

LANE GEOMETRY

LANE	NORTHBOUND rtcv WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T.. 14.0	RT. 14.0	R.. 13.0
2	T.. 12.0	T.. 12.0	T.. 12.0
3	L.. 12.0	T.. 12.0
4
5
6

TRAFFIC VOLUMES

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	235	0	0	0
THRU	223	429	269	0
RIGHT	0	561	589	0

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	10	0	1

PHASING N/S : 4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W : 1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT*	122	530	164	0
LEFT	233	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	235	0	0	0
ADJUSTED VOL	238	0	0	0
CAPACITY	0	0	164	0
MOVEMENT	N/A	N/A	OK	OK

CAPACITY ANALYSIS FOR GREENWOOD LAKE TURNPIKE & SKYLANDS ROAD -
INTERSECTION 22

The A.M. **peak hour** will be the critical peak hour at this intersection. **The first** tests were done with all approaches having three lanes. Then the CALA analysis for the 1993 A.M. peak hour indicated a Level of service D at 84% saturation for the "As Zoned" scenario **and** a Level of service E at 94% saturation for the "Full Development" scenario.

For the **second tests**. Greenwood Lake Turnpike was assumed to be five lanes wide. Then the CMA analysis for the 1993 A.M. peak hour shows a **Level of** service B at 57% saturation for the "As Zoned" scenario **and** a Level of service B at 63% saturation for the "Full Development" scenario.

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SKYLANDS RD

DATE 1993 AM PEAK AS ZONED

*****#

LEVEL OF SERVICE D
 SATURATION 84
 CRITICAL N/S VOL 11(38)
 CRITICAL E/W VOL 335
 CRITICAL SUM 1443

*****#

LANE	NORTHBOUND		LANE GEOMETRY		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	RT.	14.0	T..	14.13	R..	13.0		
2	L..	12.0	T..	14.0		
3		
4		
5		
6		

	NORTHBOUND		TRAFFIC VOLUMES		EASTBOUND		WESTBOUND	
	MOV	VOL	MOV	VOL	MOV	VOL	MOV	VOL
LEFT		0		34		0		0
THRU		969		911		0		496
RIGHT		87		0		0		7

	TRUCKS (%)	LOCAL BUSES	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	0	0	1
WESTBOUND	2	0	.9

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	1108	956	0	335
LEFT	0	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	34	0	0
ADJUSTED VOL	0	0	0	0
CAPACITY	0	0	0	335
MOVEMENT	N/A	N/A	OK	OK

6-21A

JOHN E. CHRIST
CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SKYLANDS RD

DATE 1993 AM PEAK AS ZONED

.....
LEVEL OF SERVICE B
SATURATION 57
CRITICAL N/S VOL 639
CRITICAL E/W VOL 335
CRITICAL SUM 974
.....

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	RT. 13.0	T.. 13.0	R. 13.0
2	T.. 12.0	T.. 12.0	T.. 12.0
3	L.. 12.0
4
5
6

	NORTHBOUND	TRAFFIC VOLUMES SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	34	0	0
THRU	969	911	0	296
RIGHT	87	0	0	7

	TRUCKS <math>\%>	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.9
SOUTHBOUND	5	0	.9
EASTBOUND	0	0	1
WESTBOUND	2	0	.9

PHASING N/S : 4. BOTH TURNS PROTECTED (WITH OVERLAP)
E/W : 1. NEITHER TURN PROTECTED
PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	639	557	0	335
LEFT	0	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	34	0	0
ADJUSTED VOL	0	0	0	0
CAPACITY	0	0	0	335
MOVEMENT	N/A	N/A	OK	OK

G-21 c

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

SLOAṬSBURG RD & MAR. KING AVE

DATE 1993 PM PEAK FULL DEVELOPMENT

*****»*****

LEVEL OF SERVICE C
 SATURATION 70
 CRITICAL N/S VOL 1021
 CRITICAL E/W VOL 183
 CRITICAL SUM 1204

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	T.. 14.0	RT. 14.0	R.. 13.0
2	T.. 12.0	T.. 12.0	T.. 12.0
3	L.. 12.0	T.. 12.0
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	390	0	0	0
THRU	238	462	300	0
RIGHT	0	646	636	0

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	5	0	.3
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	10	0	1

PHASING N/S :4. BOTH TURNS PROTECTED (WITH OVERLAP)
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
FHRU -RIGHT	131	593	183	0
LEFT	428	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	390	0	0	0
ADJUSTED VOL	428	0	0	0
CAPACITY	0	0	183	0
MOVEMENT	N/A	N/A	OK	OK

G-20 G

CAPACITY ANALYSIS FOR GREENWOOD LAKE TURNPIKE & SLOATSBURG ROAD -
INTERSECTION 23

f
V

The P.M. peak hour will be the critical peak hour at this intersection. The first tests were with Greenwood Lake Turnpike four lanes wide and Sloatsburg Road three lanes wide. With this geometry the GVfA analysis for the 1993 P.M. peak hour indicated a Level of service C at 74% saturation for the "As Zoned" scenario and a Level of service D at 86% saturation for the "Full Development" scenario.

For the second tests Greenwood Lake Turnpike was widened to five lanes. Then the CMA indicated a Level of service B at 64% saturation for the "As Zoned" scenario and a Level of service C at a saturation of 73% for the "Full Development" scenario.

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SLOATSBURG RD

DATE 1993 PM PEAK FULL DEVELOPMENT

*****#**#*****>>>

LEVEL OF SERVICE D
 SATURATION 36
 CRITICAL N/S VOL 590
 CRITICAL E/W VOL 9S5
 CRITICAL SUM 1555

*****#*****>>>

LANE	LANE GEOMETRY			
	NORTHBOUND MOV WIDTH	SOUTHBOUND MOV WIDTH	EASTBOUND MOV WIDTH	WESTBOUND MOV WIDTH
1	...	RT. 13.0	T.. 14.0	RT. 14.0
2	...	T.. 12.0	L.. 12.0	T.. 12.0
3
4
5
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	0	7	0
THRU	0	960	592	1174
RIGHT	0	5	0	637

	TRUCKS (1)	LOCAL BUSES <#/HR>	PEAK HOUR FACTOR
NORTHBOUND	0	0	1
SOUTHBOUND	5	0	.9
EASTBOUND	5	0	.9
WESTBOUND	5	0	.9

PHASING N/S :1. NEITHER TURN PROTECTED
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 <#PEDS/HR>
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	0	590	621	965
LEFT	0	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	0	7	0
ADJUSTED VOL	0	0	0	0
CAPACITY	0	590	0	344
MOVEMENT	OK	OK	OK	OK

JOHN E. CHRIST
 CRITICPIL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SLOATSBURS RD

DATE 1393 PM PEAK FULL DEVELOPMENT

*****#*****-*****-*****

LEVEL OF SERVICE C
 SATURATION 73
 CRITICAL N/S VOL 590
 CRITICAL E/W VOL 713
 CRITICAL SUM 1309

*****>>>*****>>>*****>>>*****>>>*****>>>*****>>>*****>>>*****

LANE	LANE GEOMETRY							
	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	RT.	13.0	T..	14.0	R..	13.0
2	T..	12.0	L..	12.0	T..	12.0
3	T..	12.0
4
5
S

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	0	7	0
THRU	0	360	532	1174
RIGHT	0	5	0	607

	TRUCKS	C/.)	LOCAL BUSES	(#/HR)	PEAK HOUR	FACTOR
NORTHBOUND	0		0		1	
SOUTHBOUND	5		0		.3	
EASTBOUND	5		0		.3	
WESTBOUND	5		0		.3	

PHASING N/S :1. NEITHER TURN PROTECTED
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 33 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	0	530	621	713
LEFT	.0	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	0	7	0
ADJUSTED VOL	0	0	0	0
CAPACITY	0	530	0	3a
MOVEMENT	OK	OK	OK	OK

JOHN E. CHRIST
 CRITICAL MOVEMENT ANALYSIS

GREENWOOD LAKE TP & SLOATSBURG RD

DATE 1993 PM PEAK AS ZONED

LEVEL OF SERVICE B
 SATURATION 64
 CRITICAL N/S VOL 541
 CRITICAL E/W VOL 616
 CRITICAL SUM 1157

LANE	LANE GEOMETRY							
	NORTHBOUND		SOUTHBOUND		EASTBOUND		WESTBOUND	
	WOV	WIDTH	MOV	WIDTH	MOV	WIDTH	MOV	WIDTH
1	RT.	13.0	T..	14.0	R..	13.0
2		12.0	1..	12.0	T..	12.0
3	T..	T..	12.0
4
S
6

	TRAFFIC VOLUMES			
	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
LEFT	0	0	7	0
THRU	0	880	554	11306
RIGHT	0	5	13	437

	TRUCKS (%)	LOCAL BUSES (#/HR)	PEAK HOUR FACTOR
NORTHBOUND	0	13	1
SOUTHBOUND	5	0	.3
EASTBOUND	5	0	.3
WESTBOUND	5	0	.3

PHASING N/S :1. NEITHER TURN PROTECTED
 E/W :1. NEITHER TURN PROTECTED
 PEDESTRIAN ACTIVITY : 1. 0 - 99 (#PEDS/HR)
 CYCLE LENGTH : 90 SECONDS

CRITICAL LANE VOLUMES BY MOVEMENT

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
THRU -RIGHT	0	541	381	616
LEFT	0	0	0	0

LEFT TURN CHECK

	NORTHBOUND	SOUTHBOUND	EASTBOUND	WESTBOUND
INPUT VOLUME	0	0	7	3
ADJUSTED VOL	0	0	0	0
CAPACITY	0	541	0	35
MOVEMENT	OK	OK	OK	OK

INTERSECTION RECOMMENDATIONS

*V- The intersection recommendations are based on the
f V Intersection Capacity Analysis. It should be noted that both
scenarios consider only nine sites in Ringwood with a
conservative expansion of the existing background traffic at 3%
per year for ten years to 1993. The traffic increase from other
development in Ringwood and the neighboring areas may well give a
background traffic growth in excess of 3% per year. Therefore,
the recommended improvements should be considered the minimum
that should be made for each scenario.

Traffic signals are not practical at many locations. When
placed at intersections too close together progression problems
may be created resulting in a Level of service F. When traffic
signals are very close together multiphasing for the purpose of
clearing "through traffic" out of the area between the
intersections is often needed, causing a reduction in capacity.

f
A There are several intersections along Skyline Drive between
Cheshire Lane and Fieldston Drive that have not been included in
the tableau. These intersecting streets are residential feeder
streets. The traffic using them will experience similar
difficulties to traffic using Cheshire Lane and Countryside in
entering and exiting Skyline Drive. The same recommendations
given for the Cheshire Lane and Countryside intersections would
apply to these other intersections along Skyline Drive.

Intersection 1 - Skyline Drive and Countryside

As Zoned Scenario

Widen Skyline Drive to five lanes with the middle lane
for left turns.

Full Development Scenario

Widen Skyline Drive to five lanes with the middle lane
16 to 20 feet wide.

Paint channelization in the middle lane for left turns
into a left turns out of Countryside. With this
arrangement, the traffic turning left from Countryside
would only have to contend with one direction of
Skyline Drive traffic at a time.

Intersection 2 - Skyline Drive and Conkl intown Road

As_Zoned_Scenario

Widen Conkl intown Road to four lanes*

Widen Skyline Drive to five lanes accepting a Level of service D at 80% saturation or widen further to six lanes yielding a Level of service B at 59% saturation.

Install a traffic control signal.

Full Development Scenario

Widen Conkl intown Road to four lanes.

Widen Skyline Drive to six lanes.

Install a traffic control signal.

Intersection 3 - Skyline Drive and Cheshire Lane

As_Zoned_Scenario

Widen Skyline Drive to five lanes with the middle lane for left turns.

Do not install a traffic control signal.

Full Development Scenario

Widen Skyline Drive to five lanes with the middle lane 16 to 20 feet wide.

Paint channelization reserving the middle lane for left turns into and out of Cheshire Lane.

Intersection 4 - Skyline Drive and Fieldstone Drive

As_Zoned_Scenario

Widen Skyline Drive to five lanes.

Widen Fieldstone Drive to five lanes.

Install a traffic control signal.

Full Development Scenario

Widen Skyline Drive to six*lanes.

Widen Fieldstone Drive to five lanes.

Install a traffic control signal.

Intersection-5 - Skyline Drive and the Site 2 Driveway

As_Zoned_Scenario

Widen Skyline Drive to five or six lanes.

Improve the horizontal alignment of Skyline Drive.

Provide two lanes for left turn exits and one lane for right turn exits.

Install a traffic control signal.

Full Development Scenario

*s~
V
Widen Skyline Drive to six lanes,
Improve the horizontal and vertical alignment of
Skyline Drive,
Provide two site roadways in close proximity to each
other so that left turns entering the site and left
turns exiting the site can do so on the same signal
phase without interfering with each other on Skyline
Drive.
Install a traffic control signal.

Intersection 6 - Skyline Drive and Knollwood Drive

Either Scenario

Widen Skyline Drive to five lanes.
Provide three lanes in Knollwood Drive.
Install a traffic control signal.

Intersection 7 - Skyline Drive and Erskine Road

As Zoned Scenario

Widen Skyline Drive to five lanes.
Provide two lanes for Erskine Road traffic to turn left
into Skyline Drive.
Provide channelization to separate the Erskine Road
right turns into Skyline Drive from the signalized part
of the intersection.
Install a traffic control signal.

Full Development Scenario

Widen Skyline Drive to six lanes.
As above, provide two lanes for southbound Erskine Road
traffic to turn left into Skyline Drive,
Provide channelization to separate the right turns out
of the intersection proper.
Install a traffic control signal.

Intersection 8 - Greenwood Lake Turnpike and Skyline Drive

* 1

As Zoned Scenario

Widen Greenwood Lake Turnpike to six lanes.

Provide dual left turn lanes for Skyline Drive traffic to turn left onto Greenwood Lake Turnpike.

Provide a separate lane on Skyline Drive for right turns to Greenwood Lake Turnpike and an acceleration lane in Greenwood Lake Turnpike so that the right turn is not included in the intersection control. This acceleration lane is in addition to the six lanes stated above.

Install a traffic control signal.

Full Development Scenario

Same as the "As Zoned" scenario accepting a Level of service D at a saturation rate of 80% because further widening would be impractical.

Intersection 9 - Greenwood Lake Turnpike and West Brook Road

Both Scenarios

Widen Greenwood Lake Turnpike to three or four lanes.

Widen West Brook Road to three lanes.

Install a traffic control signal.

Intersection 14 - Greenwood Lake Turnpike and Stonetown Road

Both Scenarios

Widen Greenwood Lake Turnpike to four lanes.

Widen Stonetown Road to three lanes.

Install a traffic control signal.

Intersection 15 - Greenwood Lake Turnpike and Margaret King Avenue

As Zoned Scenario

Widen Greenwood Lake Turnpike to four lanes.

Provide separate lanes for the westbound left and right turns from Margaret King Avenue.

Install a traffic control signal.

Full Development Scenario

Widen Greenwood. Lake Turnpike to five lanes.

Provide separate lanes for the westbound left and right turns from Margaret King Avenue.

Install a traffic control signal.

Intersections 16 6c 17 - Margaret King Avenue and Sterling Forest Tract

Both Scenarios

Widen Margaret King Avenue to five lanes with the middle lane 16 to 20 feet wide.

Paint channelization in the middle lane reserving it for left turns into and left turns out of the site.

Provide two or more access points to the site.

Do not install a traffic control signal.

Intersection 18 - Margaret King Avenue and Site 6

As Zoned Scenario

Widen Margaret King Avenue to five lanes.

Do not install a traffic control signal.

Full Development Scenario

Widen Margaret King Avenue to five lanes with the middle lane 16 to 20 feet wide.

Paint channelization in the middle lane reserving it for left turns into and left turns out of the site.

Do not install a traffic control signal.

Intersection 19 - Margaret King Avenue and Site 7

Both Scenarios

Widen Margaret King Avenue to five lanes with the middle lane 16 to 20 feet wide.

Paint channelization in the middle lane reserving it for left turns into and left turns out of the site.

Do not install a traffic control signal.

Intersection 21 - Sloatsburg Road and Margaret King Avenue

Both Scenarios

Widen Sloatsburg Road to five lanes

Widen Margaret King Avenue to five lanes with two eastbound lanes for left turns and one eastbound lane for right turns.

Install a traffic control signal.

Intersection 22 - Greenwood Lake Turnpike and Skylands Road

Both Scenarios

Widen Greenwood Lake Turnpike to five lanes.

Install a traffic control signal.

Intersection 23 - Greenwood Lake Turnpike and Sloatsburg Road

As. Zoned Scenario Widen Greenwood Lake Turnpike to four lanes.

Install a traffic control signal.

Full Development Scenario

Widen Greenwood Lake Turnpike to five lanes.

Install a traffic control signal.

ROADWAY RECOMMENDATIONS

These recommendations are to cover roadway sections between the major intersections. At the major intersections the Intersection Recommendations would apply.

SKYLINE DRIVE

As Zoned Scenario

Skyline Drive should be widened to five lanes from Greenwood Lake Turnpike to south of Intersection 1 at Countryside (Site 1) near the water tower. From Countryside (Site 1) south Skyline Drive should be four lanes wide.

Full Development Scenario

Skyline Drive should be widened to five lanes with the middle lane 16 to 20 feet wide from Greenwood Lake Turnpike to south of Countryside (Site 1), and four lanes from this point southerly.

Greenwood Lake Turnpike

Both Scenarios

Widen Greenwood Lake Turnpike to four lanes from the southern Borough line to Skyline Drive, then five lanes to Sloatsburg Road, then four lanes to the New York border.

Sloatsburg Road

Both Scenarios

Widen Sloatsburg Road to four lanes for its entire length.

Margaret King Avenue

As Zoned Scenario

Widen Margaret King Avenue to five lanes from Greenwood Lake Turnpike to Peters Mine Road, and then four lanes to Sloatsburg Road,

Full Development Scenario

Widen Margaret King Road to five lanes with the middle lane 16 to 20 feet wide from Greenwood Lake Turnpike to Peters Mine Road, and then four lanes to Sloatsburg Road,

West Brook Road and Stonetown Road

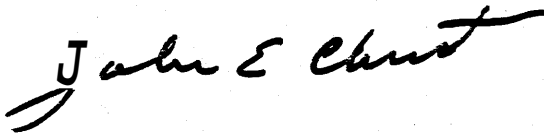
Both Scenarios

Improve these roadways to two lane roadways with cross sections conforming to the AASHTO Policy on Design of Urban Highways.

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I certify that the above is a true representation of my findings.



John E. Christ, P.E.
New Jersey License 13883

?0 Orton Road

West Caldwell, New Jersey 07006

201-226-3609

PROFESSIONAL ENGINEER

^ Licensed in the State of New Jersey, Certificate #13883

EDUCATION

Bachelor of Science in Civil Engineering, Rutgers University, June 1953-
Certificate in Traffic Engineering, Yale University Bureau of Highway
Traffic, 1959 (academic year full time graduate school)

EXPERIENCE

Senior Engineer-Traffic, New Jersey Division of Motor Vehicles, Bureau of
Engineering and Planning, June 1959 to April 1963* Design of traffic con-
trol devices such as traffic signals, speed zone signs, "through streets"
channelizations, intersection geometries, regulatory and warning signs,
review of traffic data including volume counts and accident reports.

Principal Engineer-Traffic, Essex County (N.J.) Highways and Bridges
Department, April 1963 to December 1965.

Traffic Engineer, Essex County Engineering Division, formerly the High-
ways and Bridges Dept., December 1965 to present: Determines the need for
and the design of traffic control devices such as traffic signal3, inter
section and roadway geometries, channelizations, regulatory, warning and
guide signs, review of accident data, traffic counts, site plans, sub-
divisions, TOPICS analysis, describes aspects of traffic to the public,
gives expert testimony concerning the County roadway system. VWorks with
other engineers in department on various roadway projects. Responsible
to the County Engineer.

f Former teacher at Rutgers University, University Extension Division, New
v- Brunswick, N.J., 1968 through 1977:

Traffic Regulations: 3 years, k sessions/yr., 2 hours per session

Traffic Signals: 5 years, 13 sessions/yr., 3 hours per session

Intersection Geometries: 1. year, 2 sessions/yr. 3 hours per session

Traffic Signs and Markings: 2 years, 10 sessions/yr, 3 hours per sessi(

Lecturer at various traffic seminars given by Rutgers University, Newark
College of Engineering, A.A.A., New Jersey State Safety Council and
Substitute Lecturer at he Bergen County Policé Academy.

Consulting As a Professional Engineer, April 1965 to present: Design of
driveways and parking facilities for businesses, design of traffic contro
signals and one-way roadway report for municipalities, expert testimony
before planning boards, variance boards, A.B.C. hearings, magistrates
courts, Superior Court, Chancery Division and Law Division of Superior-
Court, Traffic Court.

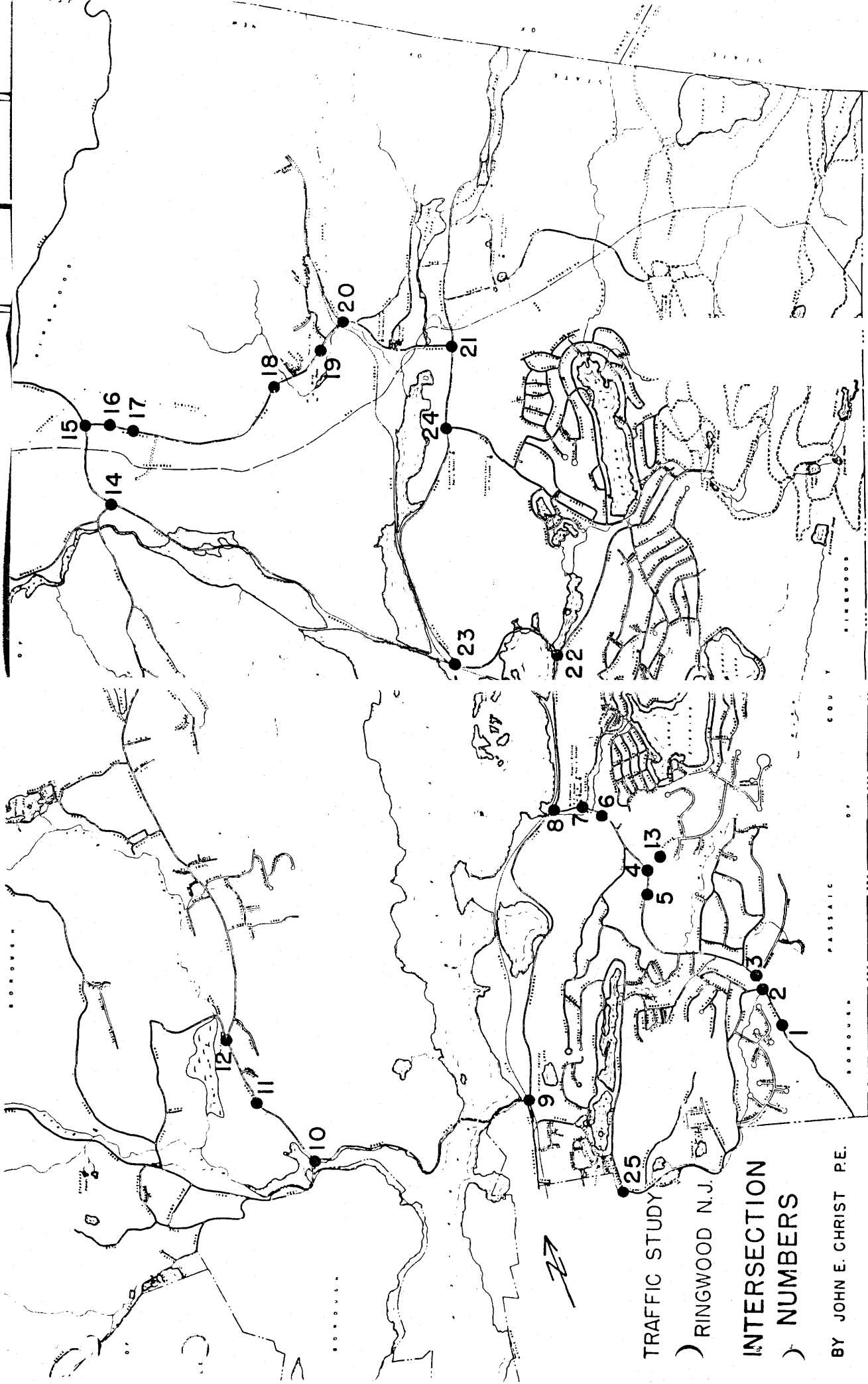
ACTIVITIES"

Member of the Institute of Transportation Engineers, currently Immediate
Past President of the N.Y. and N.J. Metropolitan Section (also past
Treasurer, Secretary, and Vice President.

Supporting Member of the Transportation Research Board, National Academy
of Sciences.

Past member of committees to review the State Laws on Traffic and the
Manual on Uniform Traffic Control Devices for Streets and Highways

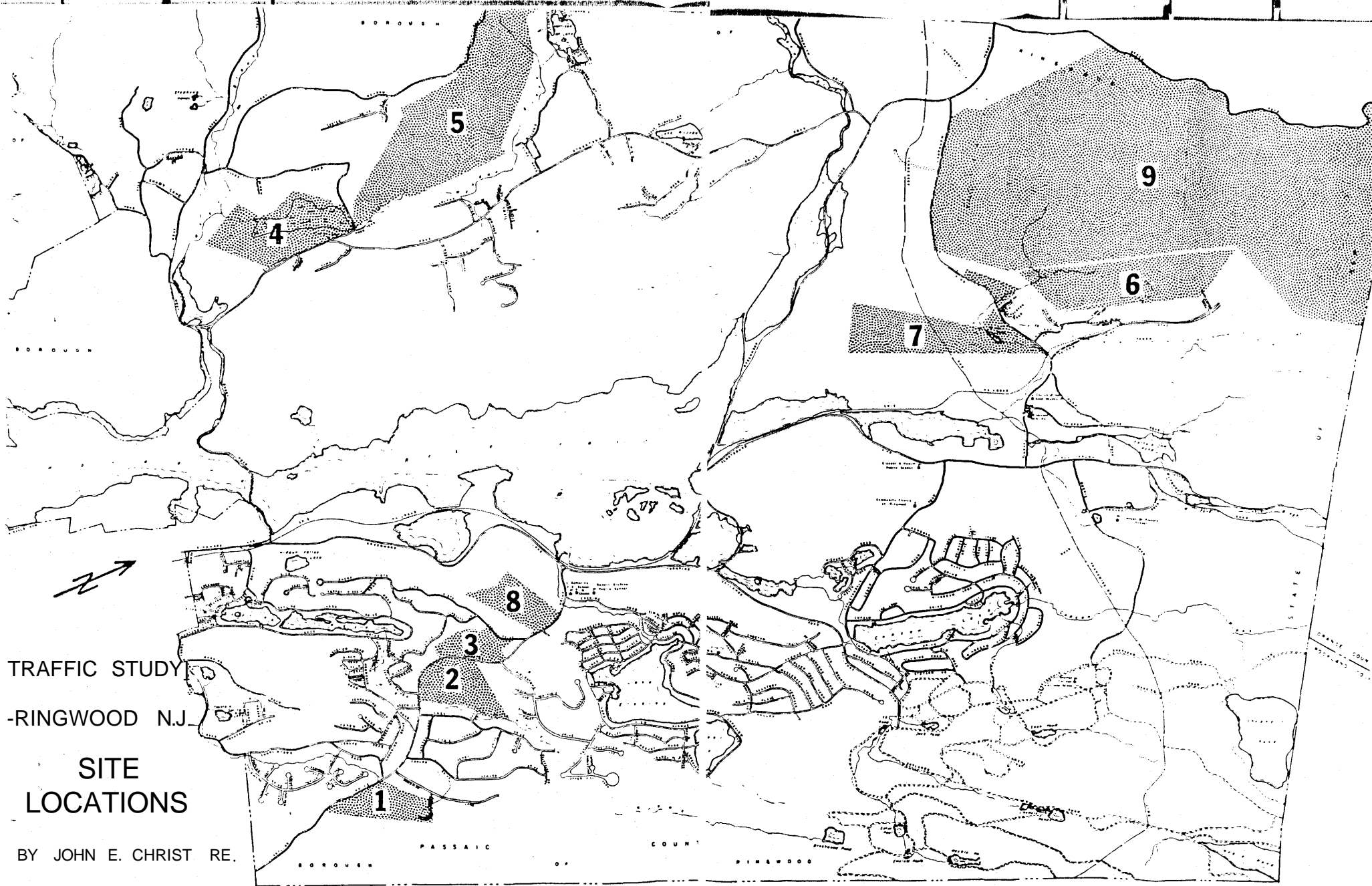
Listed in the 1980 edition of Who's Who in Engineering, published by
the American Association of Engineering Societies.



TRAFFIC STUDY
RINGWOOD N.J.

**INTERSECTION
NUMBERS**

BY JOHN E. CHRIST P.E.



TRAFFIC STUDY
-RINGWOOD N.J.
SITE
LOCATIONS

BY JOHN E. CHRIST RE.

PASSAIC COUNTY

BERGEN COUNTY

APPENDIX A

1983 BACKGROUND TRAFFIC

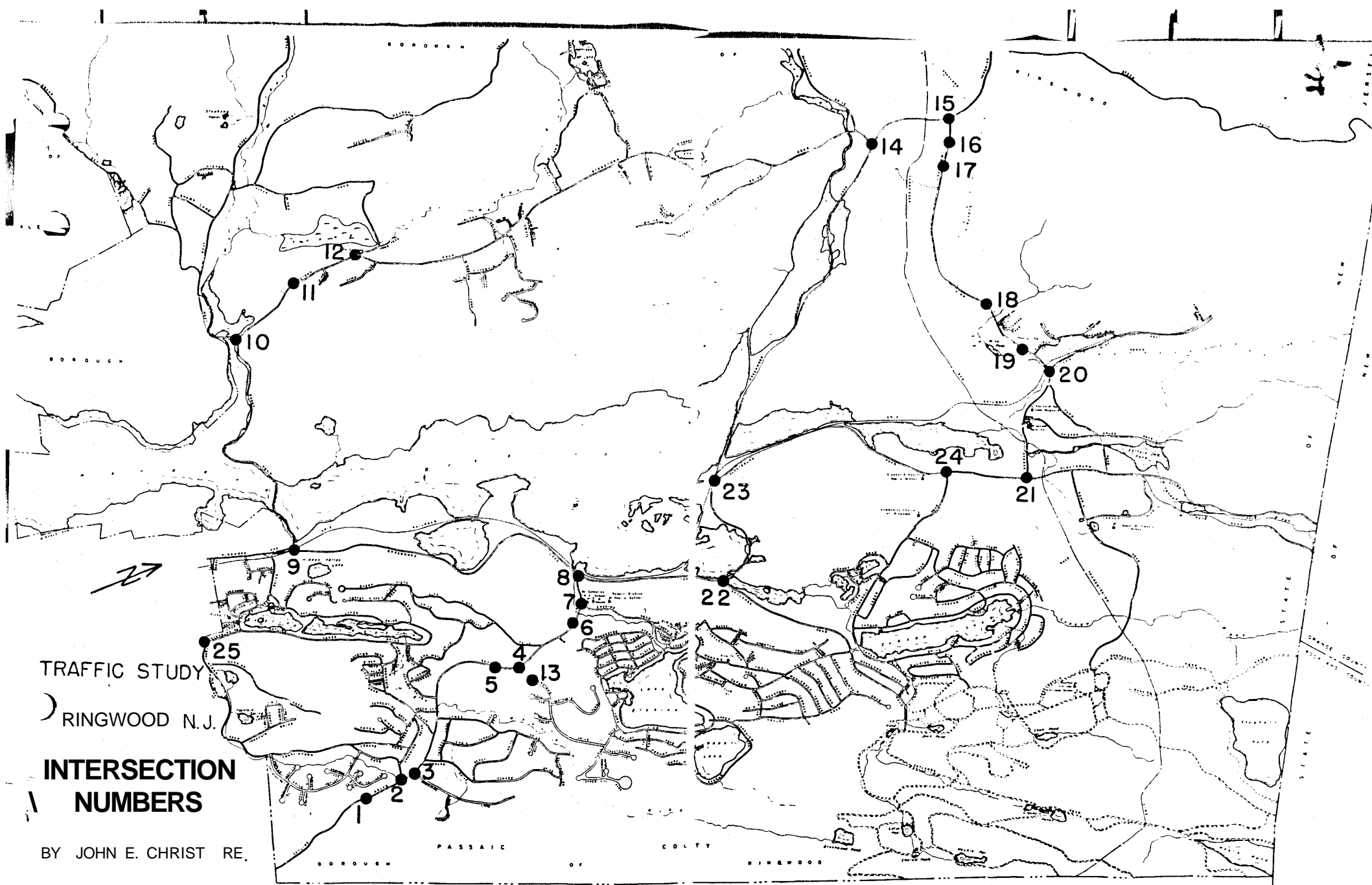
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P.M. EXISTING TRAFFIC VOLUMES	A- 2
A.M. 1993 TRAFFIC VOLUMES	A- 3
P.M. 1993 TRAFFIC VOLUMES	A- 4

1993 BACKGROUND TRAFFIC AND SITE TRAFFIC

~ A.M. RESULTING TRAFFIC VOLUMES WITH STUDY SITES DEVELOPED AS ZONED	A- 5
C	A - 6
^ P.M. RESULTING TRAFFIC VOLUMES WITH STUDY SITES DEVELOPED AS ZONED	
A.M. RESULTING TRAFFIC VOLUMES WITH STUDY SITES DEVELOPED AS PROPOSED BY OTHERS	A- 7
P.M. RESULTING TRAFFIC VOLUMES WITH STUDY SITES DEVELOPED AS PROPOSED BY OTHERS	A- 8

1983 BACKGROUND TRAFFIC AND SITS TRAFFIC

A.M. EXISTING TRAFFIC VOLUMES WITH STUDY SITES DEVELOPED AS ZONED	A- 9
P.M. EXISTING TRAFFIC VOLUMES WITH STUDY SITES DEVELOPED AS ZONED	A-10
A.M. EXISTING TRAFFIC VOLUMES WITH STUDY SITES DEVELOPED AS PROPOSED BY OTHERS	A-H
P.M. EXISTING TRAFFIC VOLUMES WITH STUDY SITES DEVELOPED AS PROPOSED BY OTHERS	A-12



TRAFFIC STUDY

RINGWOOD N.J.

**INTERSECTION
NUMBERS**

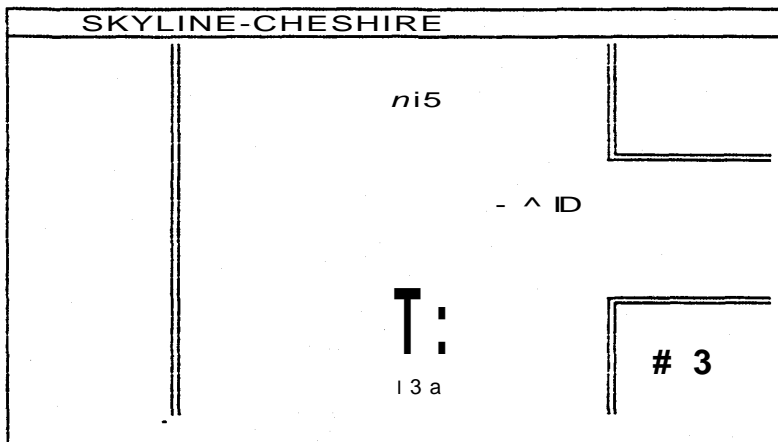
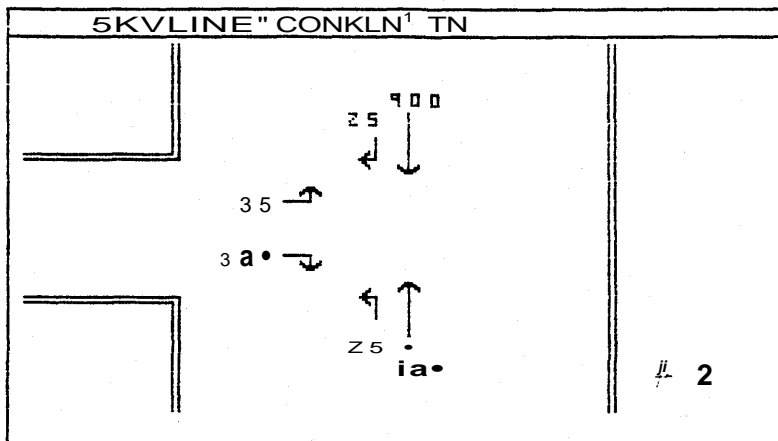
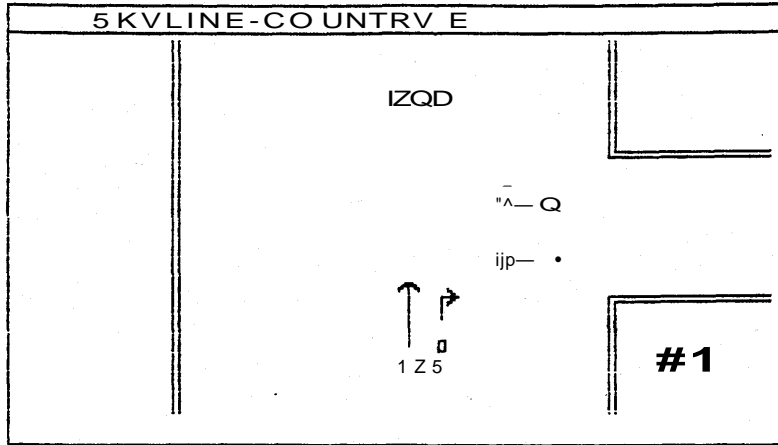
BY JOHN E. CHRIST RE.

1983 BACKGROUND TRAFFIC

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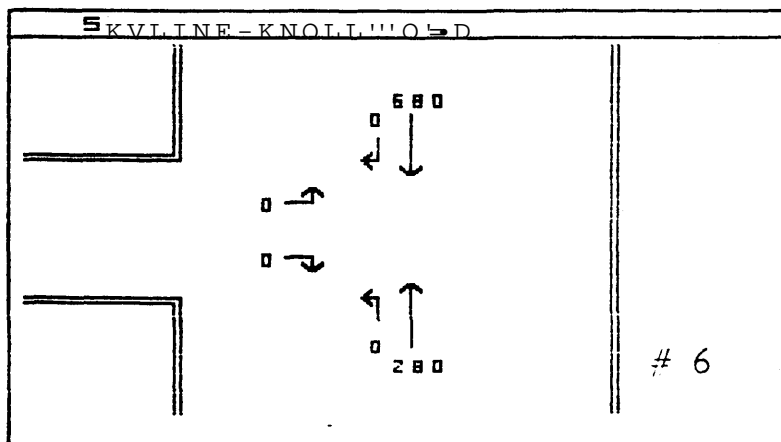
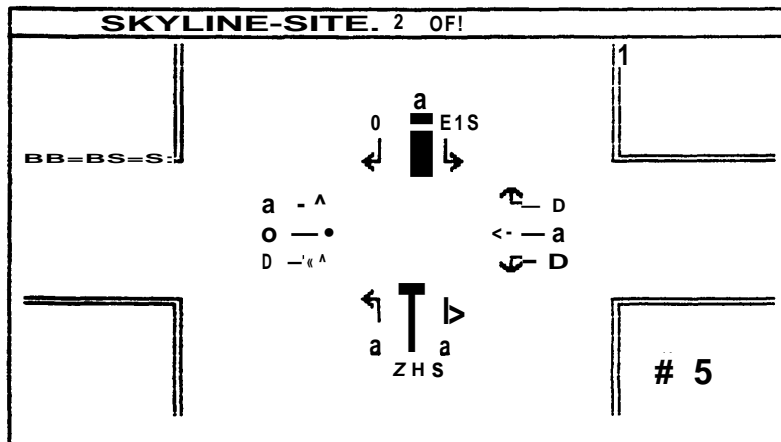
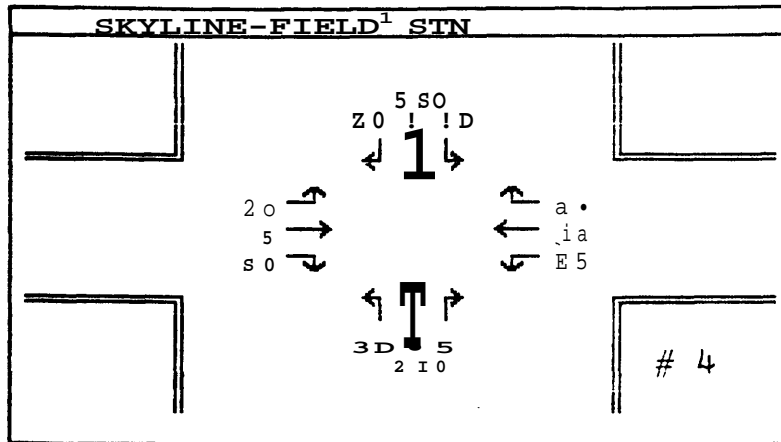
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A.M. PEAK HOUR



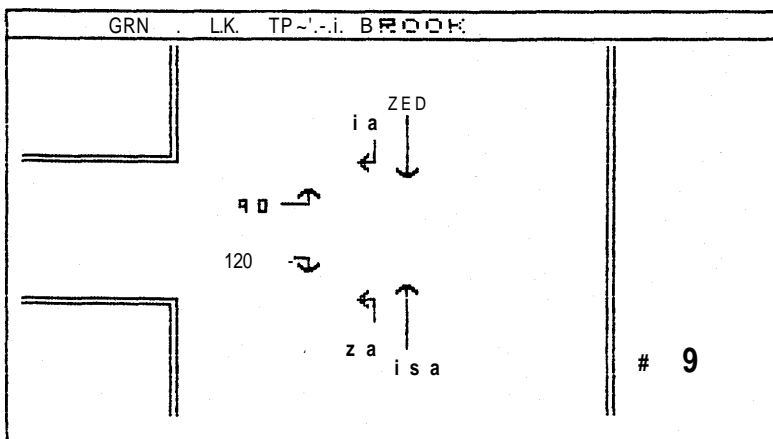
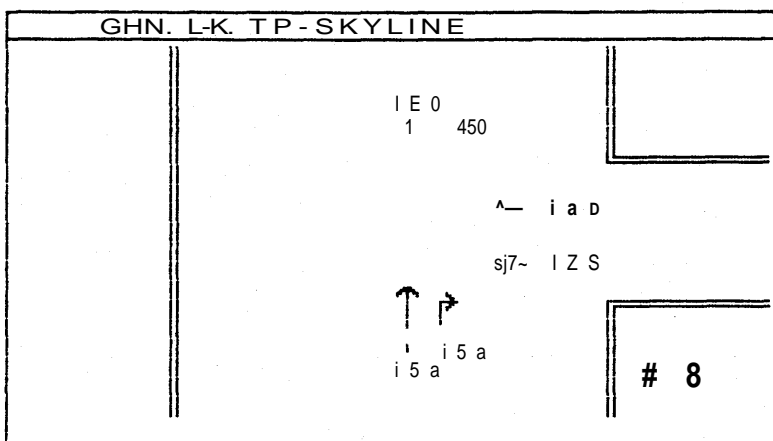
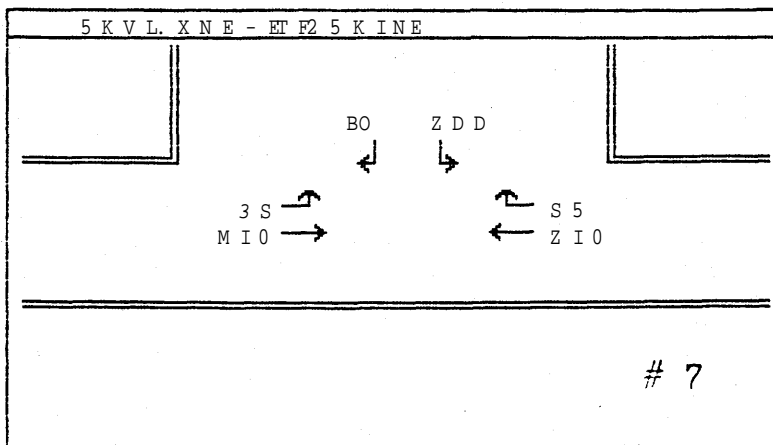
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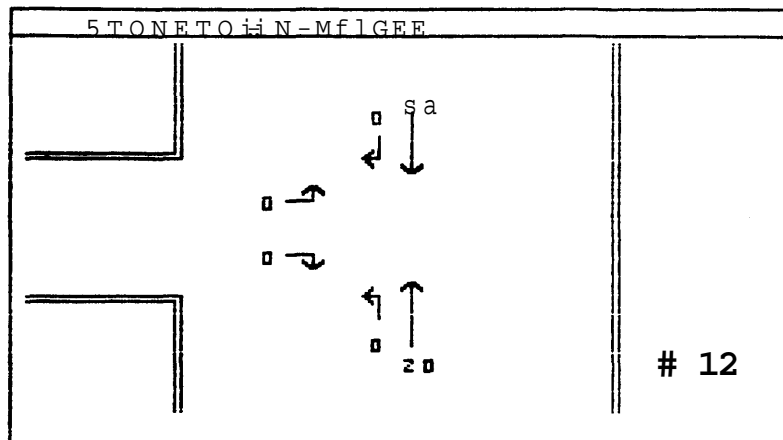
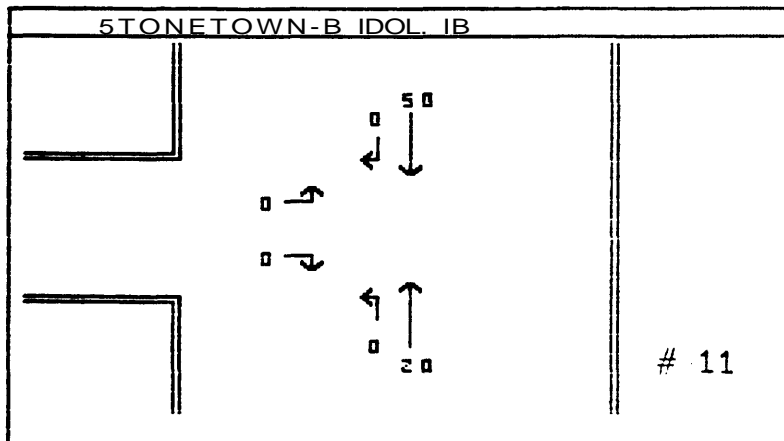
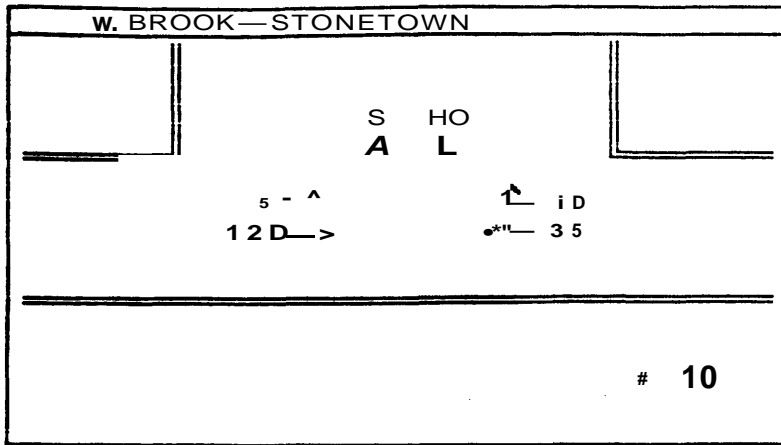


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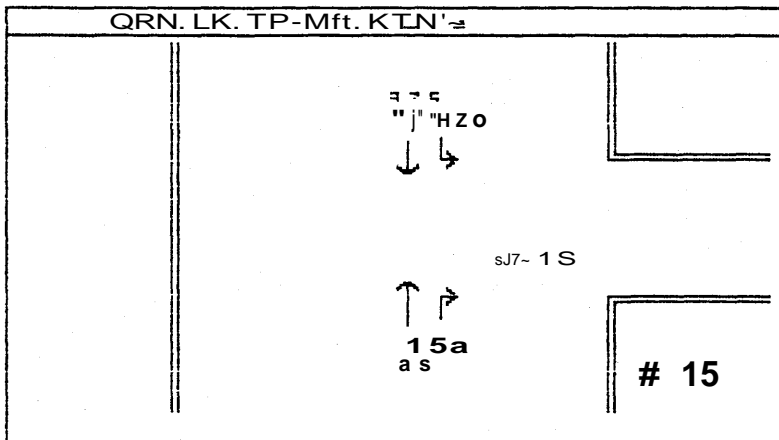
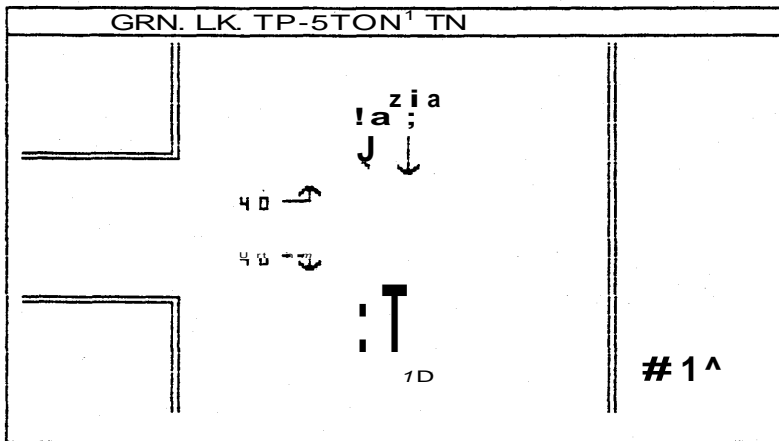
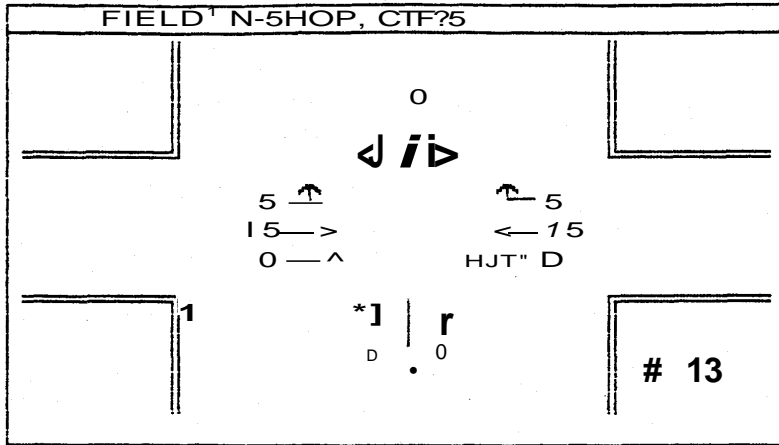
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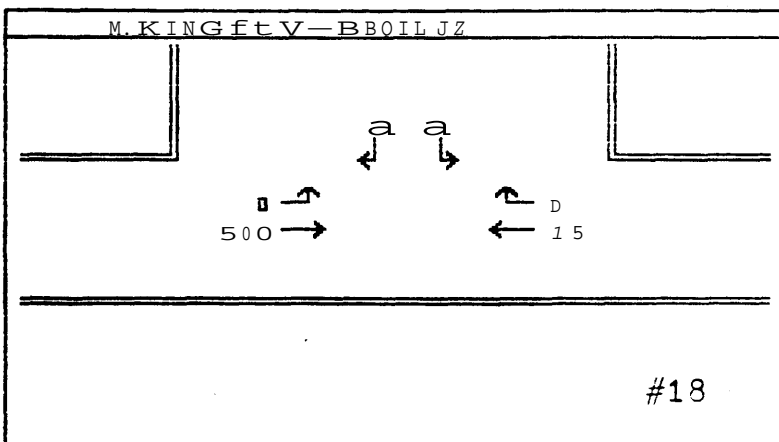
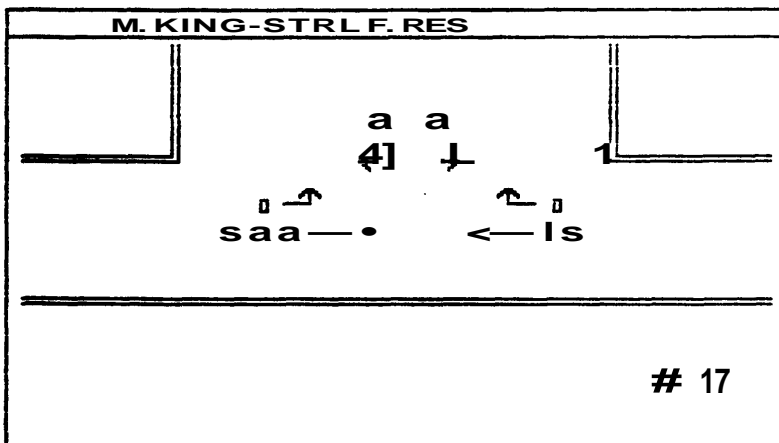
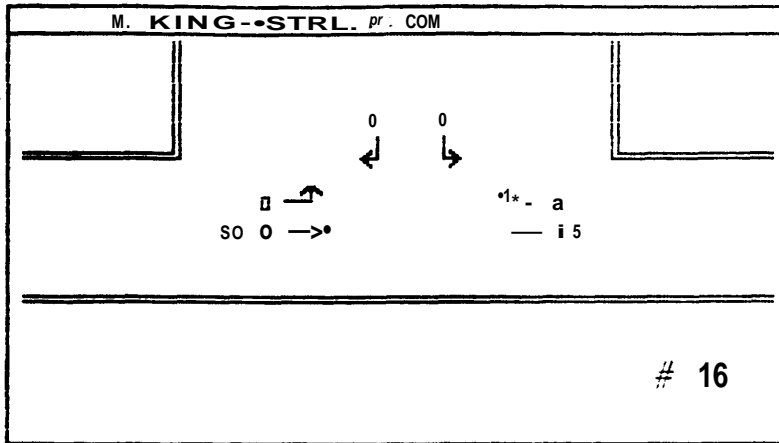


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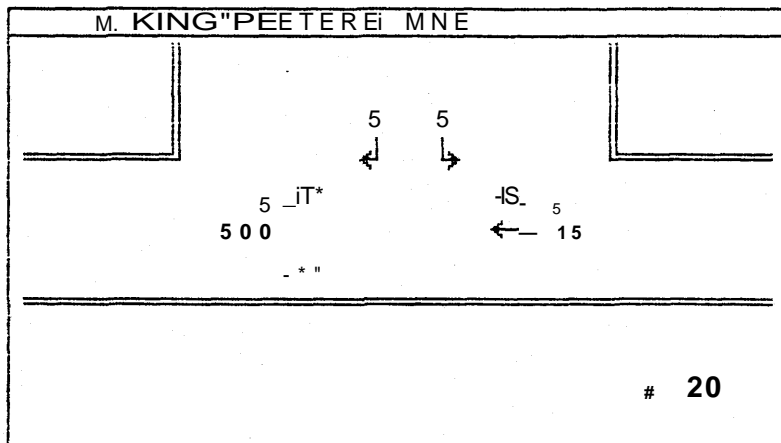
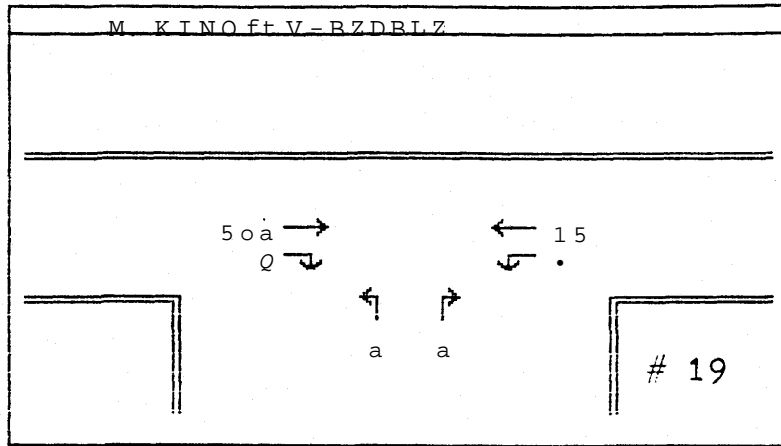


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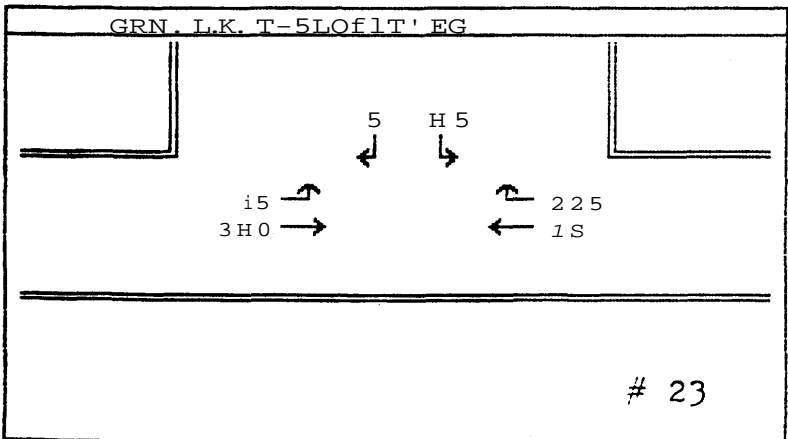
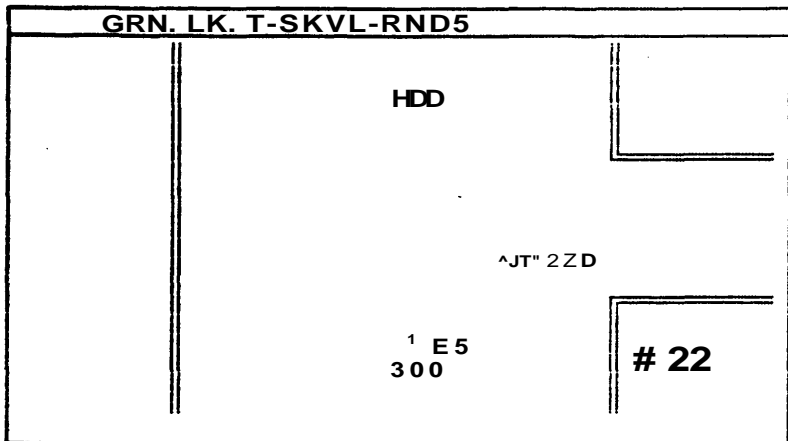
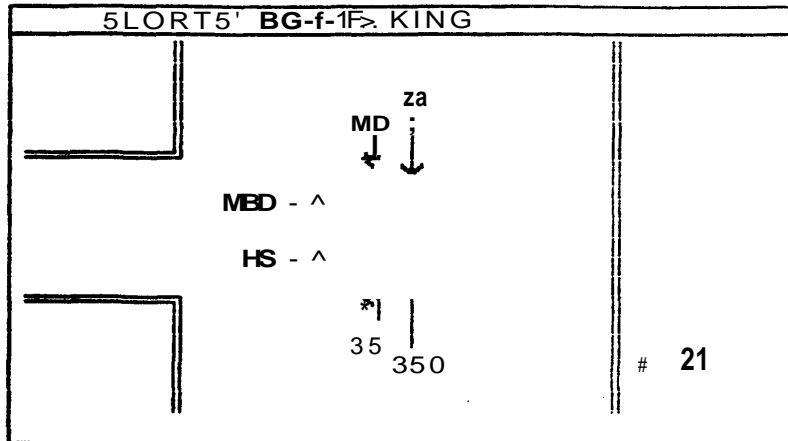
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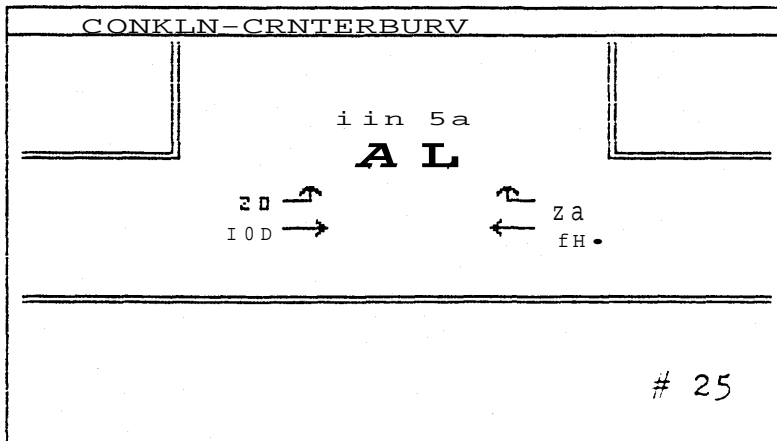
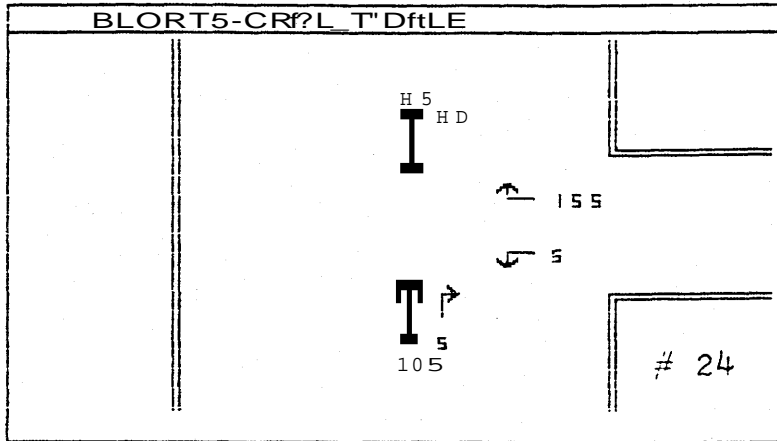


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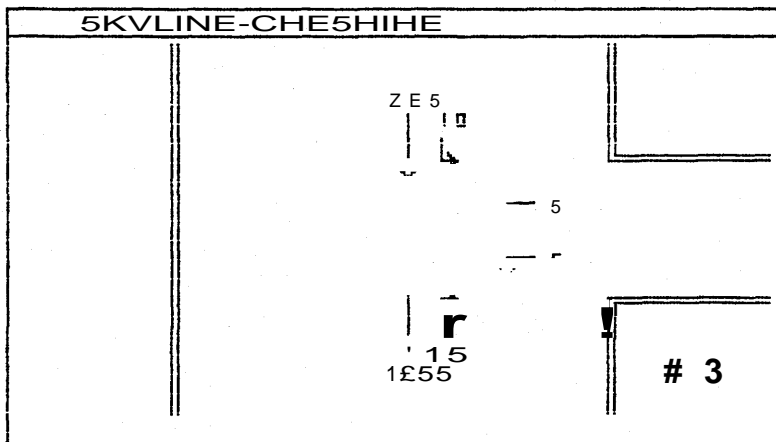
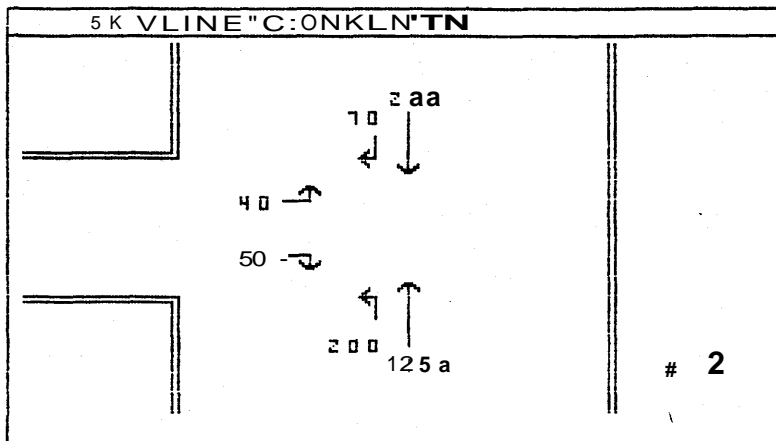
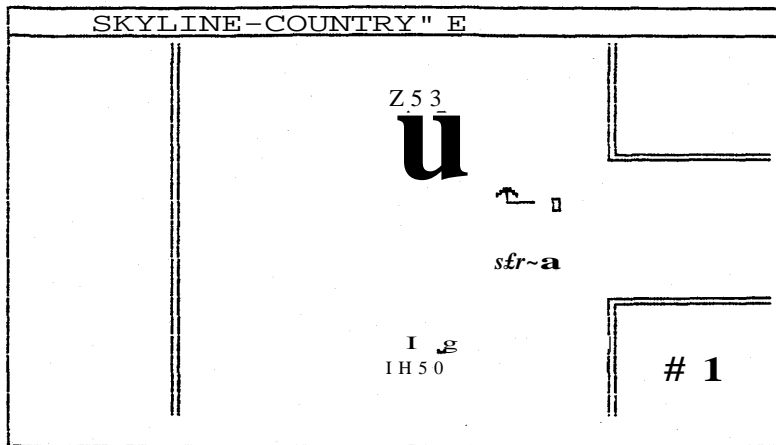


1983 BACKGROUND TRAFFIC

P.M. PEAK HOUR EXISTING TRAFFIC VOLUMES

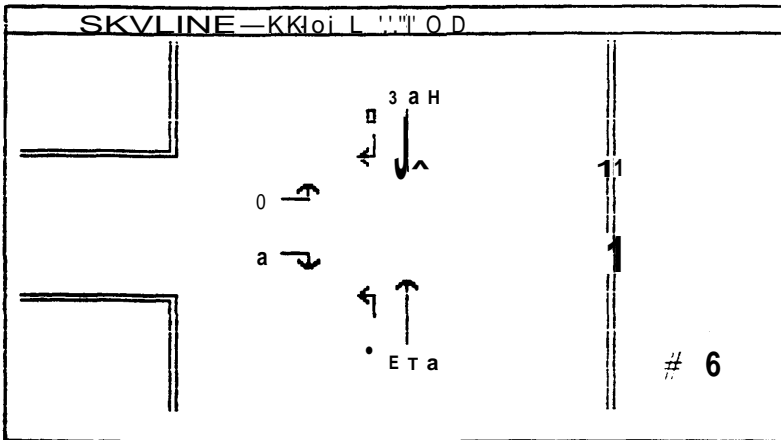
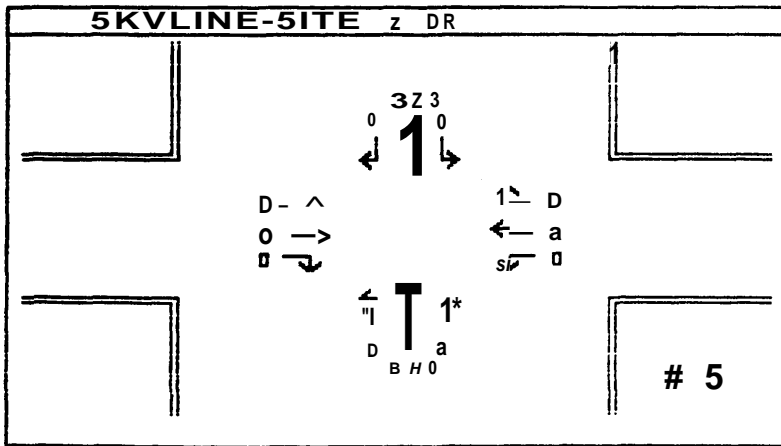
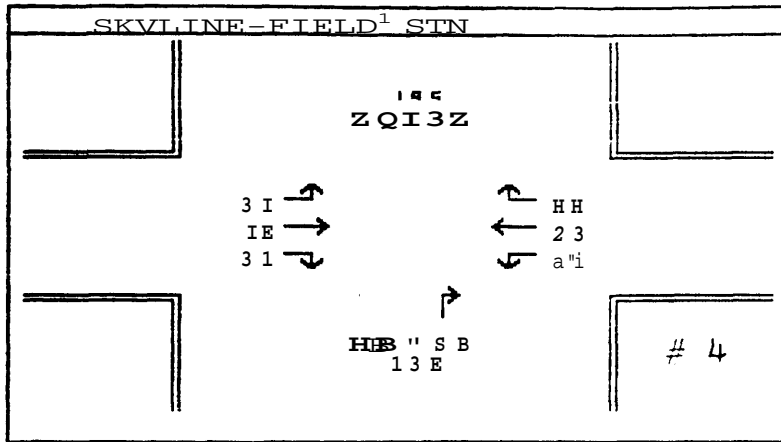
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P.M. PEAK HOUR

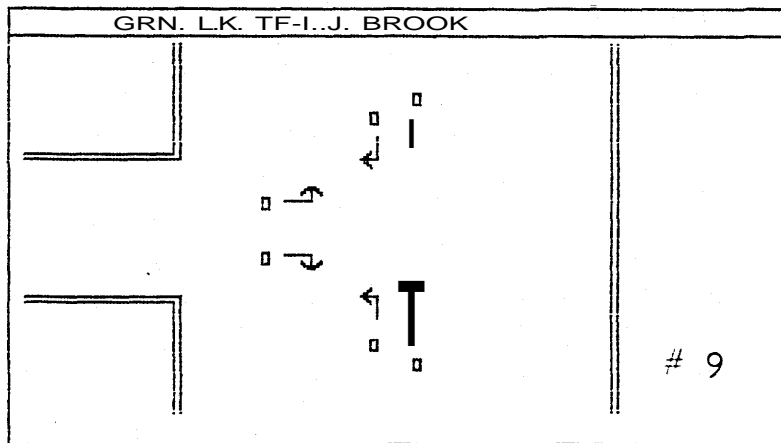
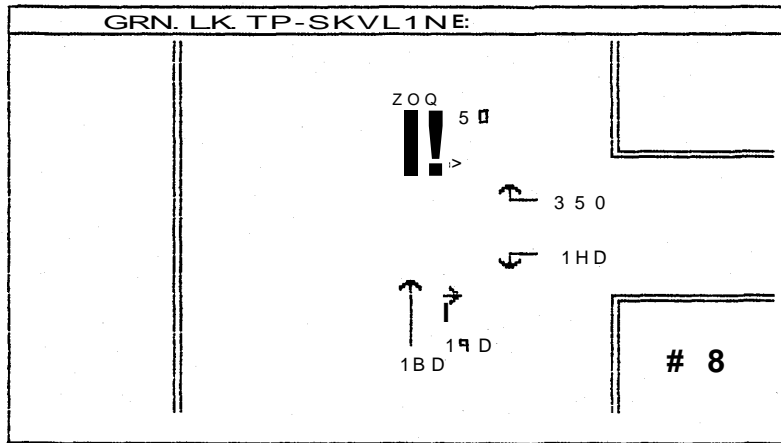
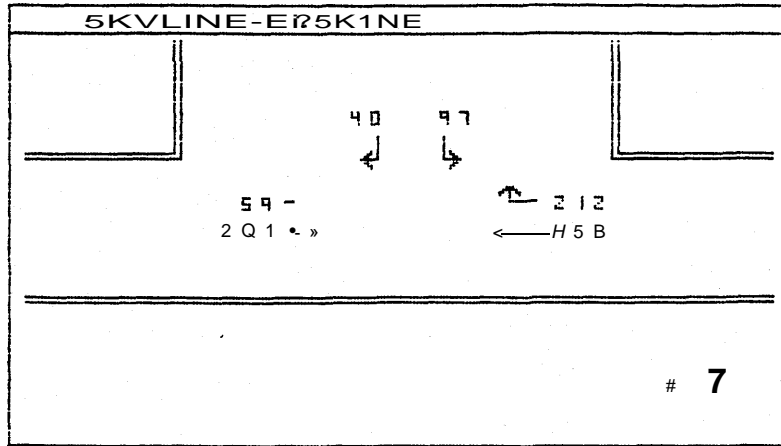


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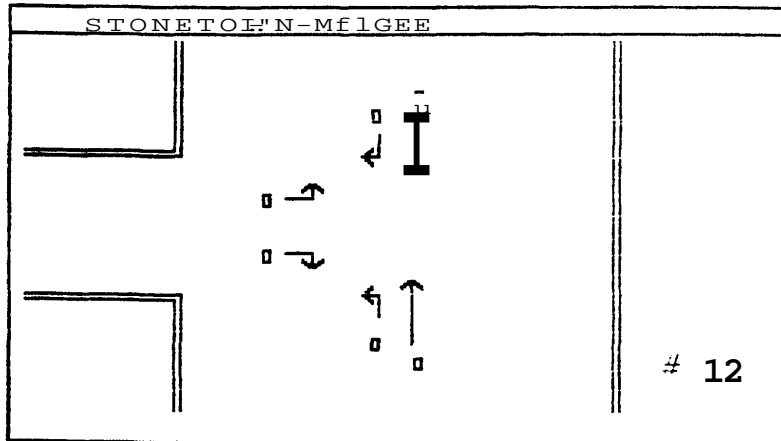
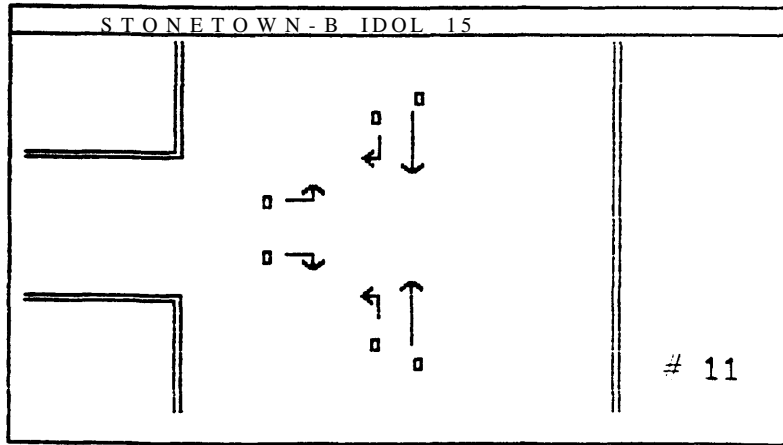
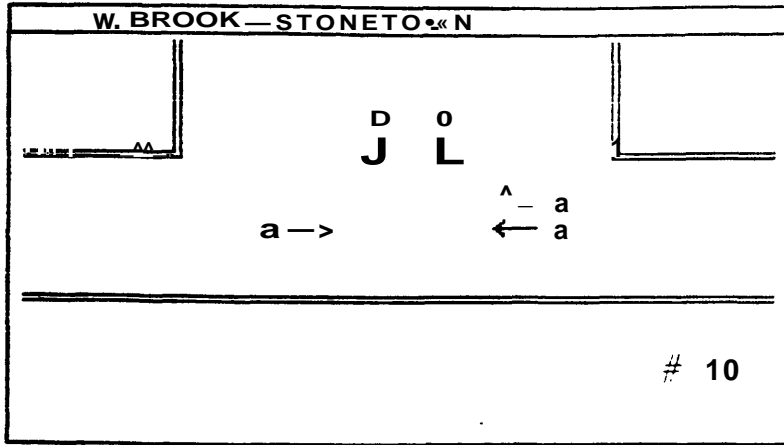
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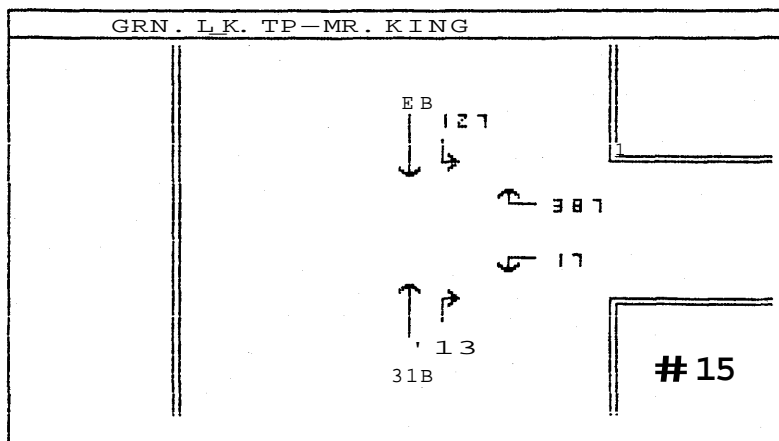
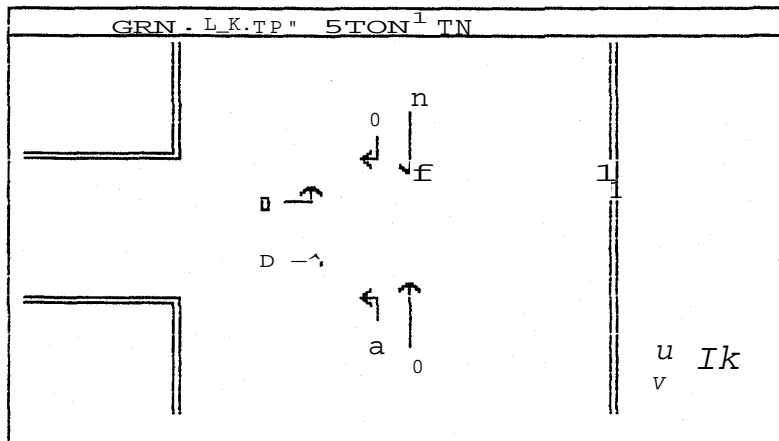
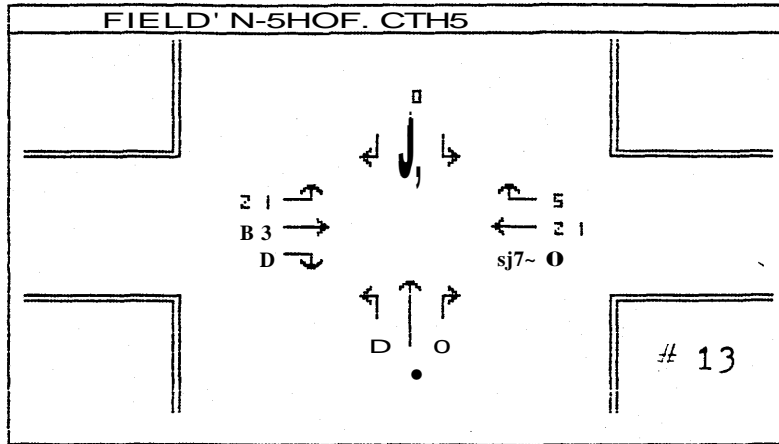
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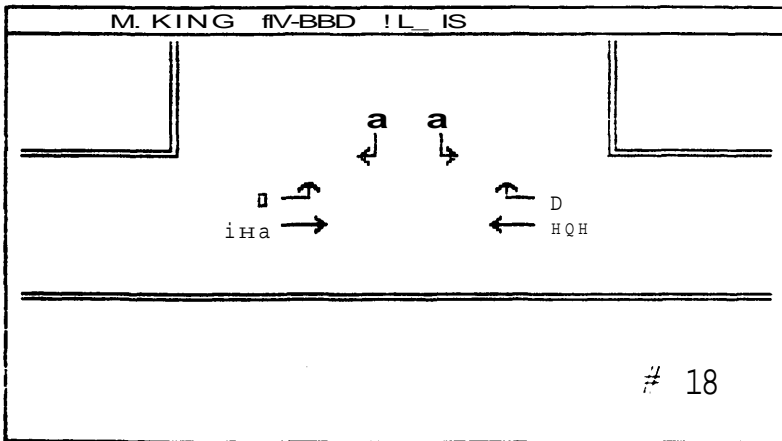
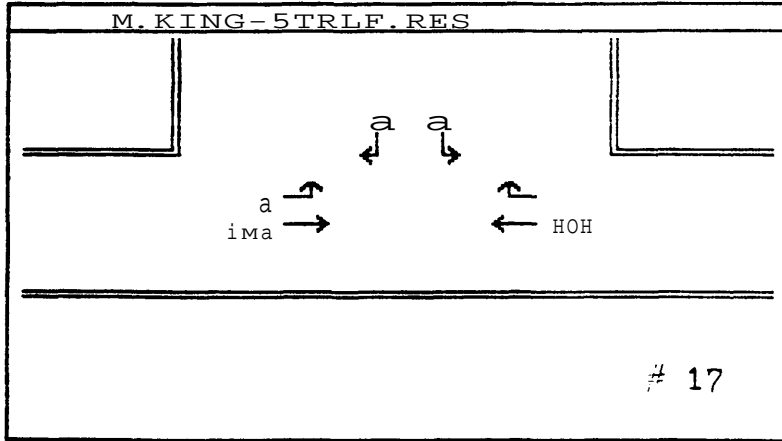
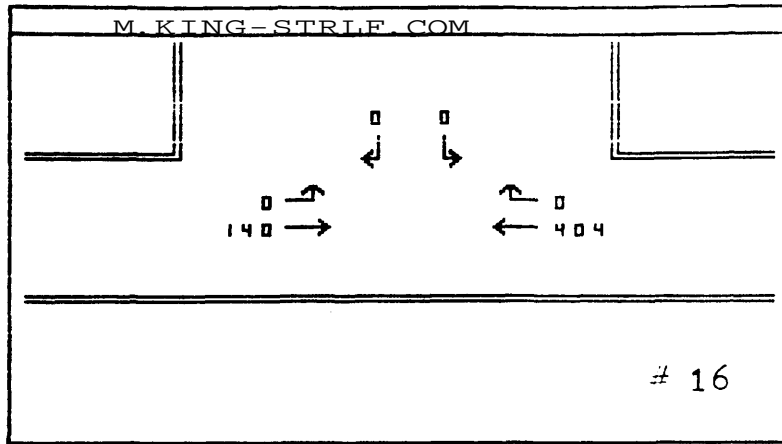


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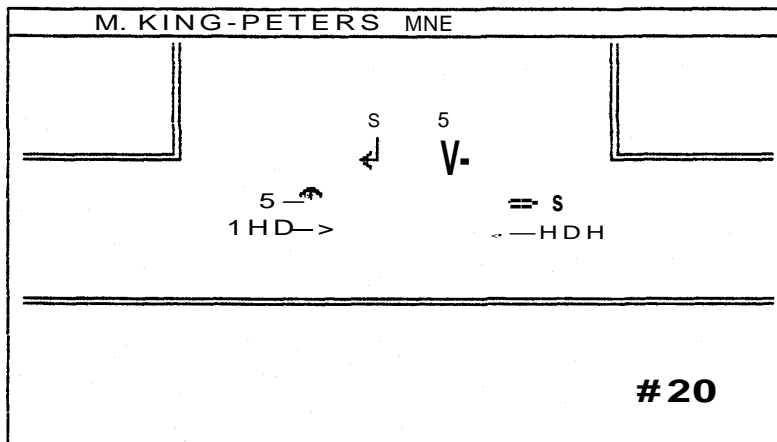
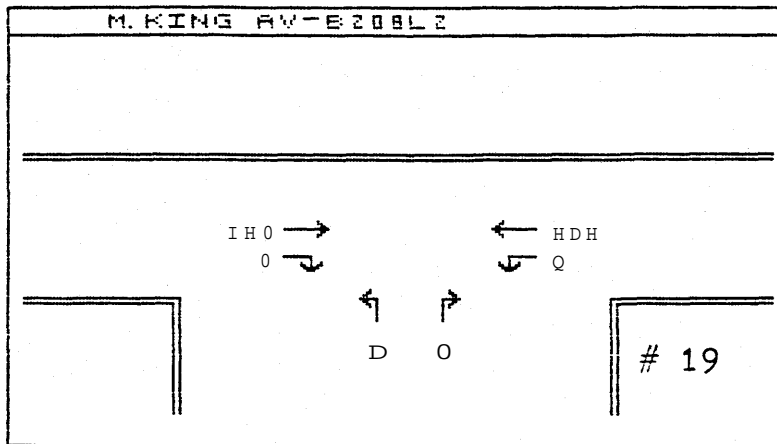
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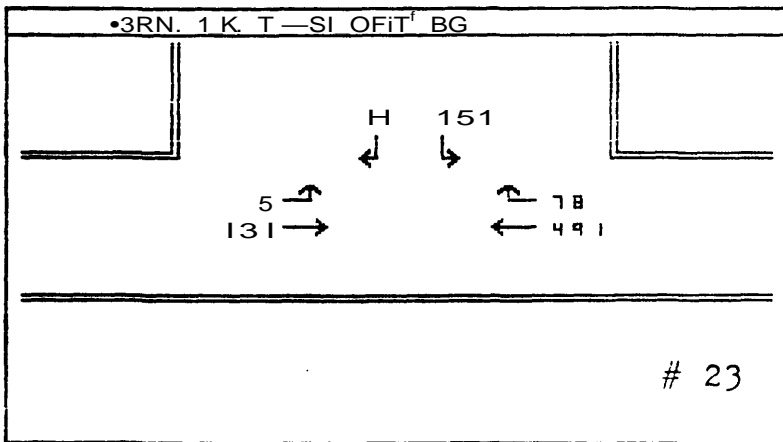
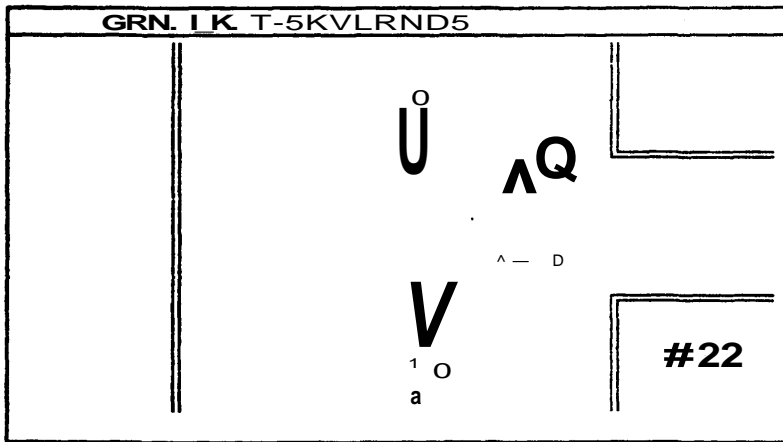
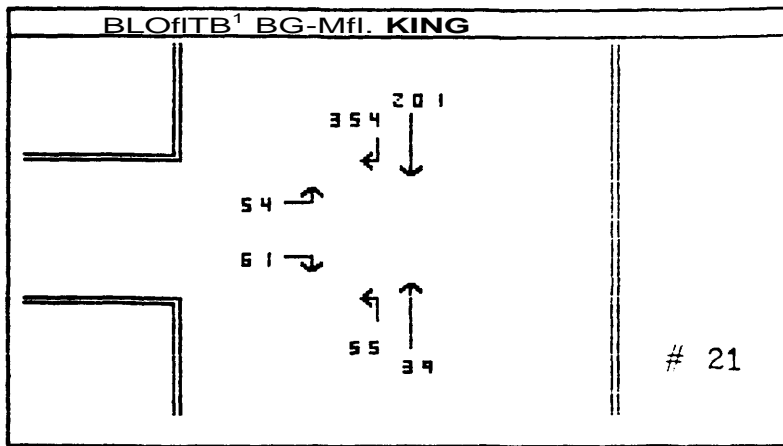


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P.M. PEAK HOUR

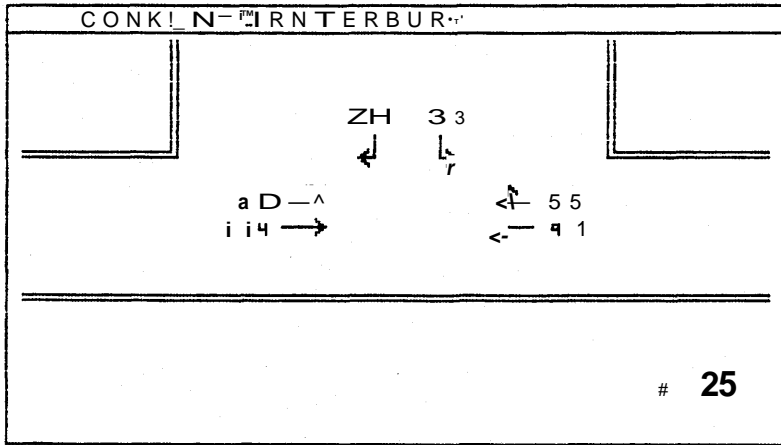
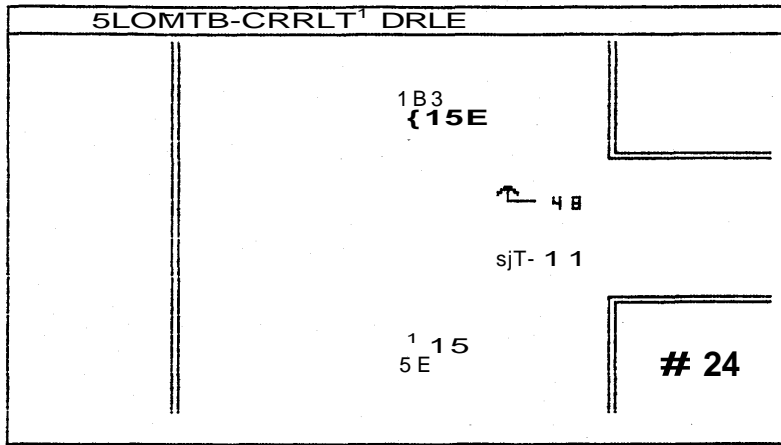


EXISTING INTERSECTION TRAFFIC
P.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC

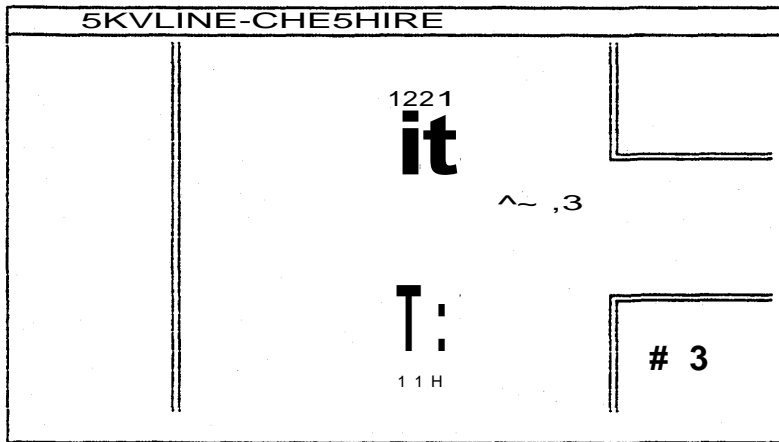
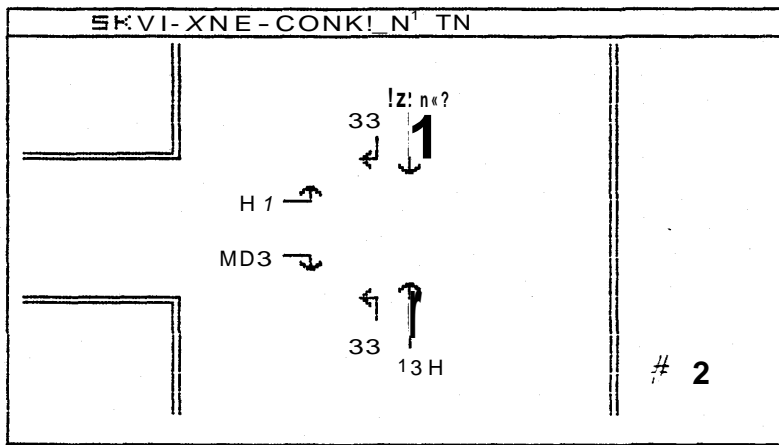
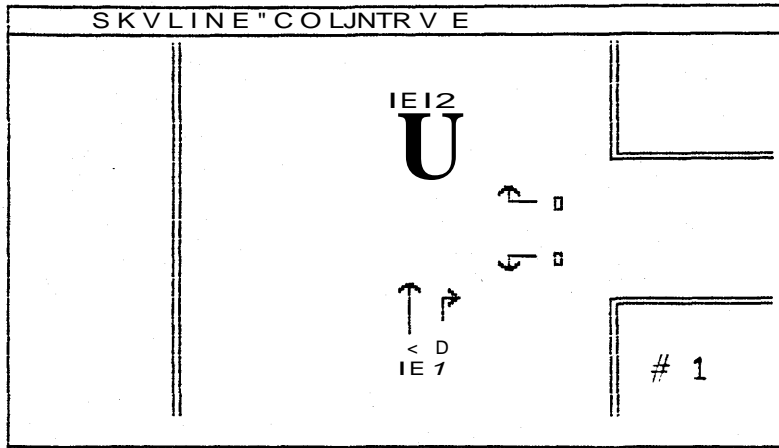
P.M. PEAK HOUR



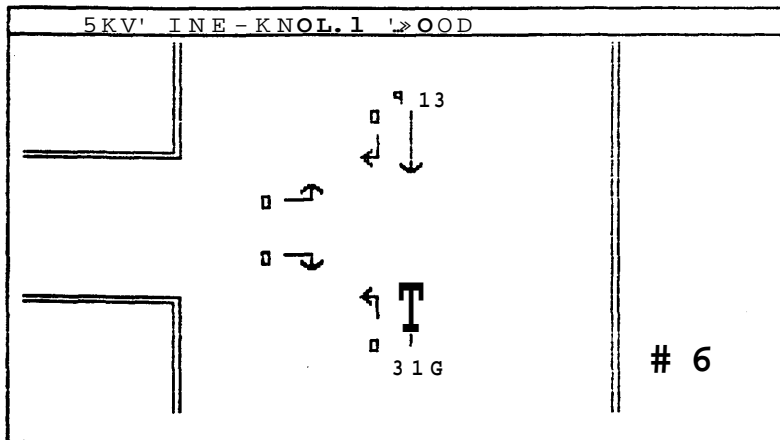
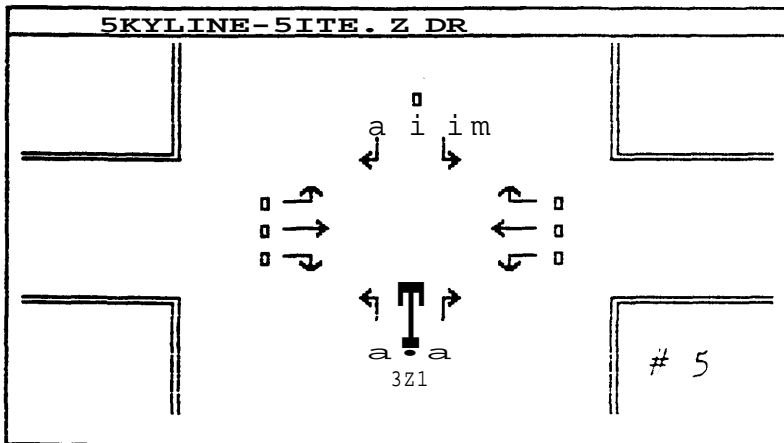
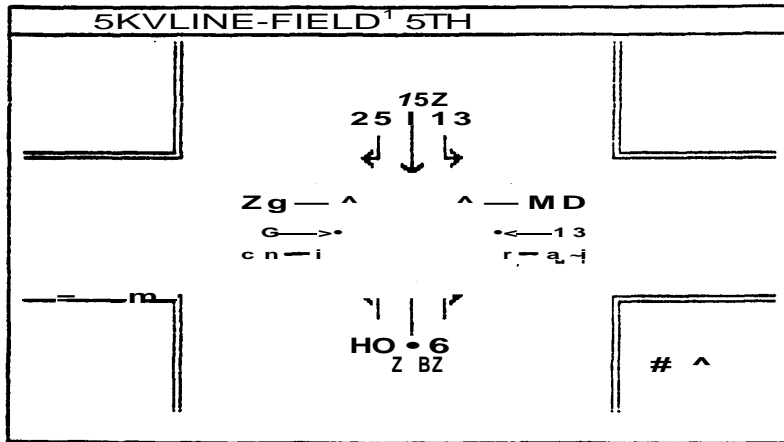
1983 BACKGROUND TRAFFIC

A/M. PEAK HOUR 1993 TRAFFIC VOLUMES

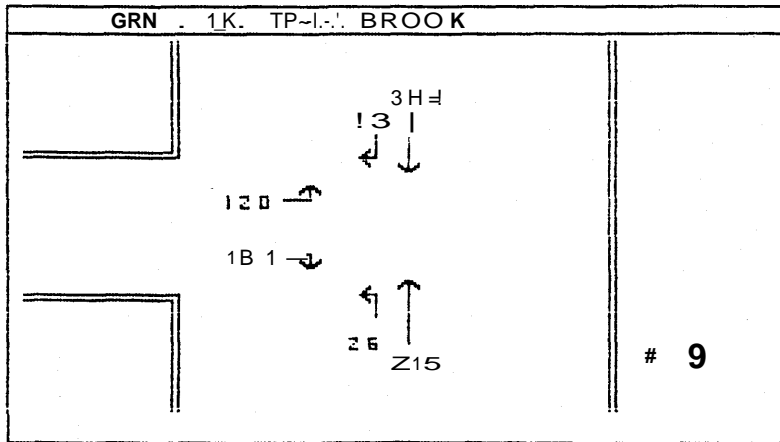
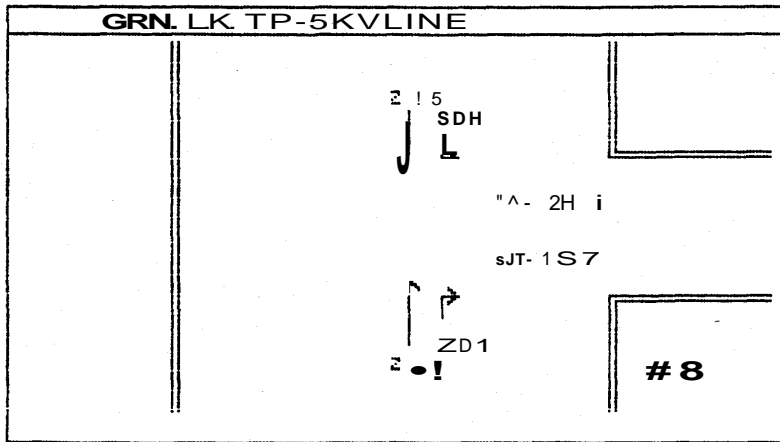
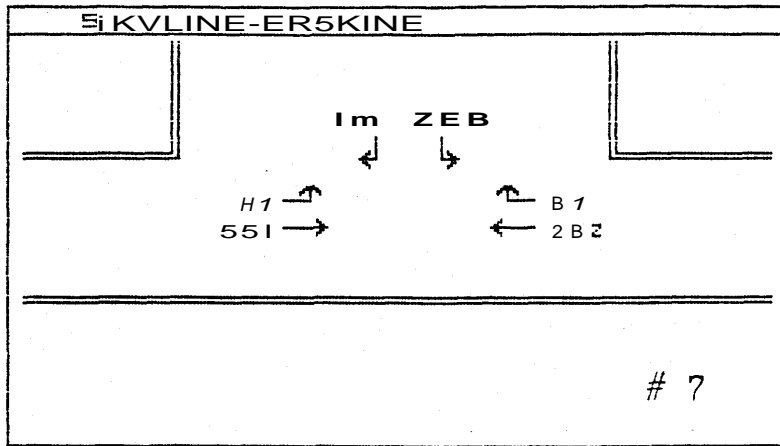
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 A.M. PEAK HOUR



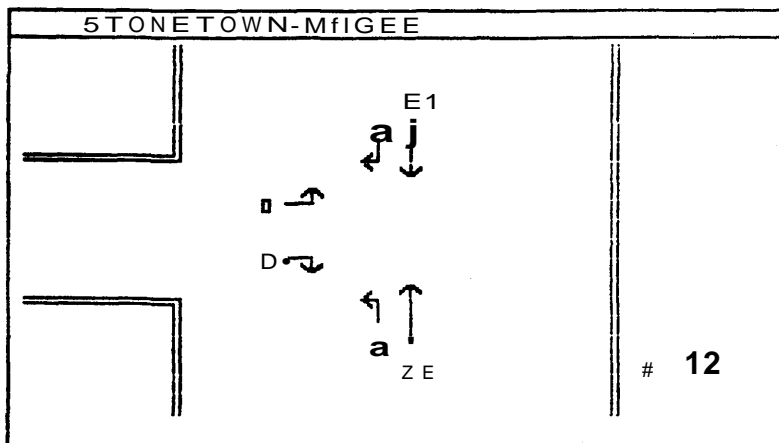
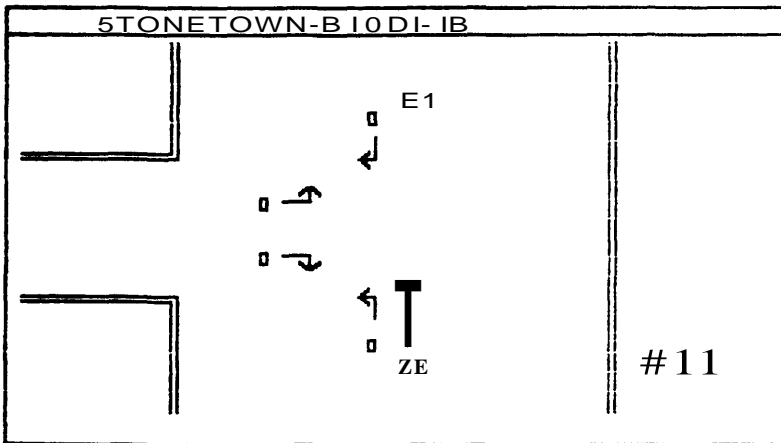
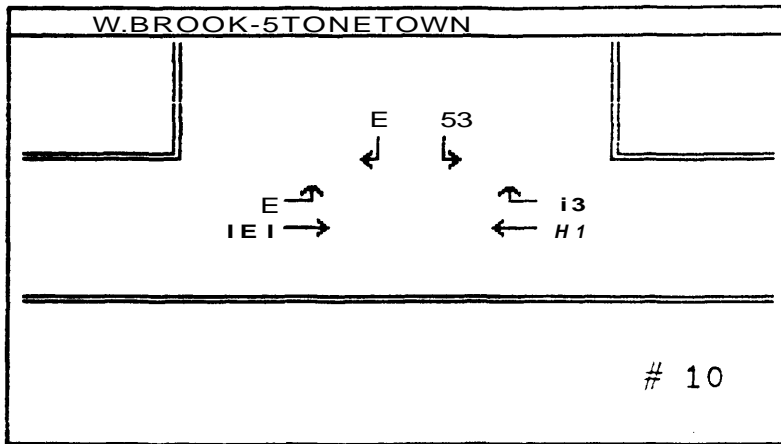
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 A.M. PEAK HOUR



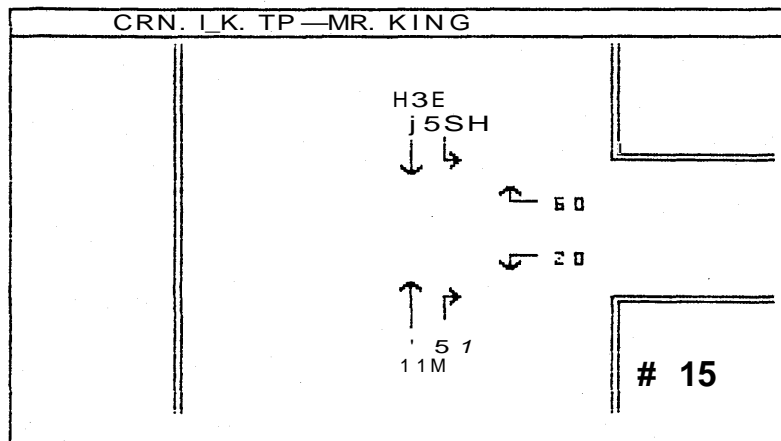
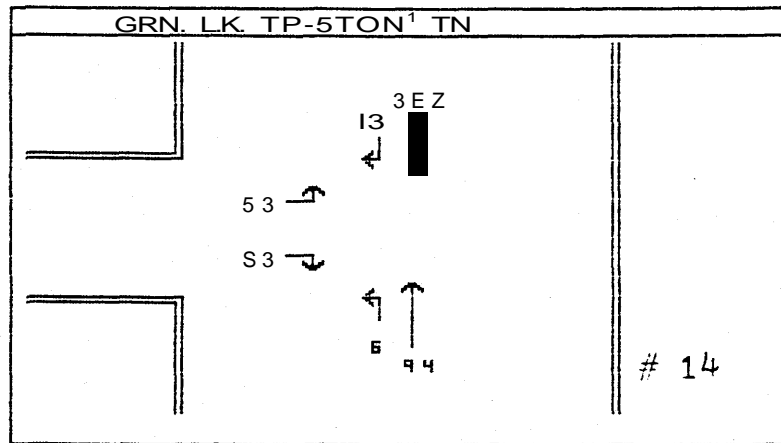
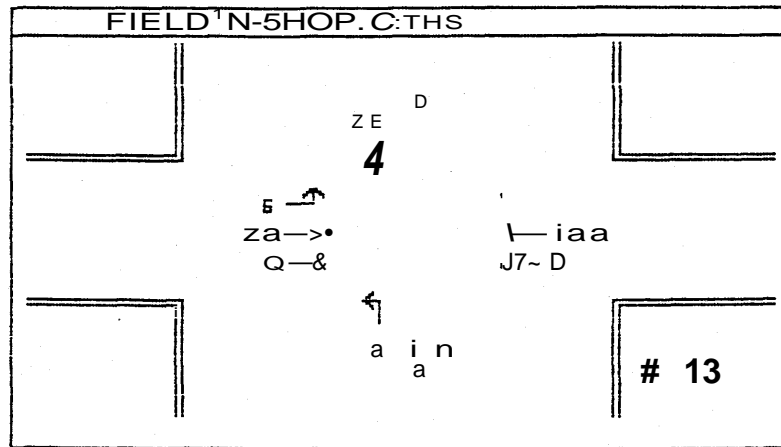
LISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 A.M. PEAK HOUR



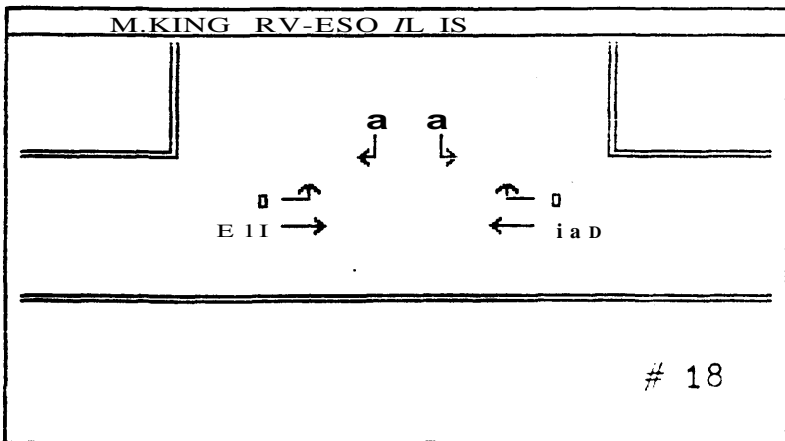
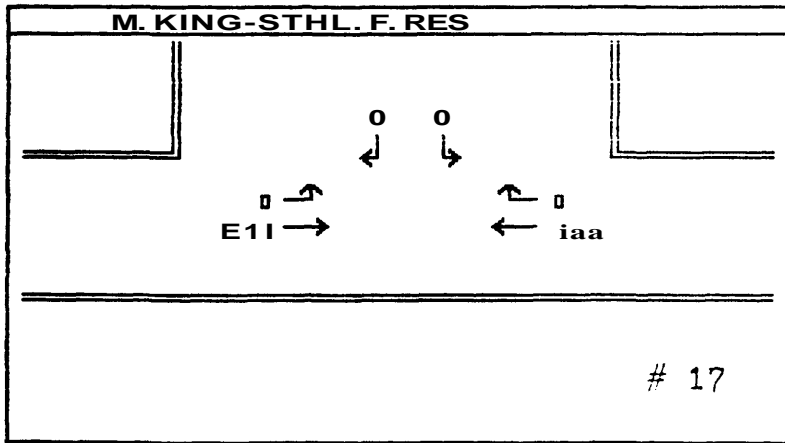
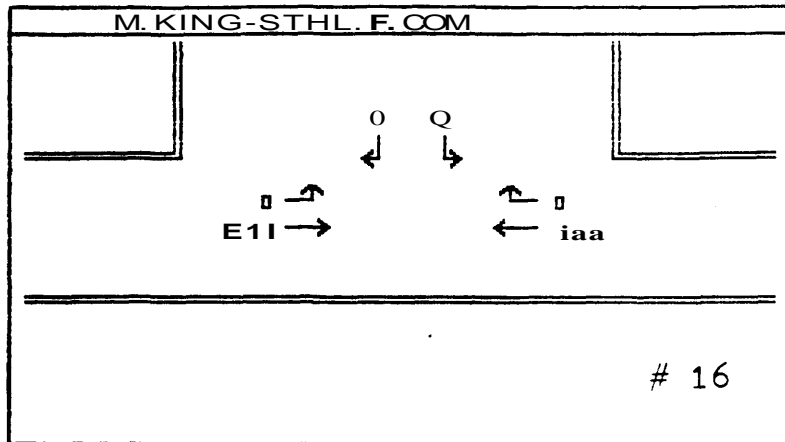
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 A.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 A.M. PEAK HOUR

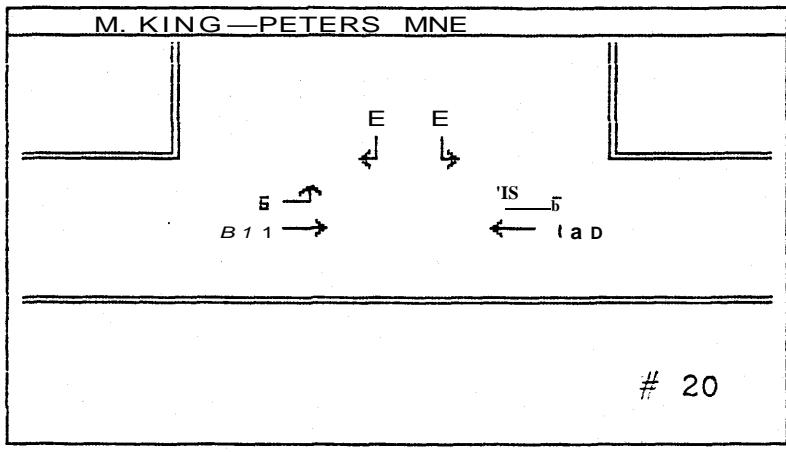
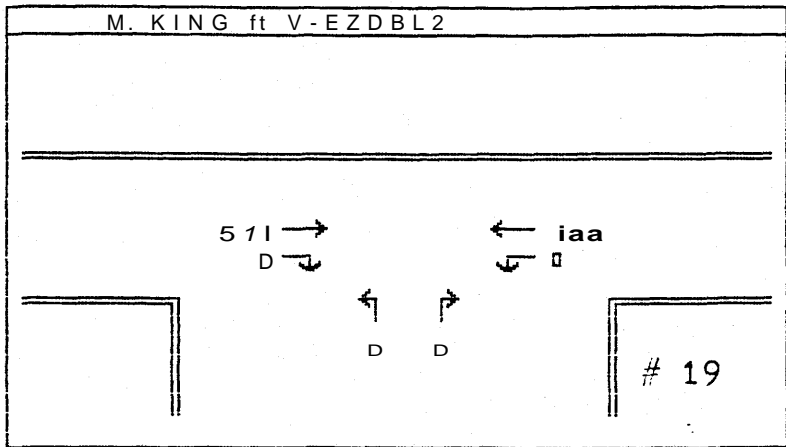


EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
A.M. PEAK HOUR

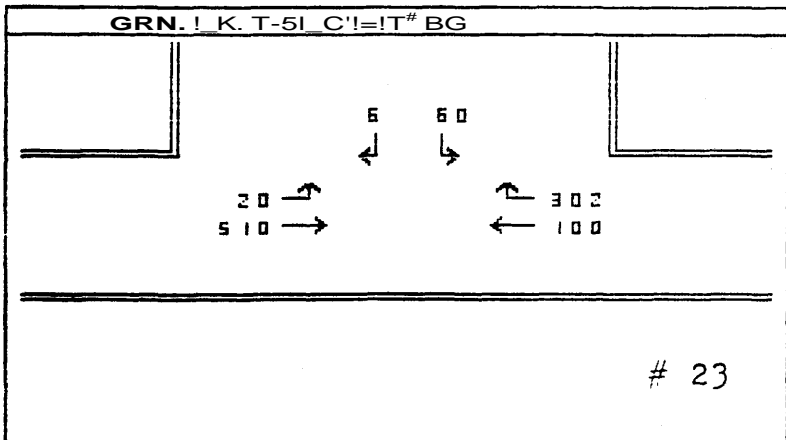
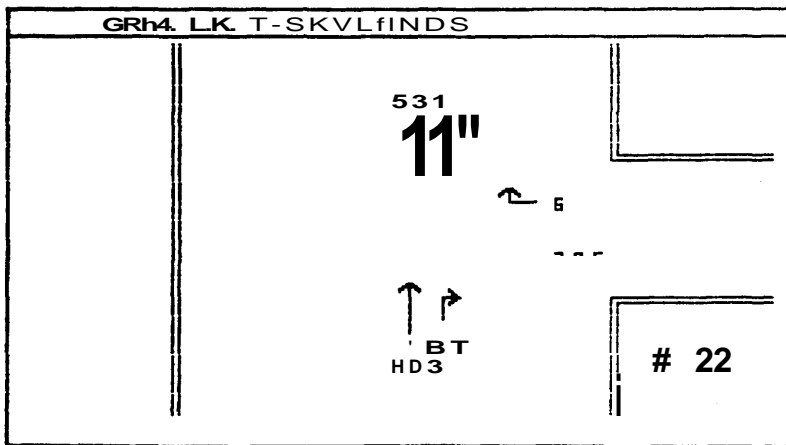
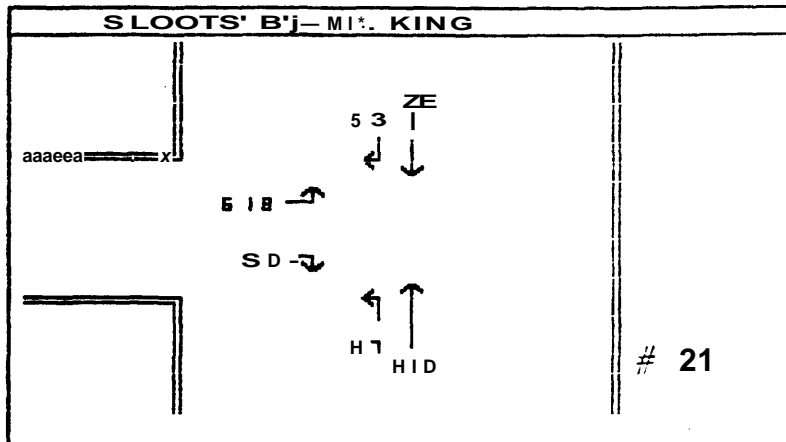


EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS

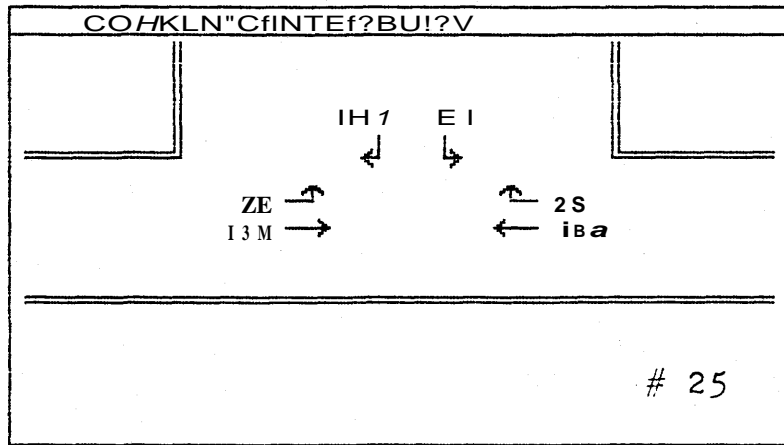
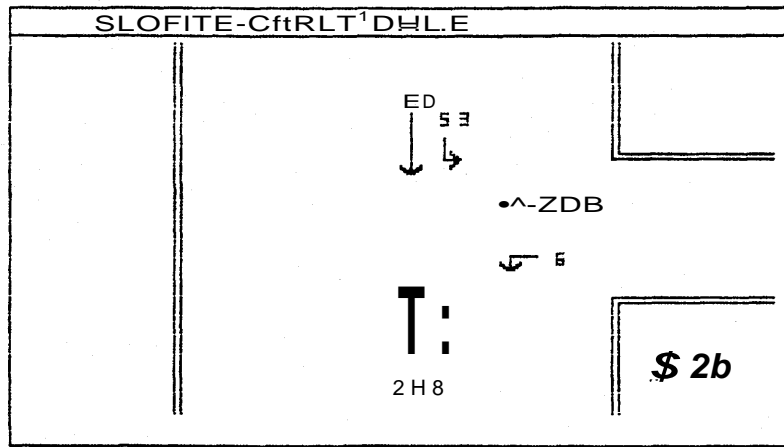
A.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 A.M. PEAK HOUR



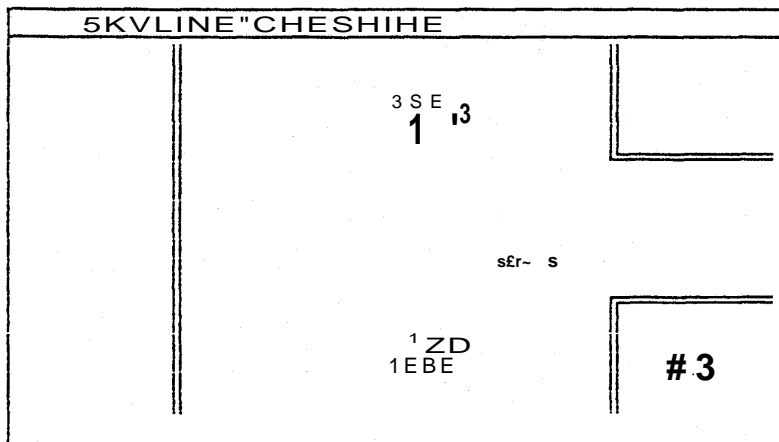
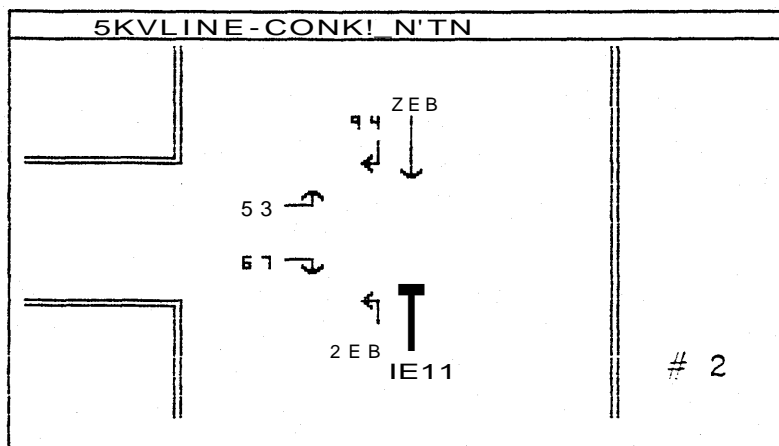
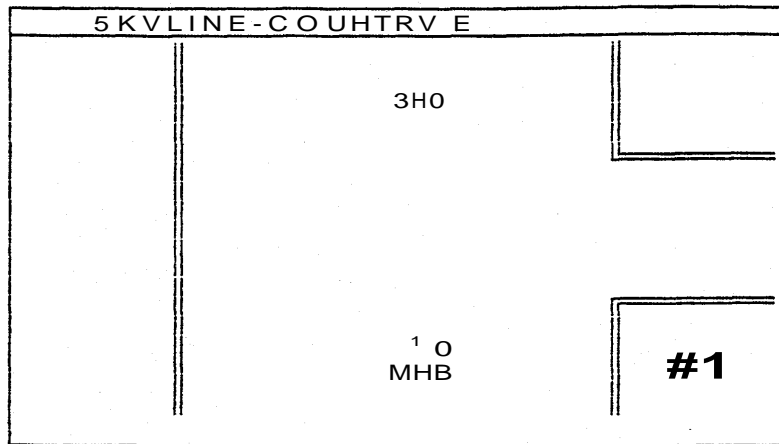
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
A.M. PEAK HOUR



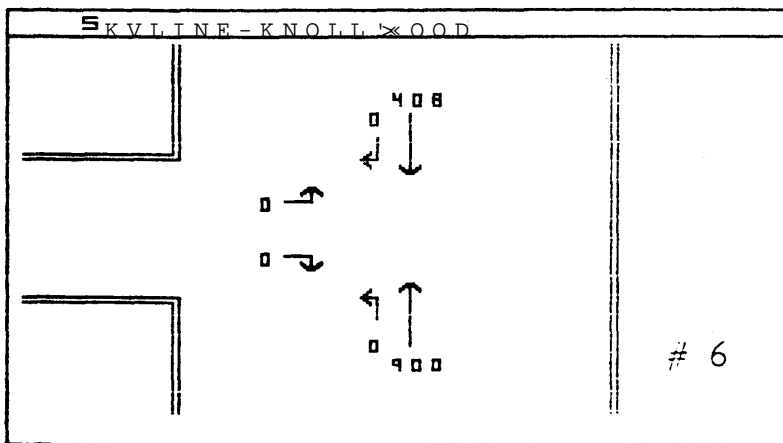
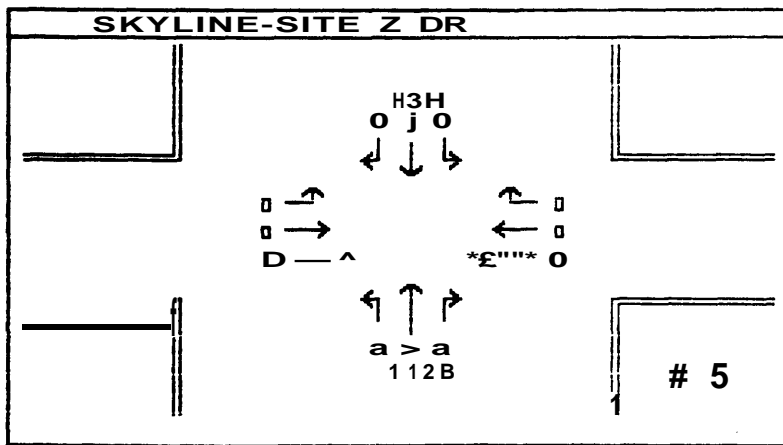
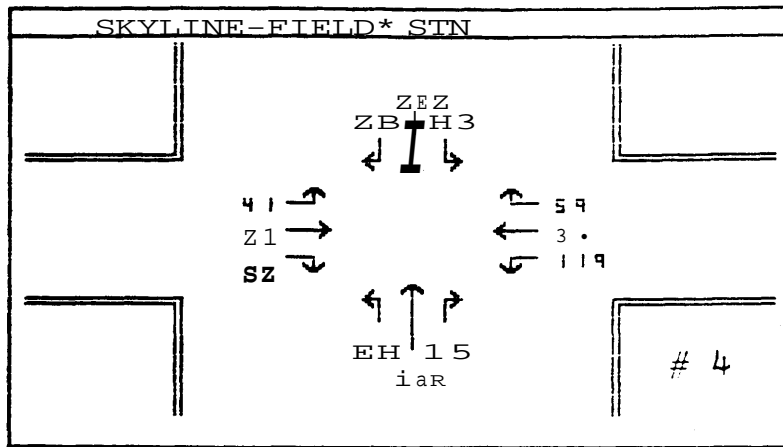
1983 BACKGROUND TRAFFIC

P.M. PEAK HOUR 1993 TRAFFIC VOLUMES

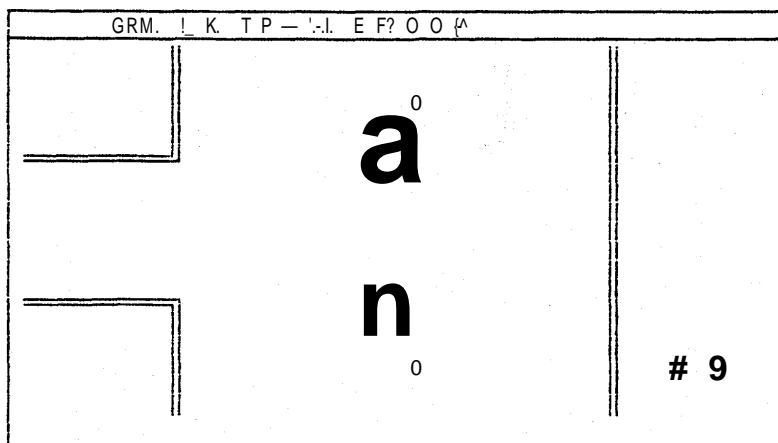
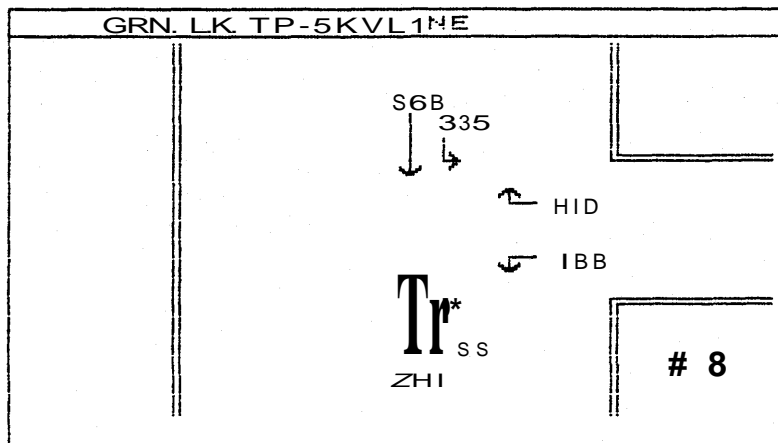
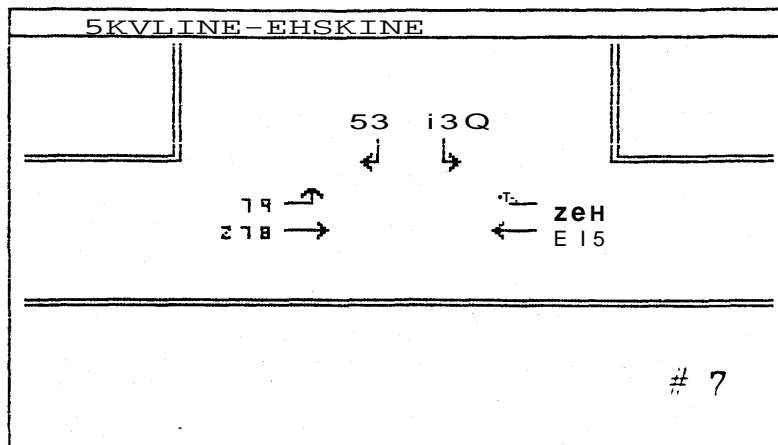
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
P.M. PEAK HOUR



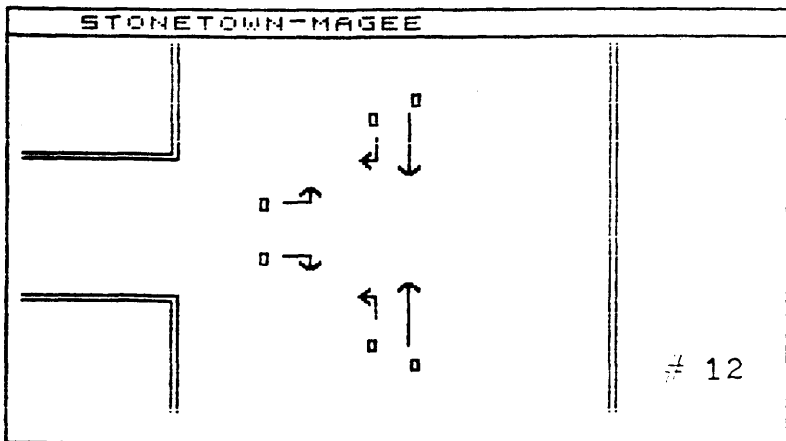
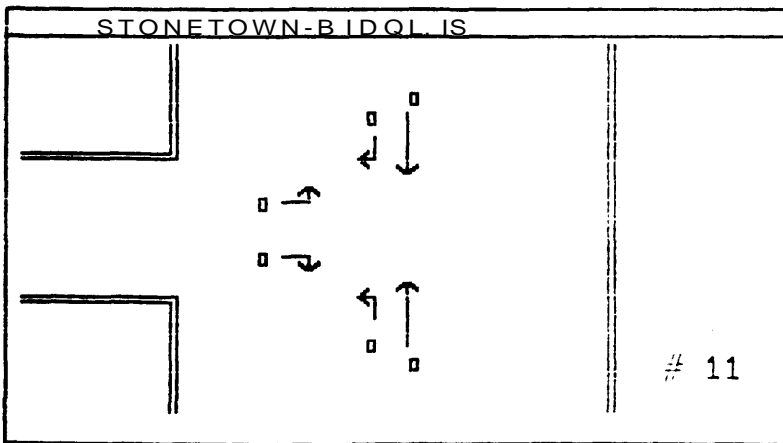
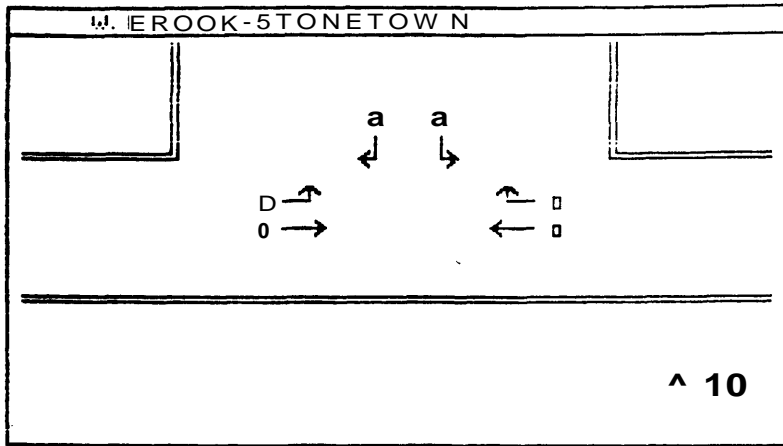
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3f*/YR FOR 10 YEARS
P.M. PEAK HOUR



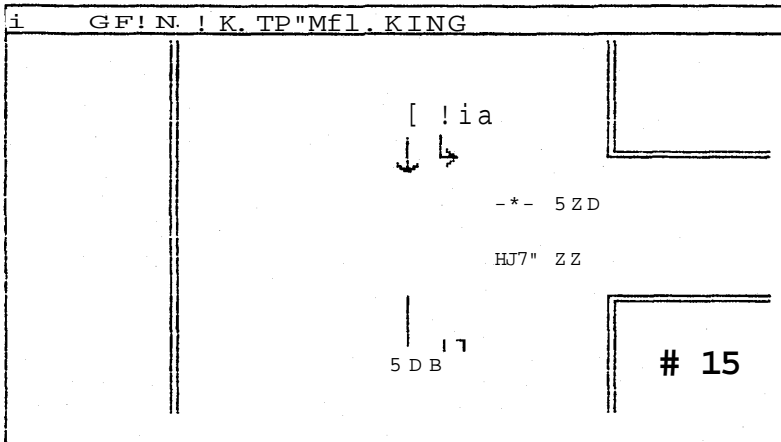
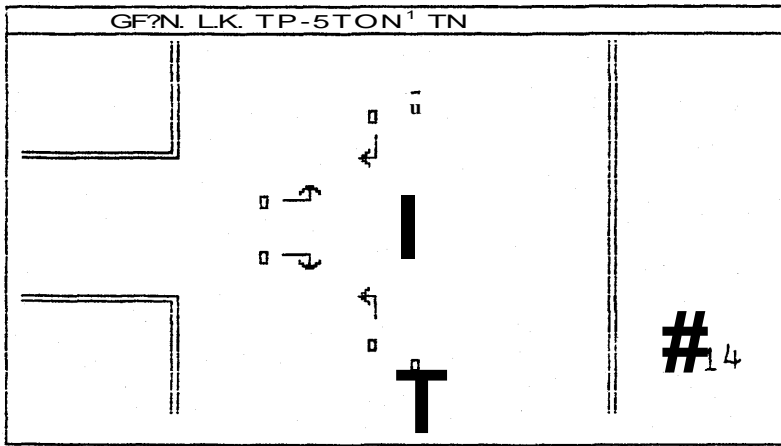
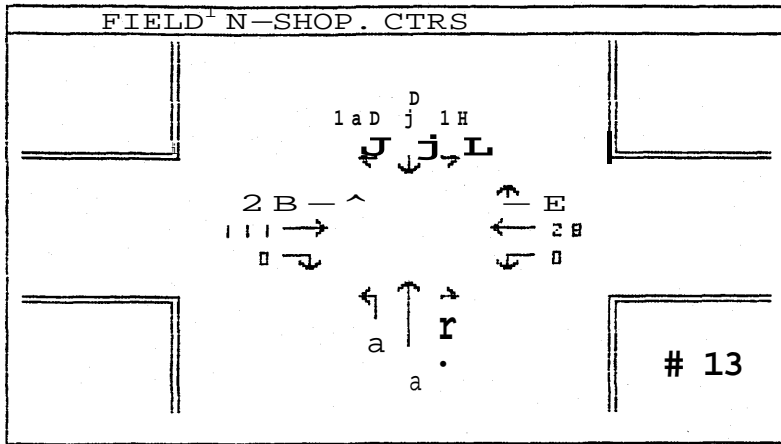
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
P.M. PEAK HOUR



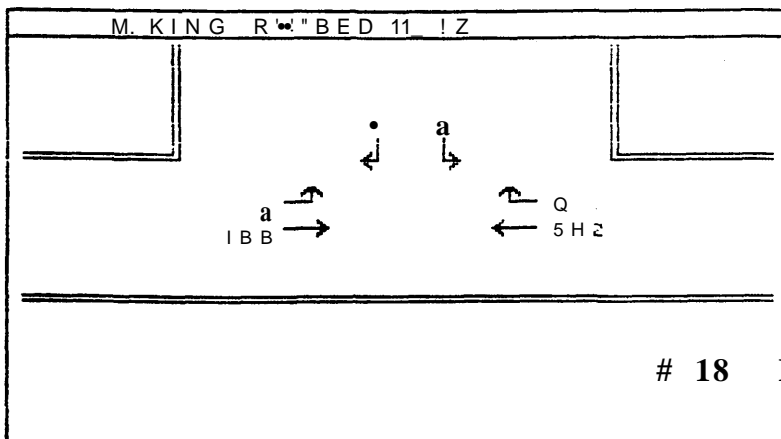
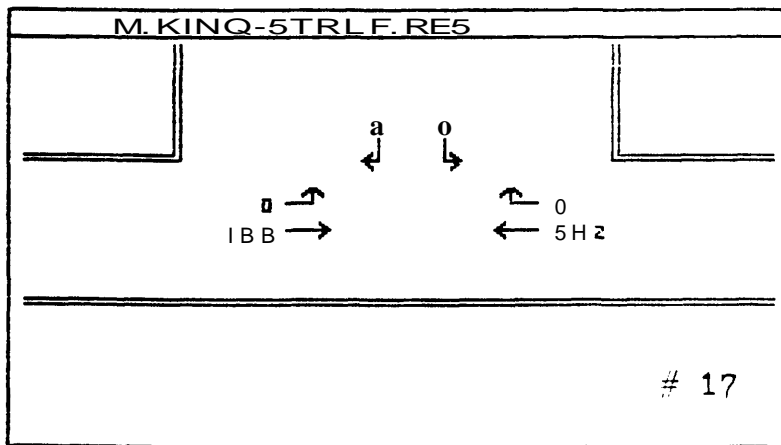
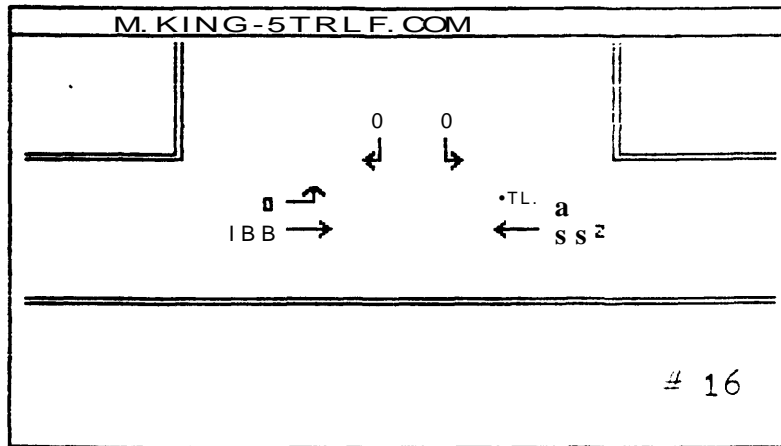
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
P.M. PEAK HOUR



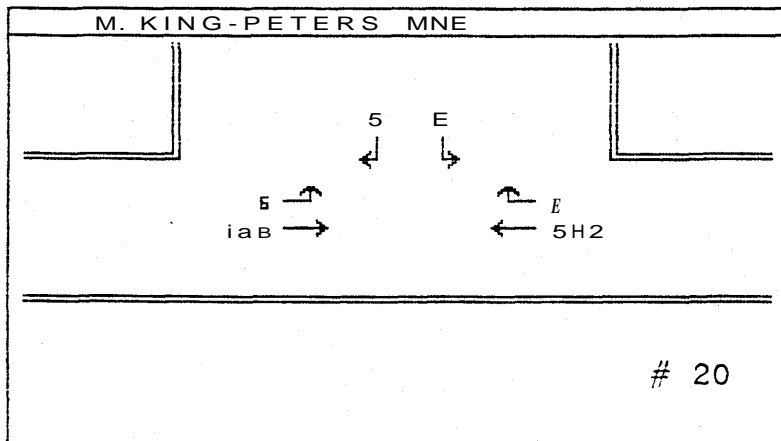
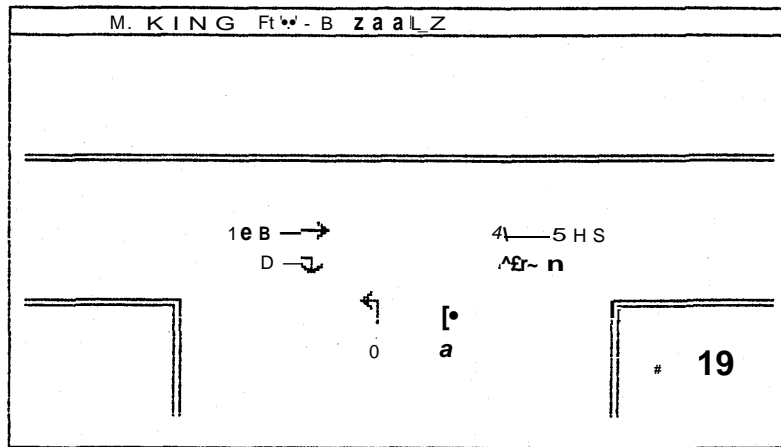
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
P.M. PEAK HOUR



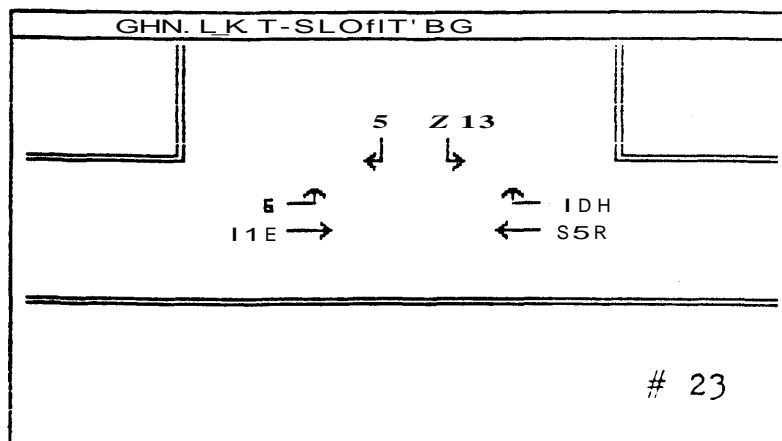
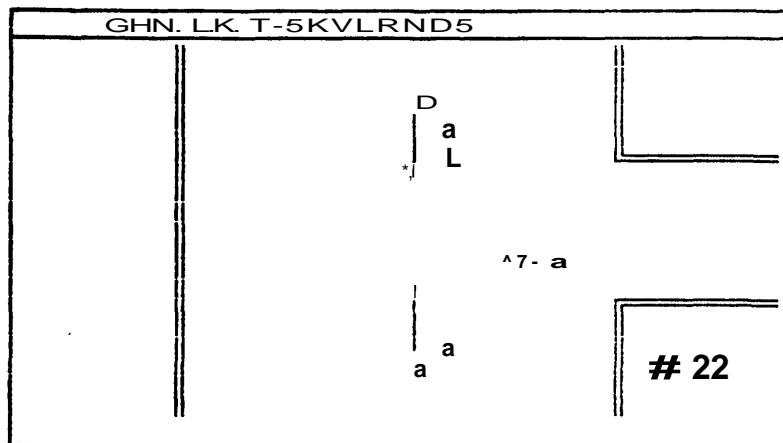
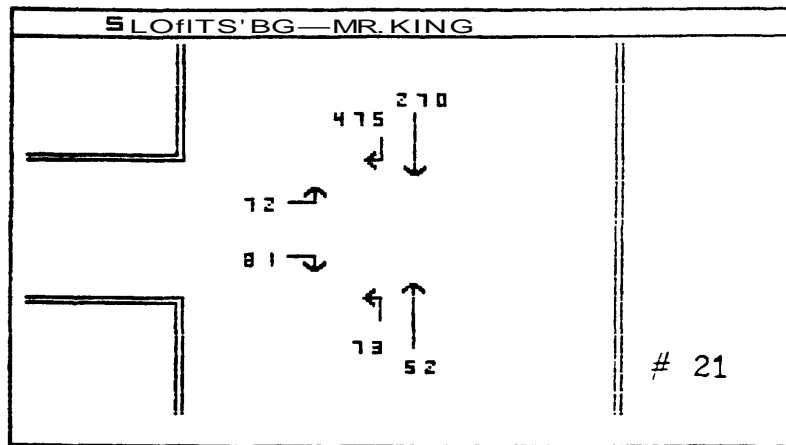
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/Y?, FOR 10 YEARS
P.M. PEAK HOUR



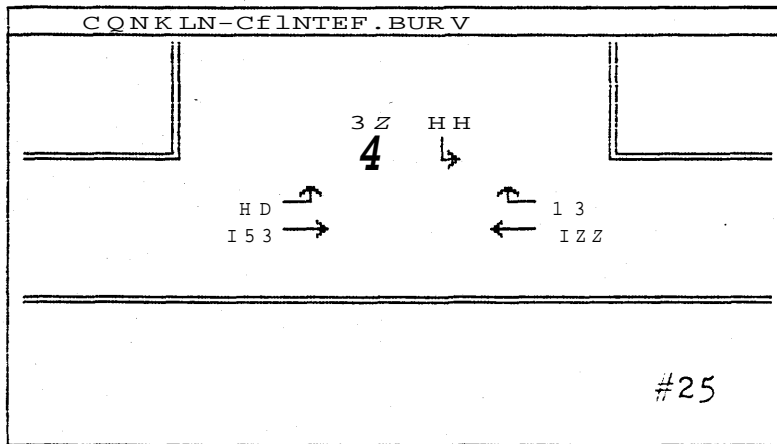
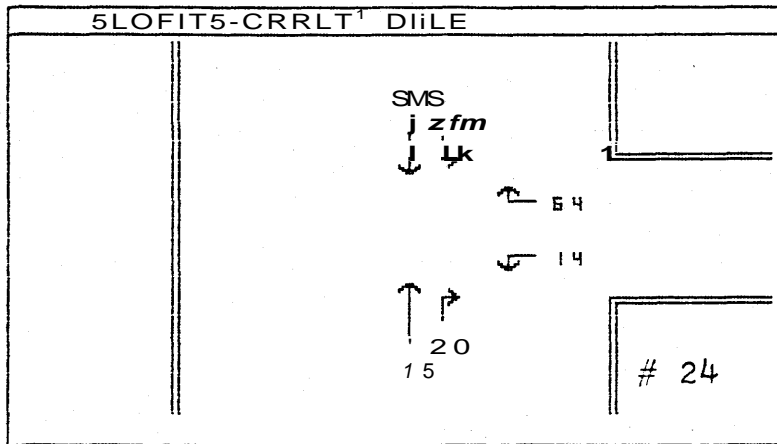
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
P.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDE AT 3%/YR FOR 10 YEARS
P.M. PEAK HOUR



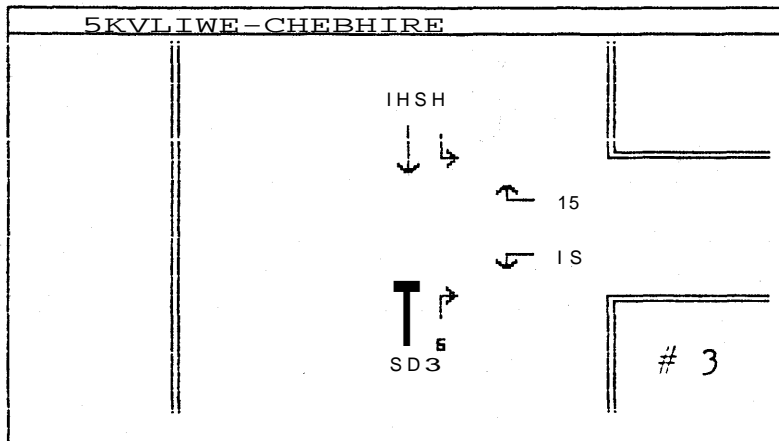
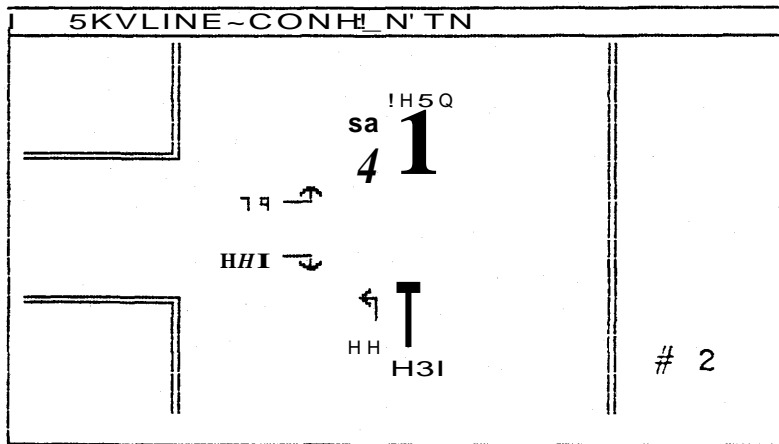
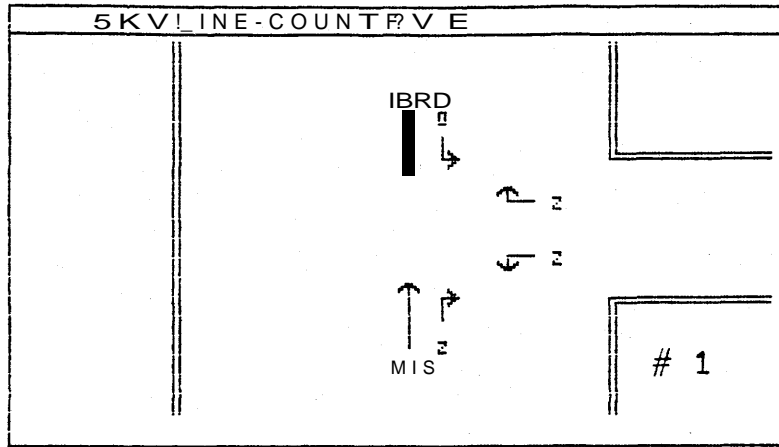
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
P.M. PEAK HOUR



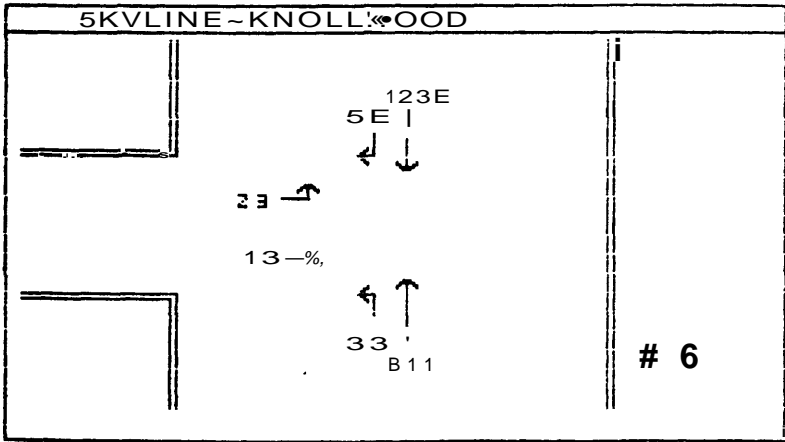
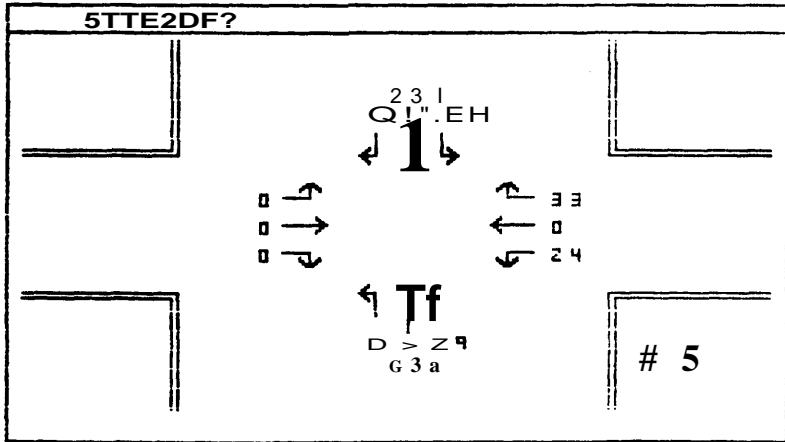
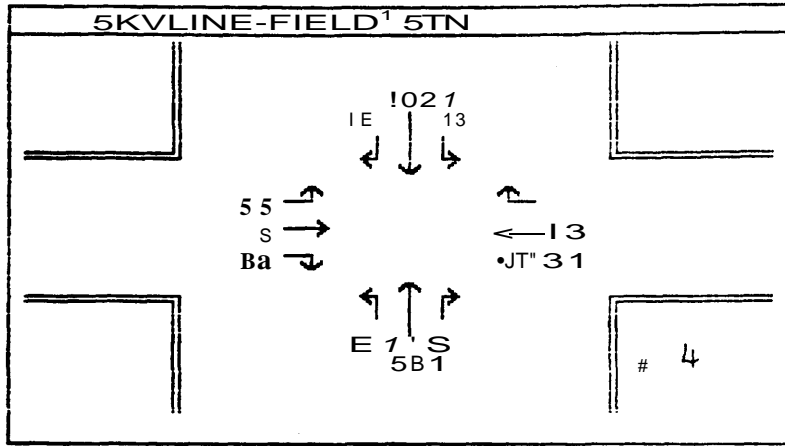
1993 BACKGROUND TRAFFIC AND SITE TRAFFIC

A.M. RESULTING TRAFFIC VOLUMES
WITH
STUDY SITES DEVELOPED AS ZONED

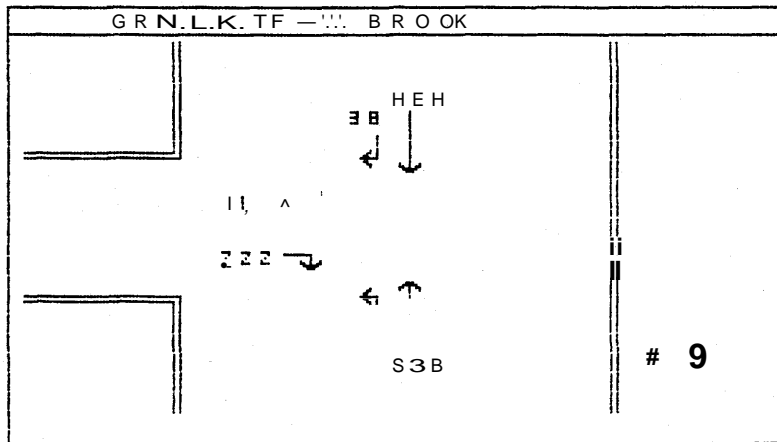
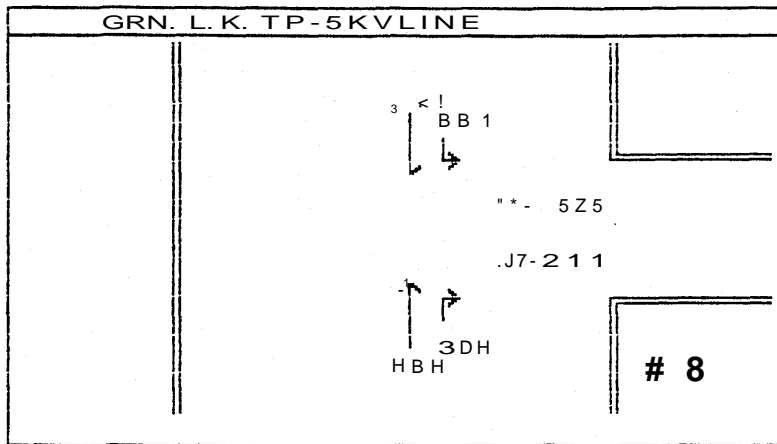
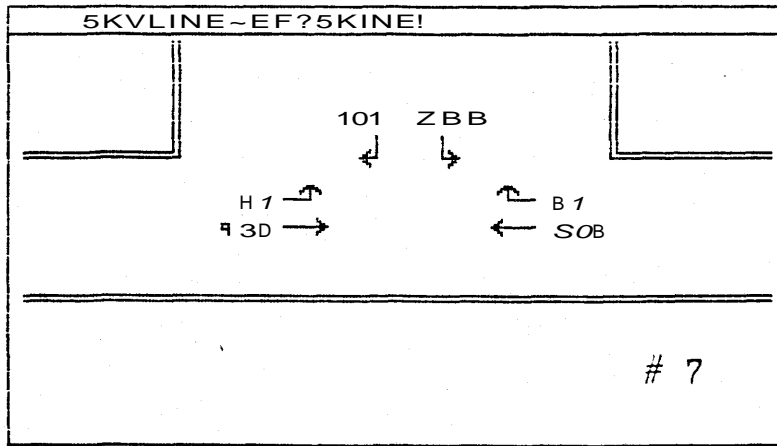
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



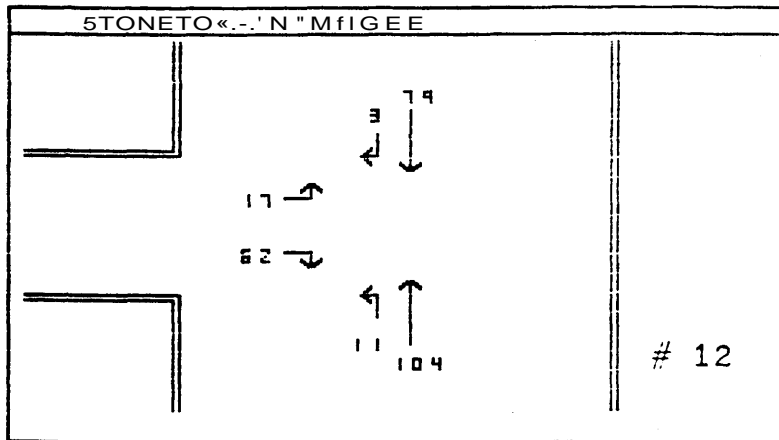
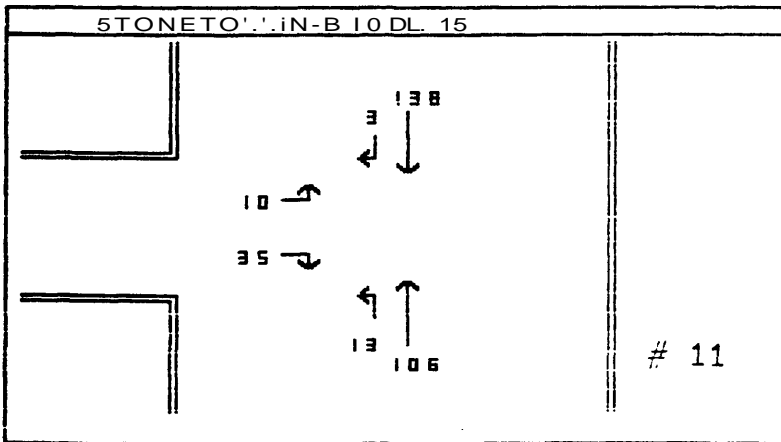
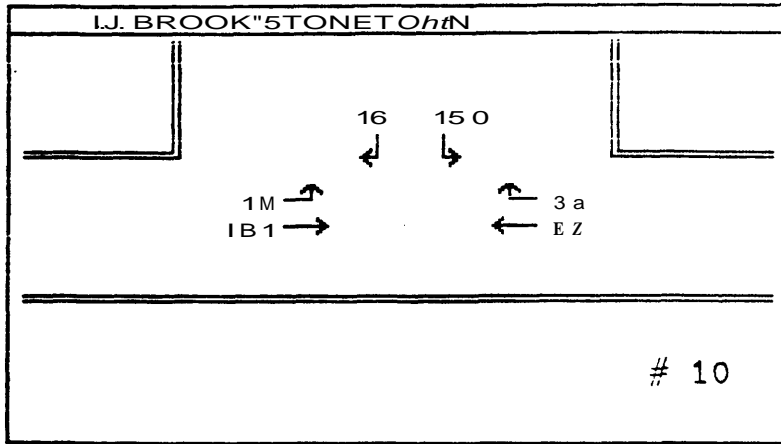
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%^c/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



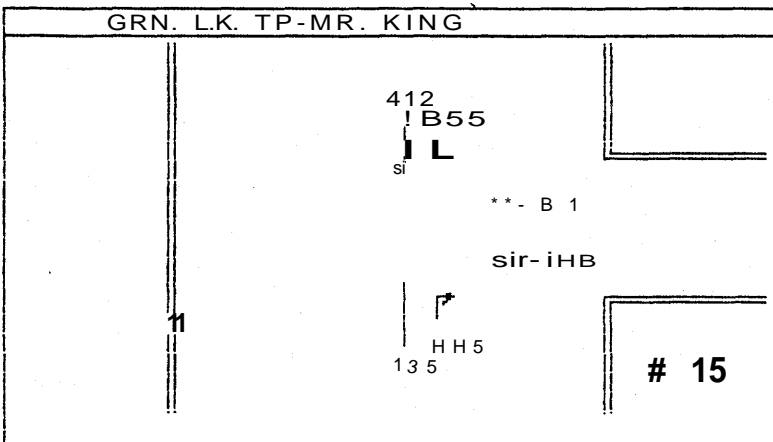
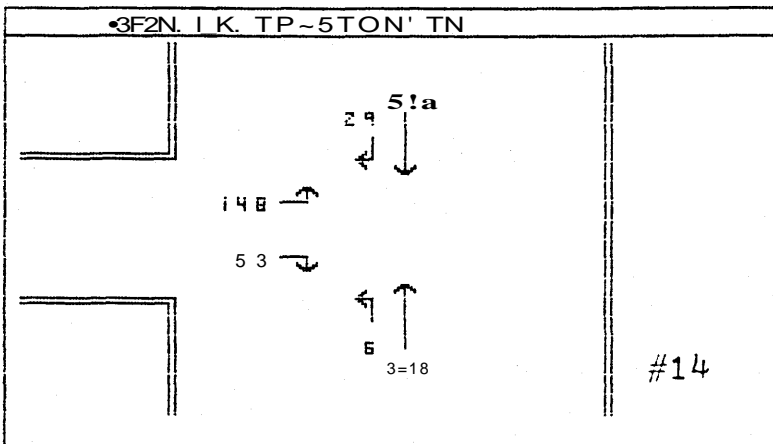
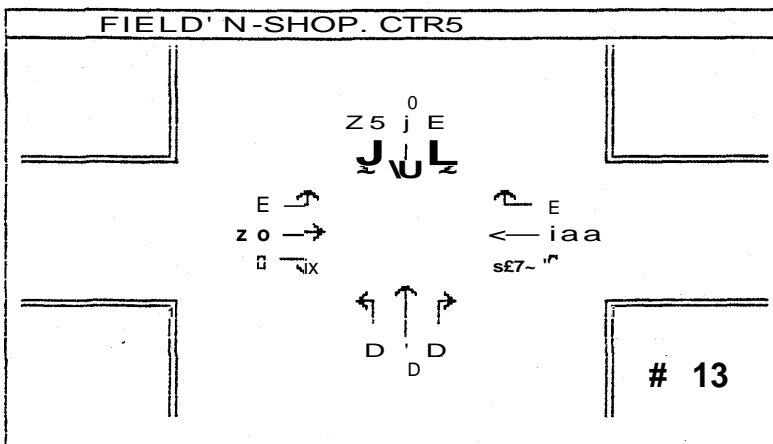
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



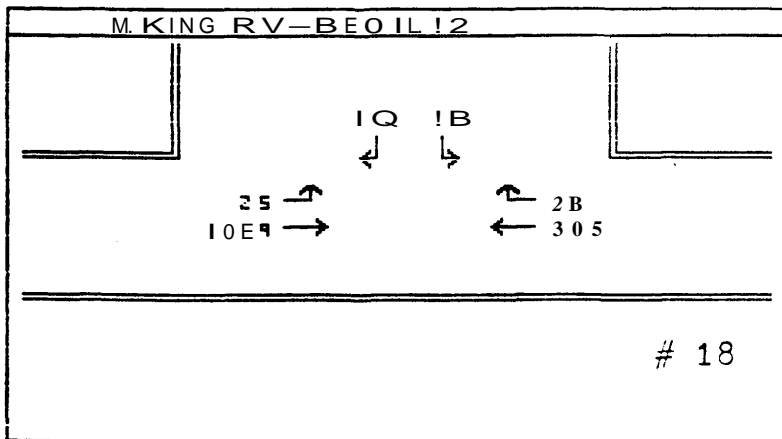
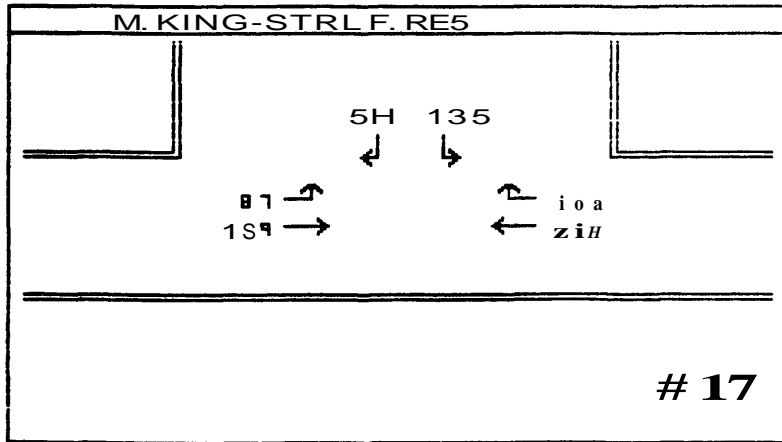
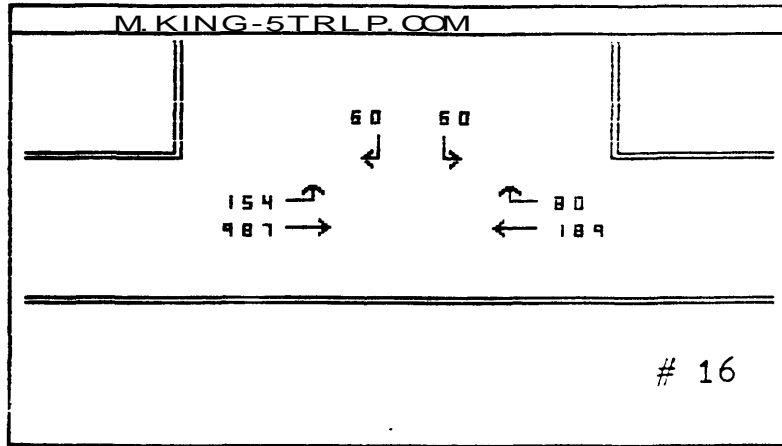
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED..
 A.M. PEAK HOUR



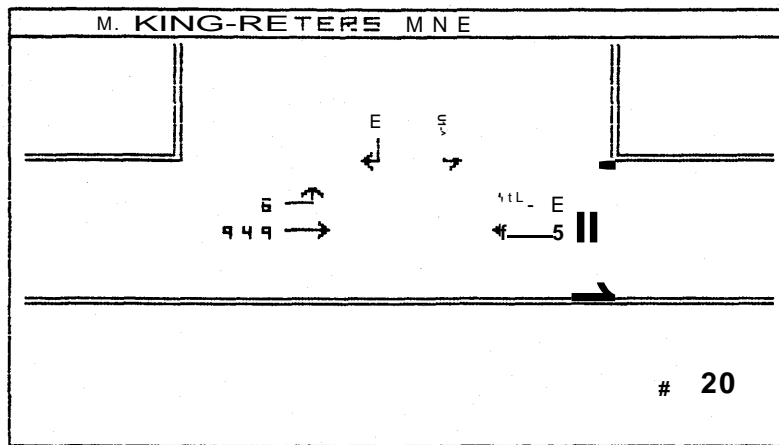
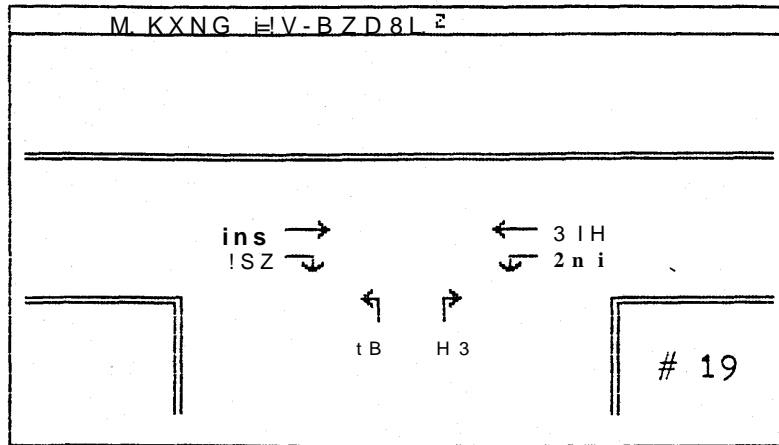
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



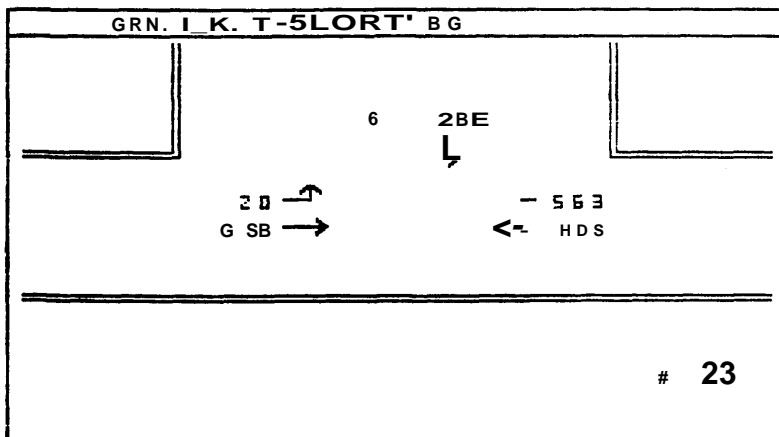
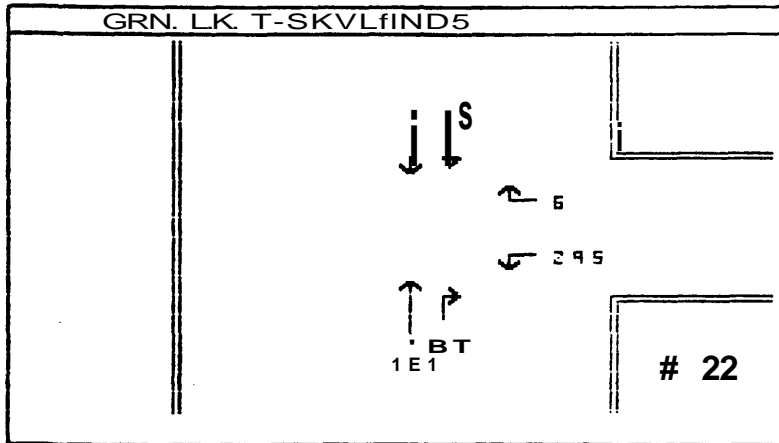
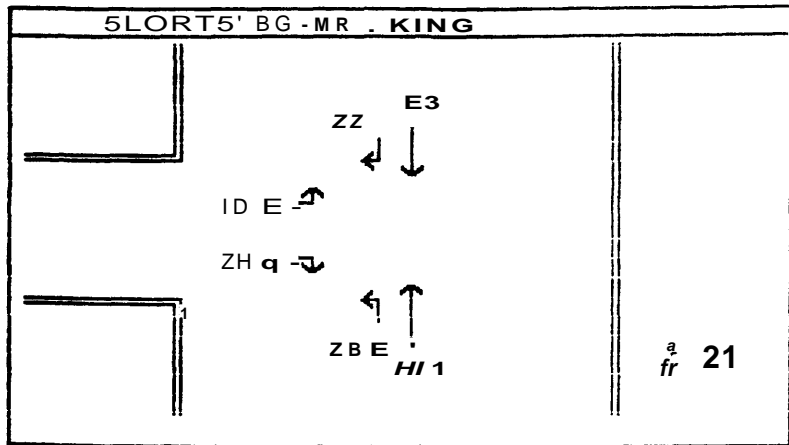
EXISTING INTERSECTION TRAFFIC EXPANDED AT *Jfo/YR* FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



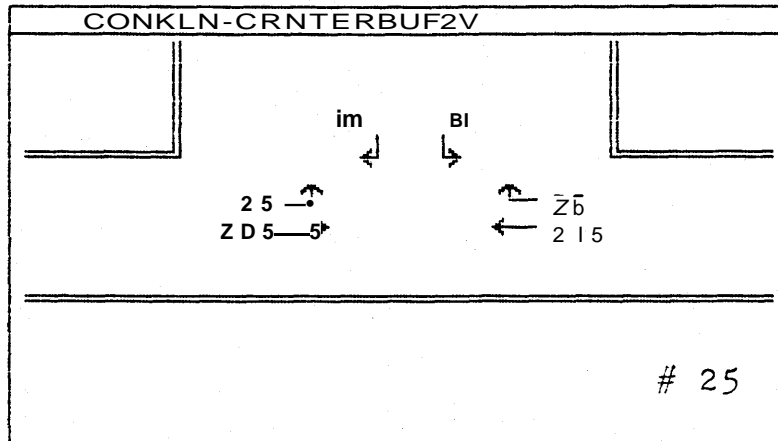
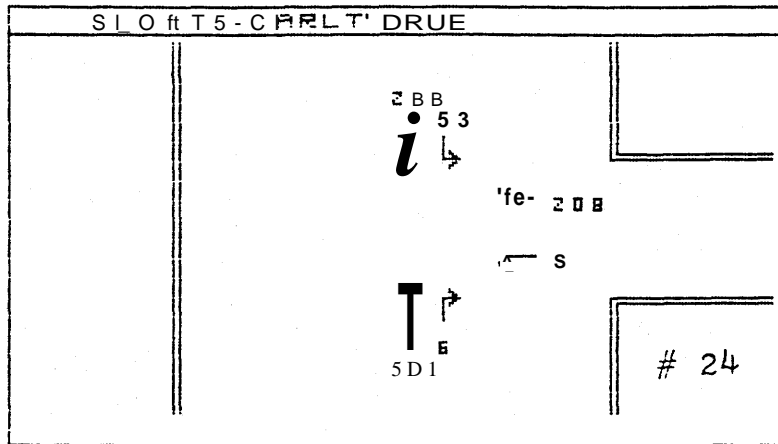
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



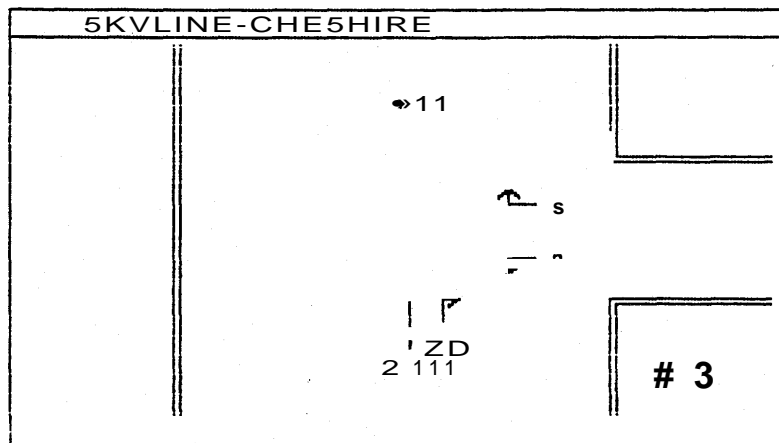
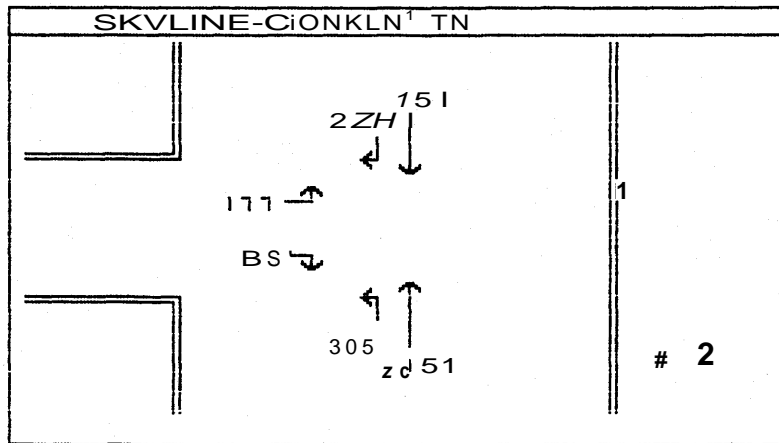
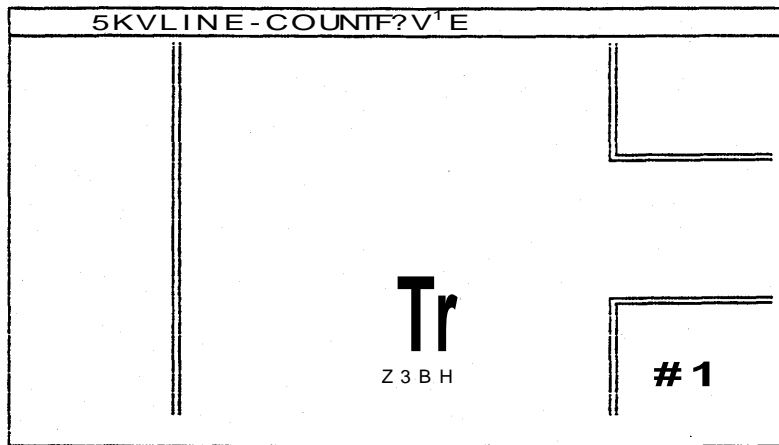
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3[^]/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



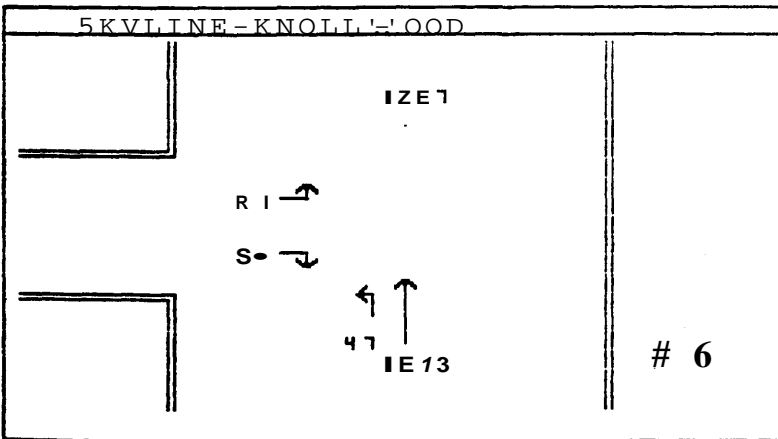
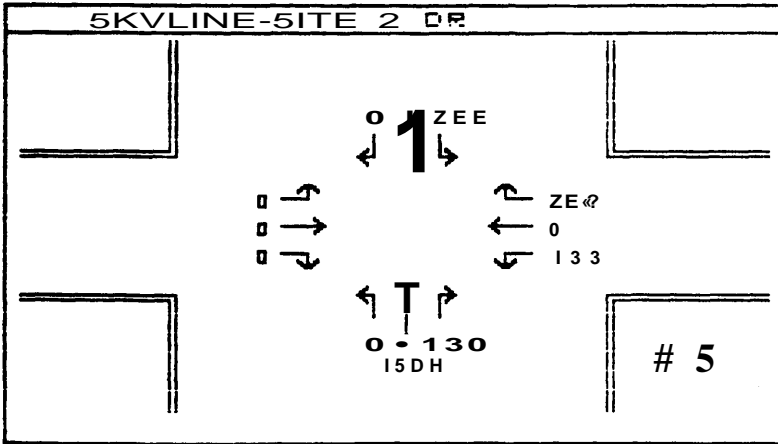
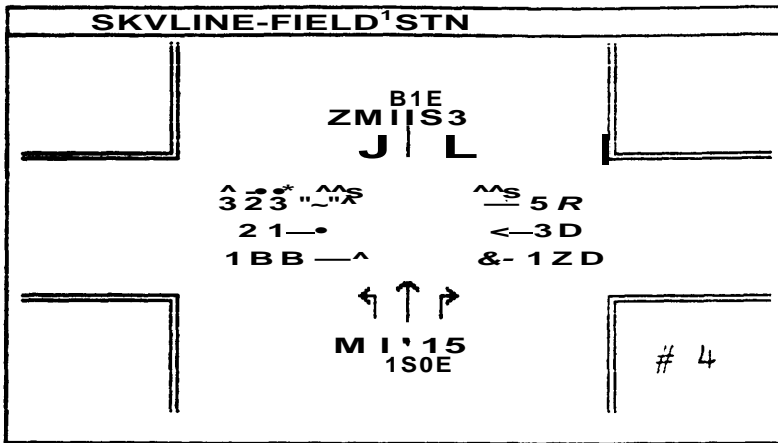
1003 BACKGROUND TRAFFIC AND SITE TRAFFIC

P.M. RESULTING TRAFFIC VOLUMES
WITH
STUDY SITES DEVELOPED AS ZONED

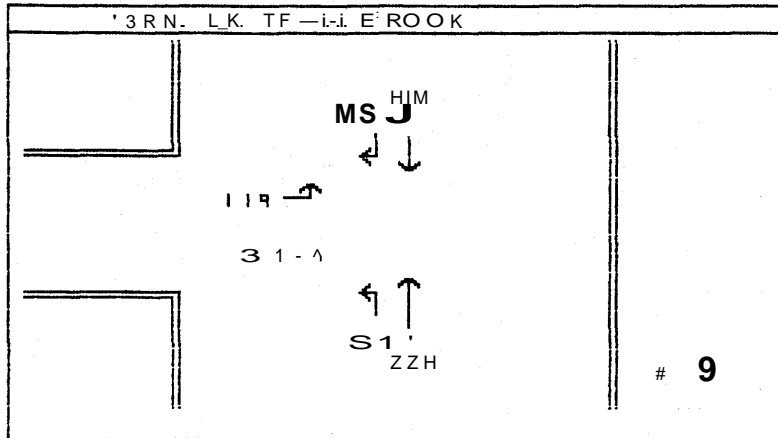
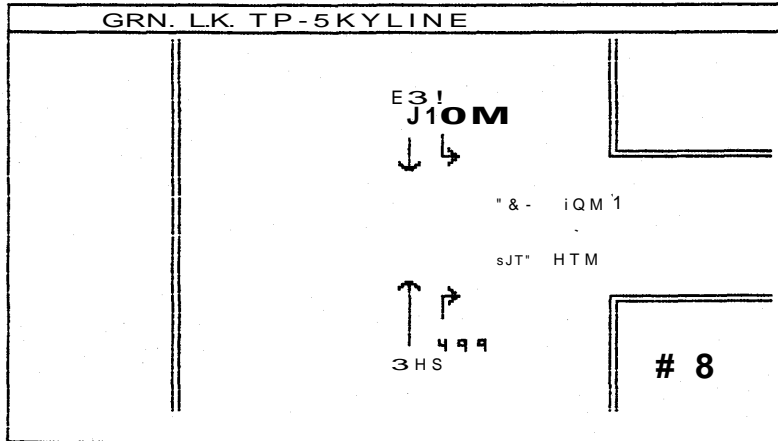
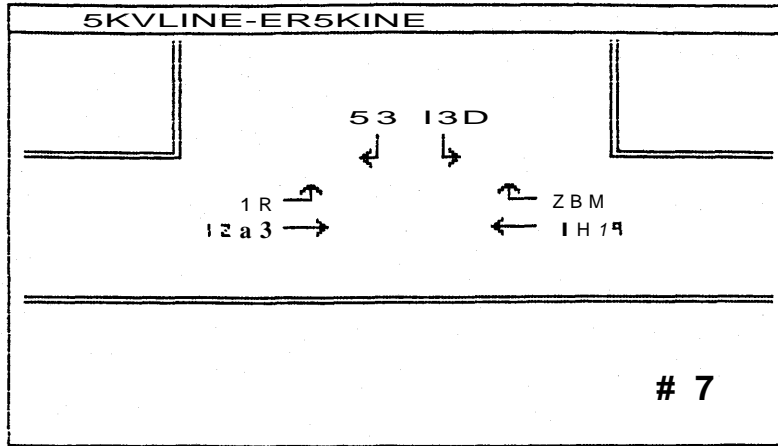
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/XR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR

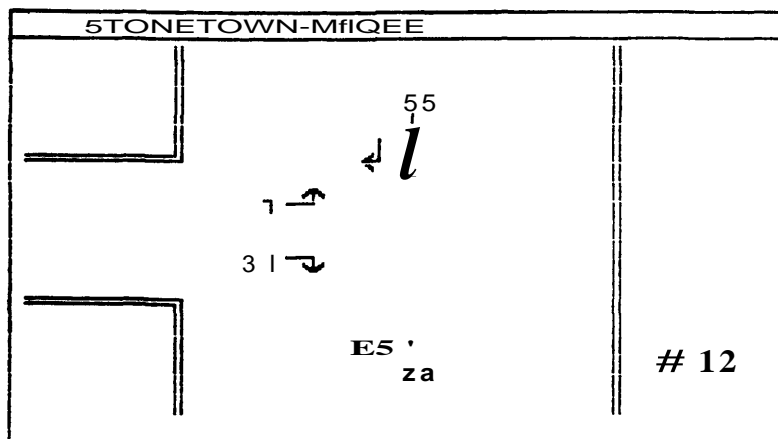
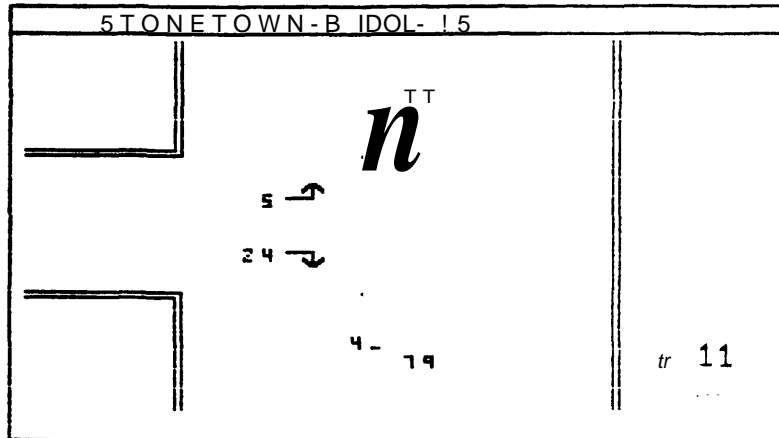
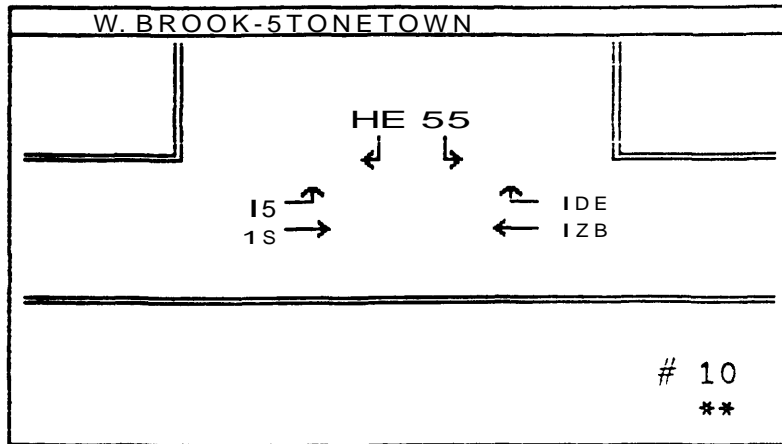


EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR



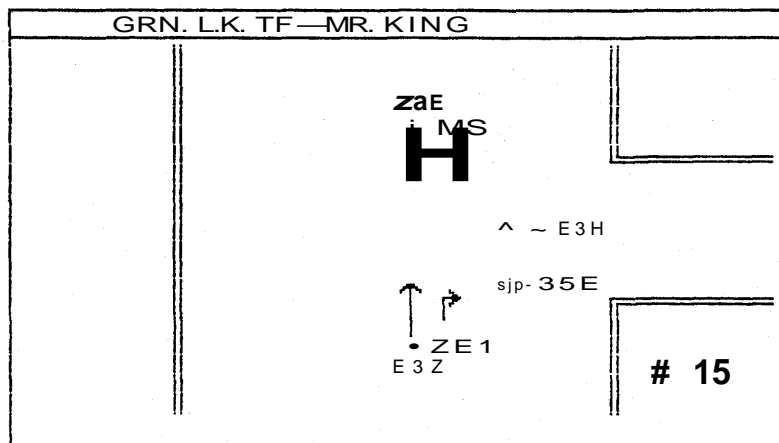
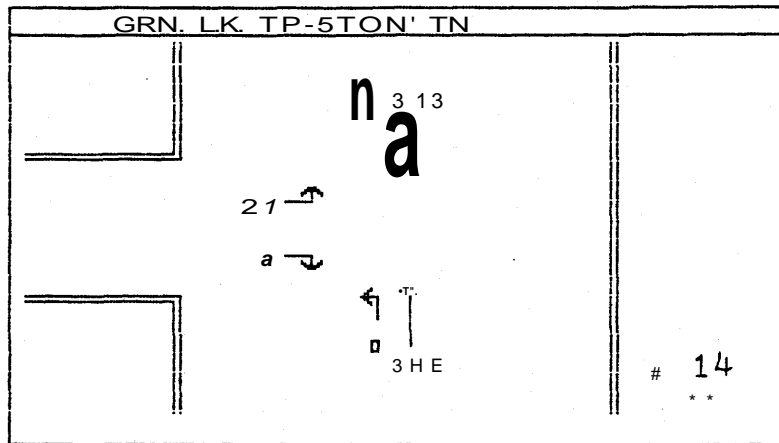
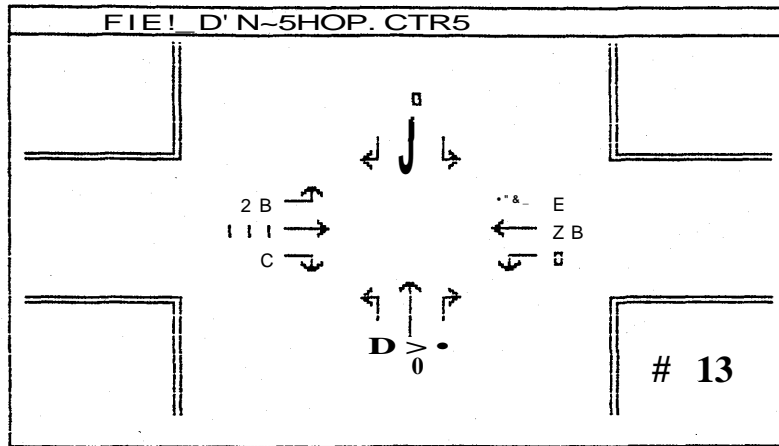
** NEW TRAFFIC ONLY

EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR



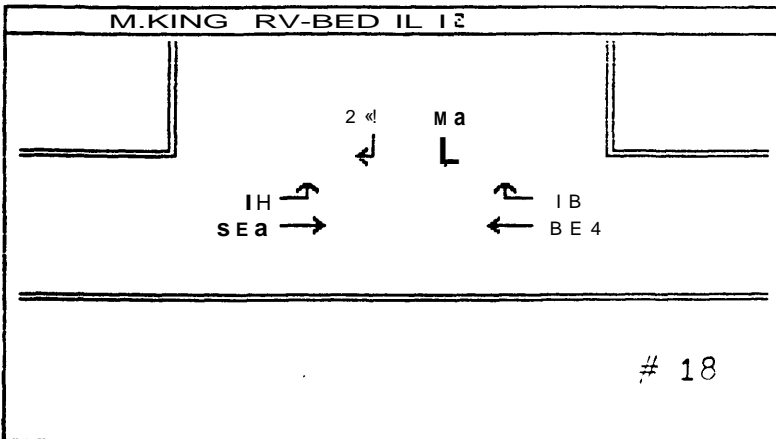
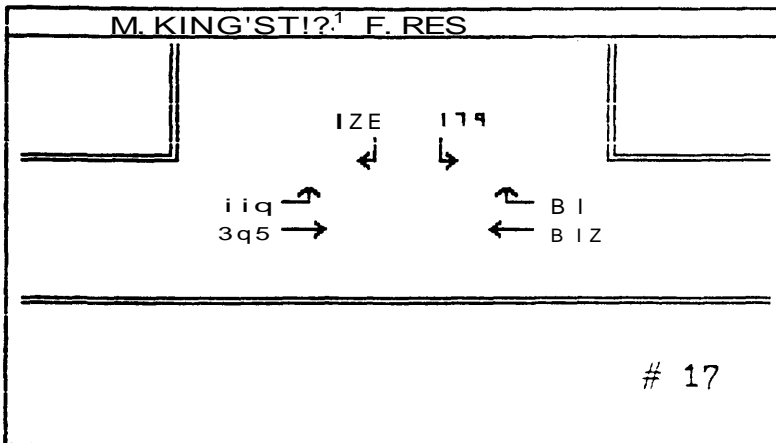
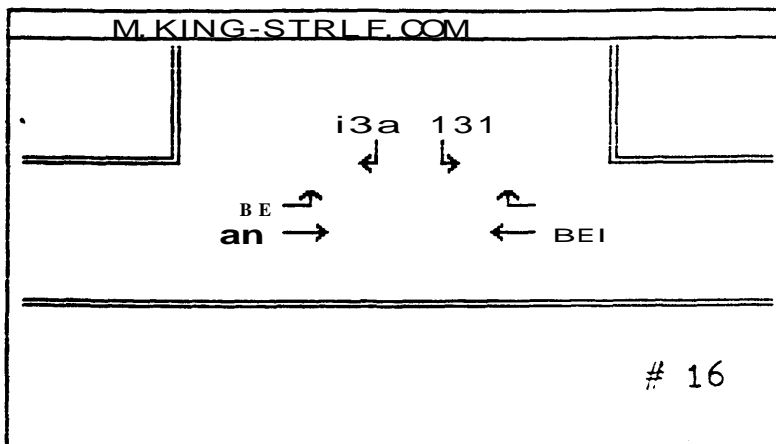
•• NEW TRAFFIC ONLY

EXISTING INTERSECTION TRAFFIC EXPANDED AT 3fo/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR

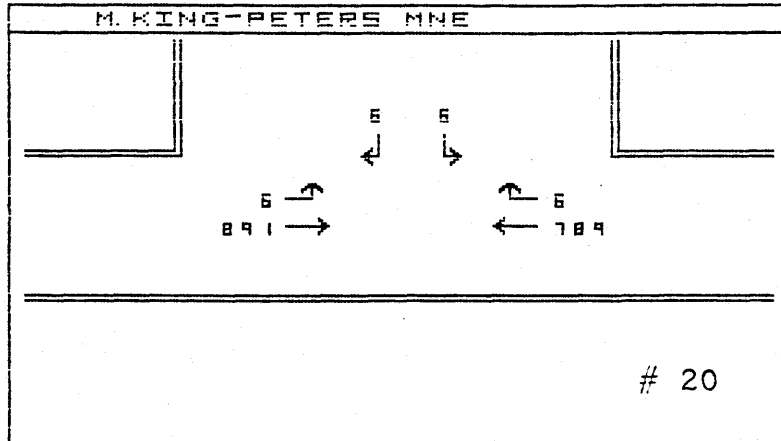
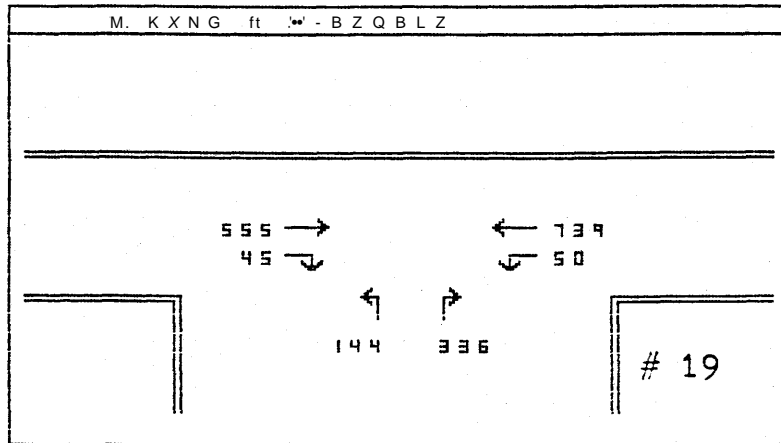


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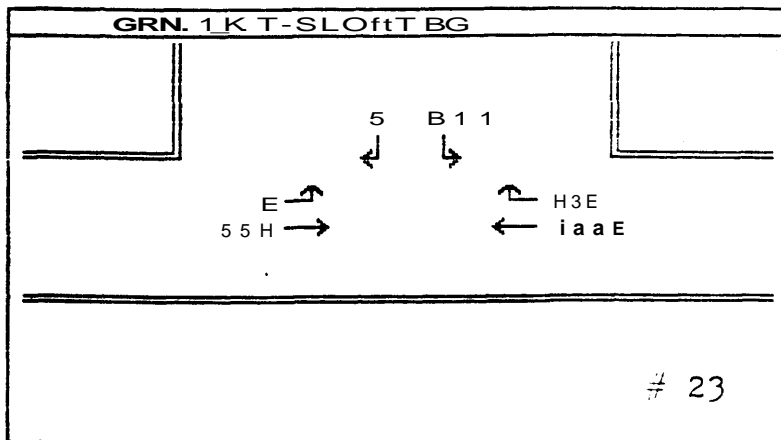
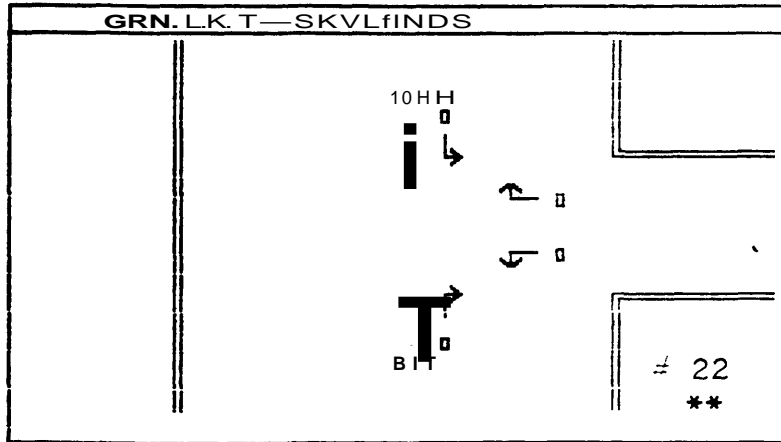
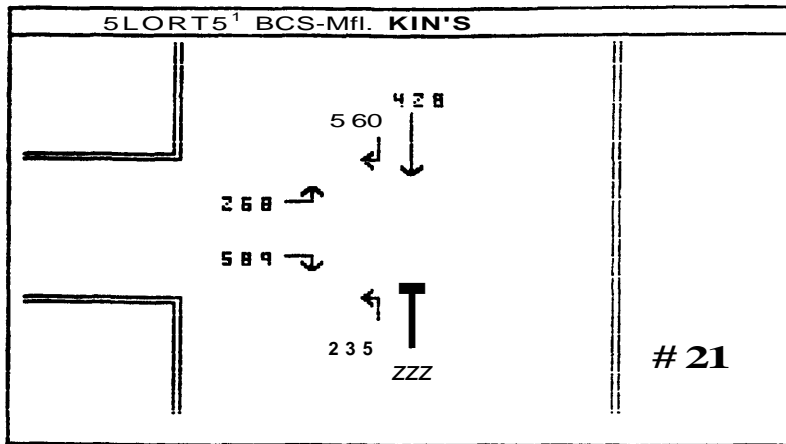
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 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
P.M. PEAK HOUR

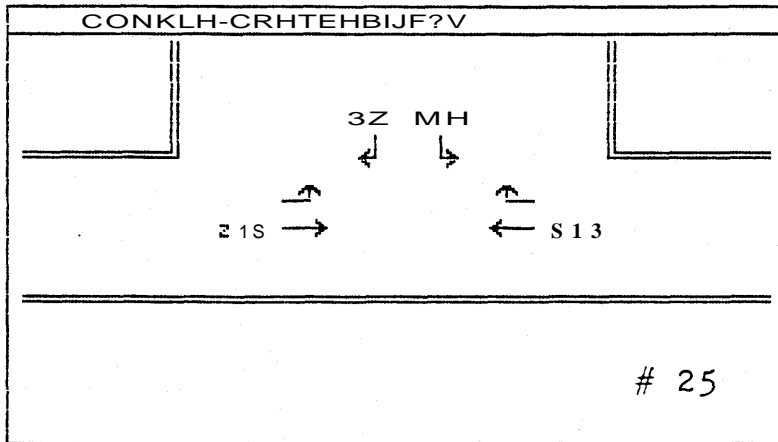
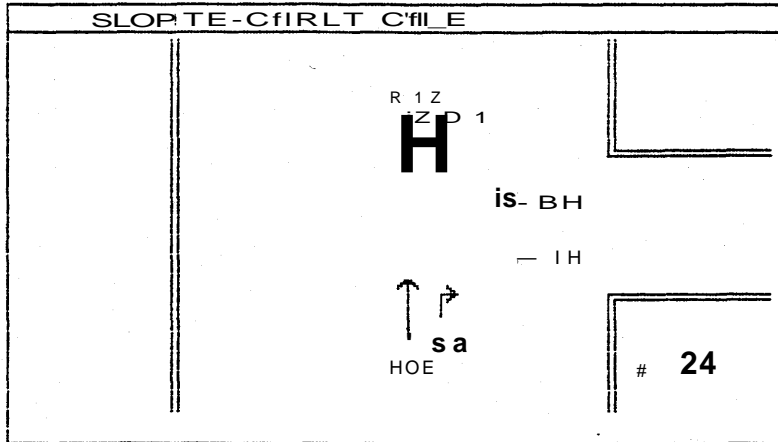


EXISTING INTERSECTION TRAFFIC EXPANDED AT 3[^]/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR



•• NEW TRAFFIC ONLY

EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
P.M. PEAK HOUR



1993 BACKS KKOND TRAFFIC AND SITE TRAFFIC

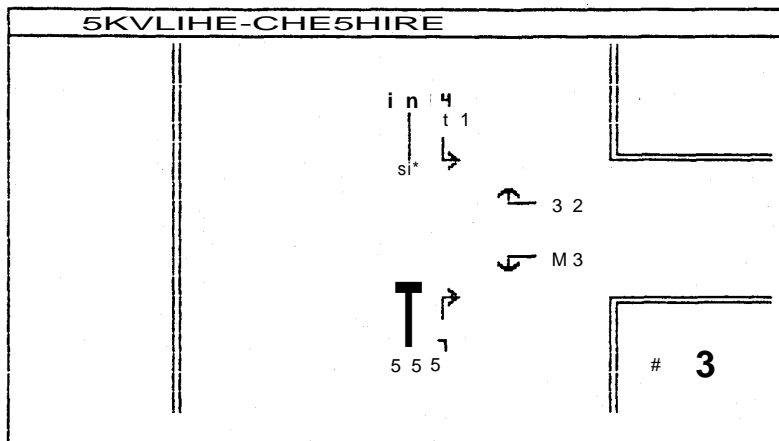
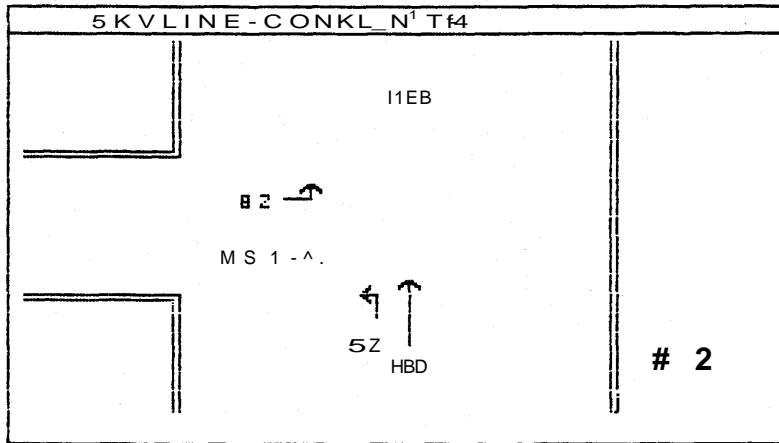
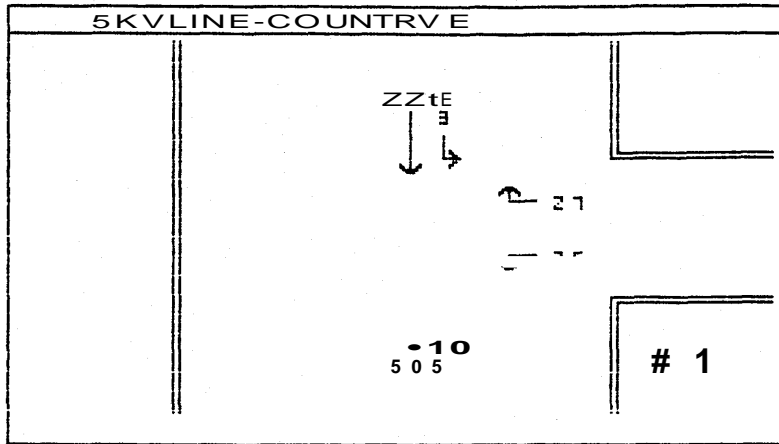
A.M. RESULTING TRAFFIC VOLUMES

WITH

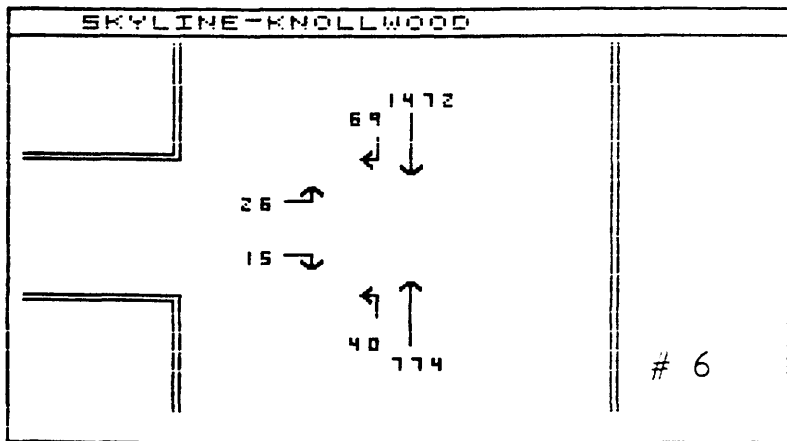
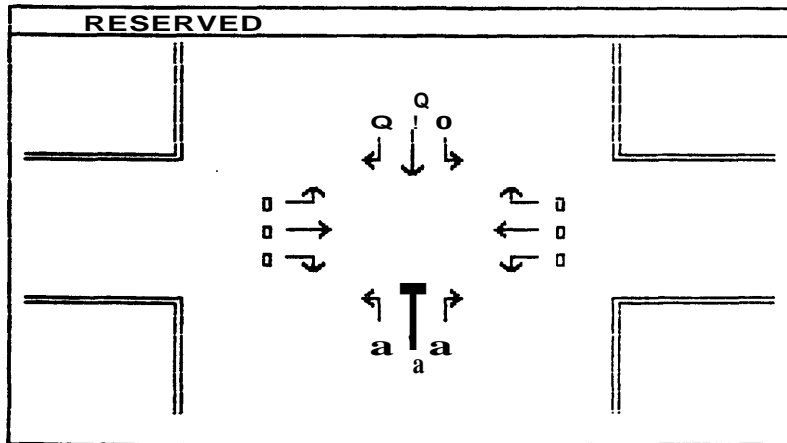
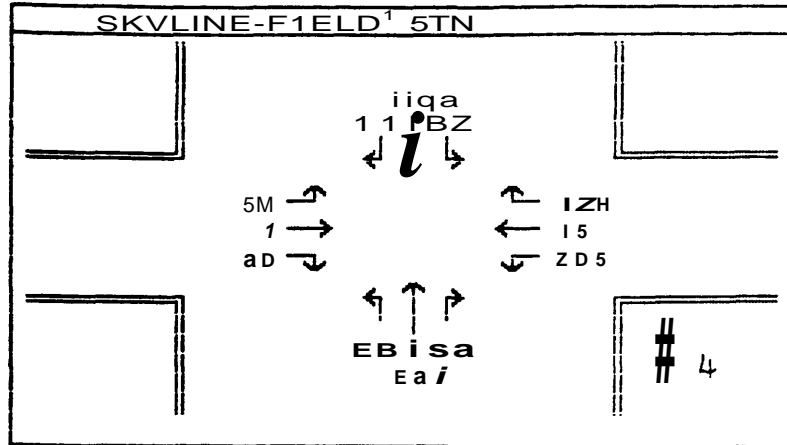
STUDY SITES DEVELOPED AS PROPOSED BY OTHERS

Access to Site 2 via Intersection 13
on Fieldstone Drive unless otherwise noted
(Last Sheet)

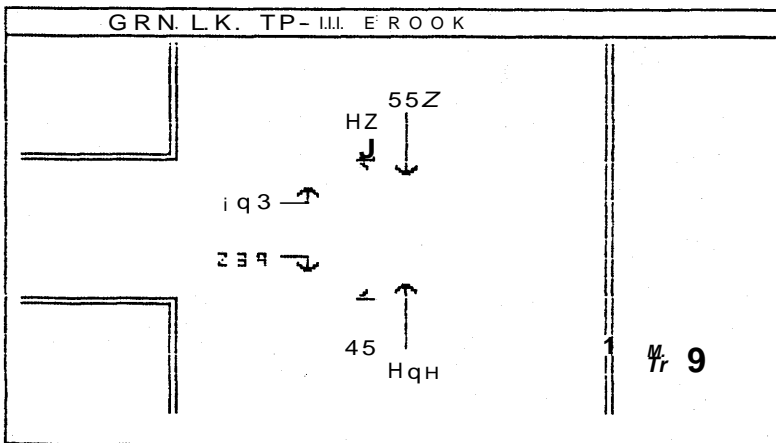
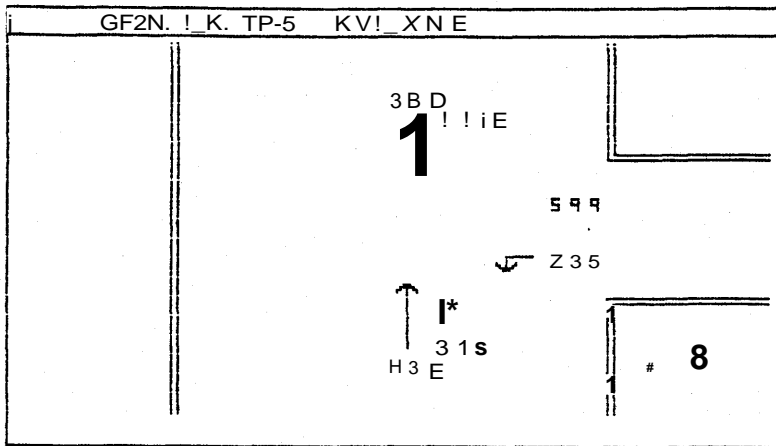
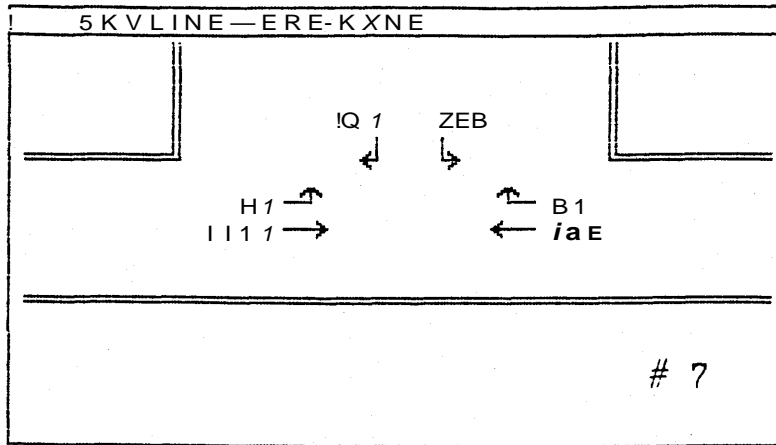
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3#/T2 FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



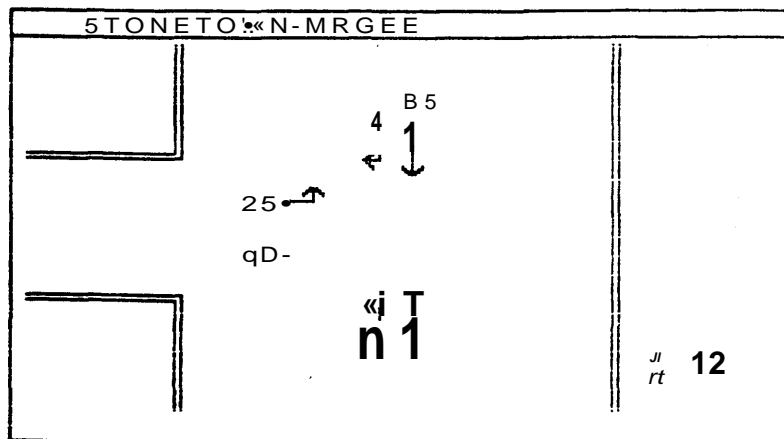
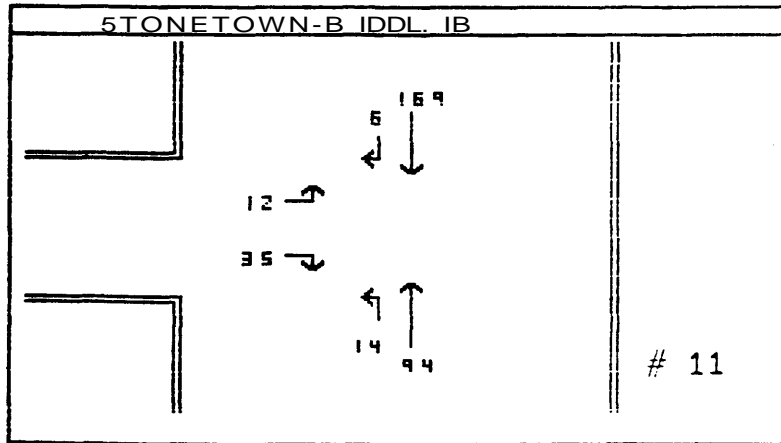
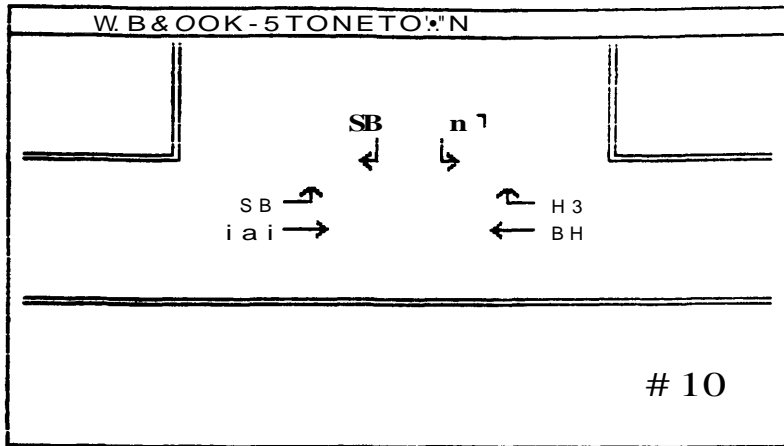
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 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



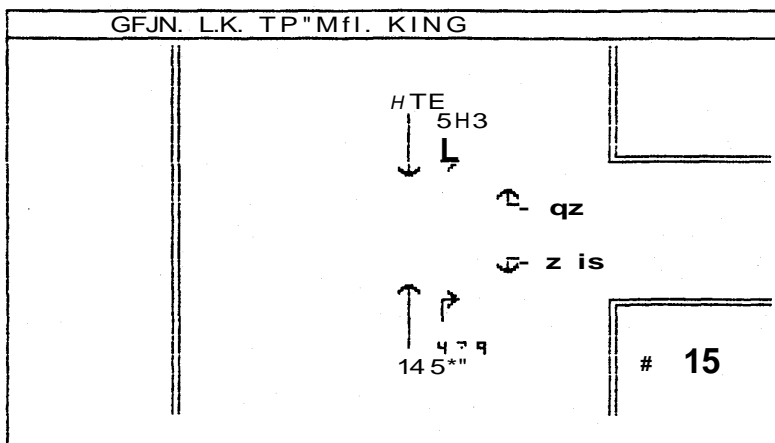
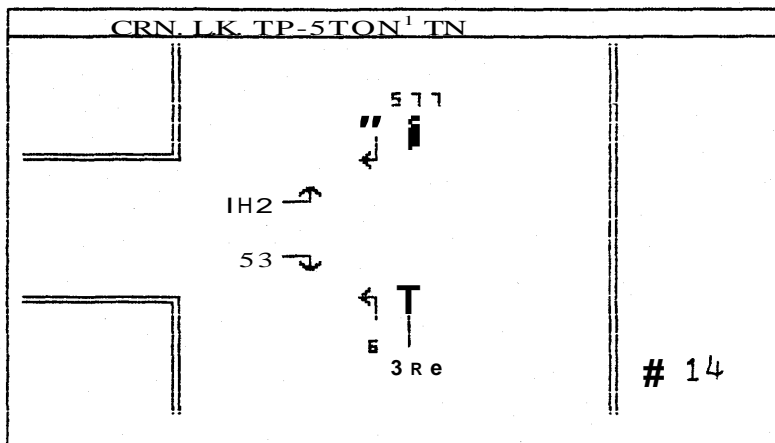
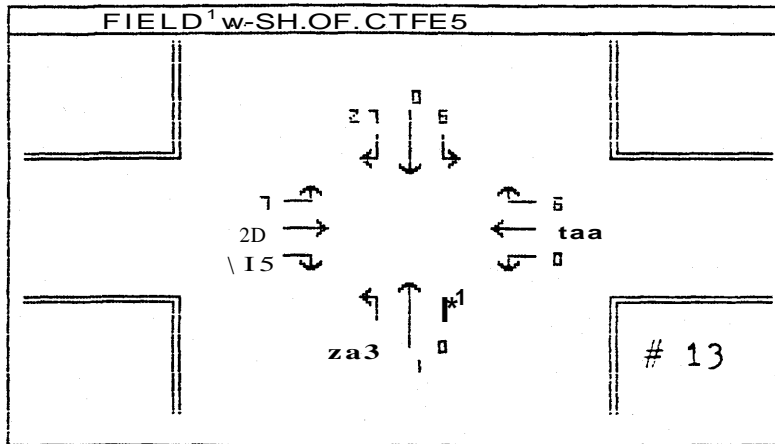
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



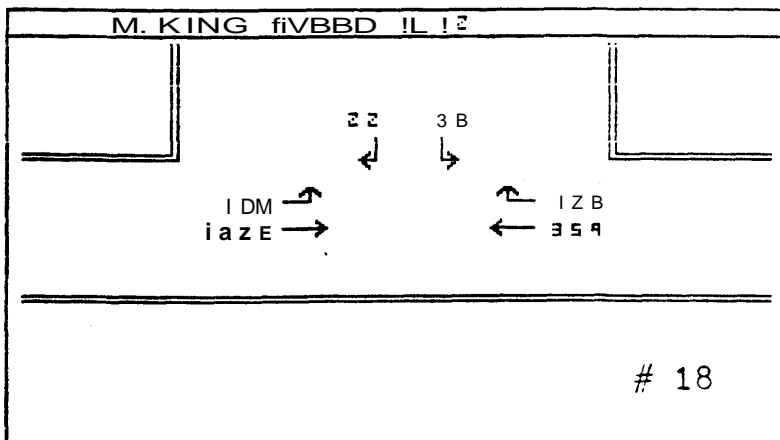
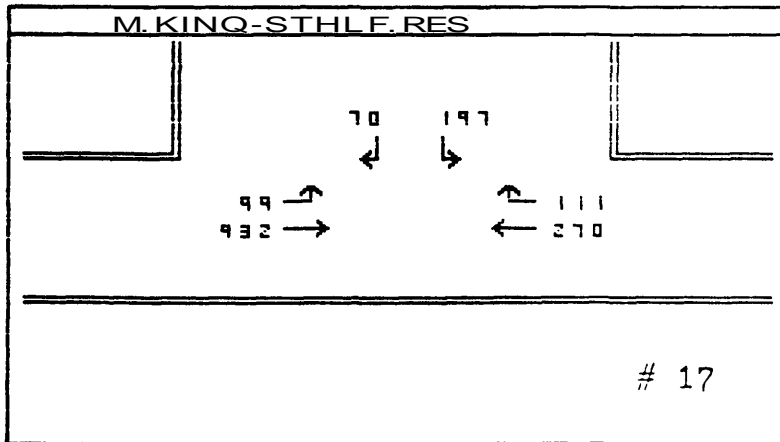
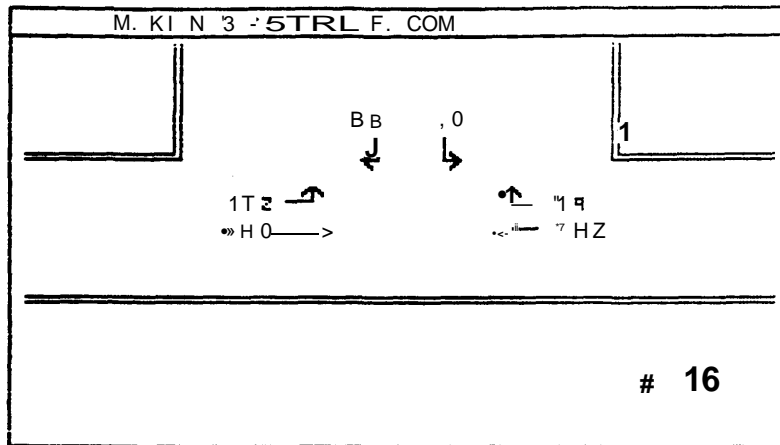
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3<VYR FOR 10 YEARS *
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED EY OTHERS
 A.M. PISAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR

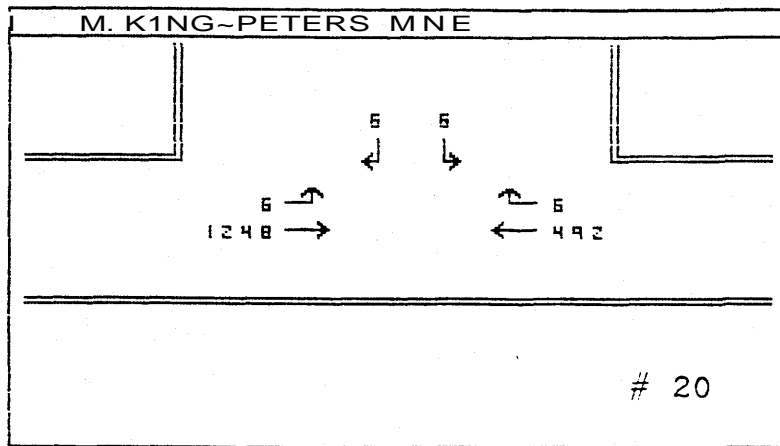
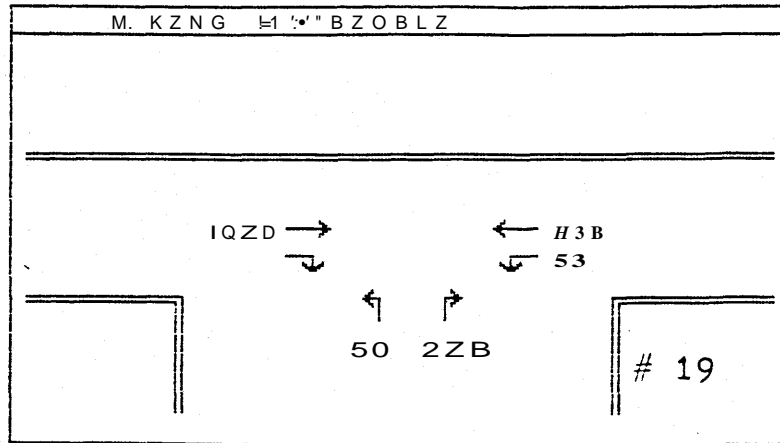


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 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A. M. PEAK HOUR

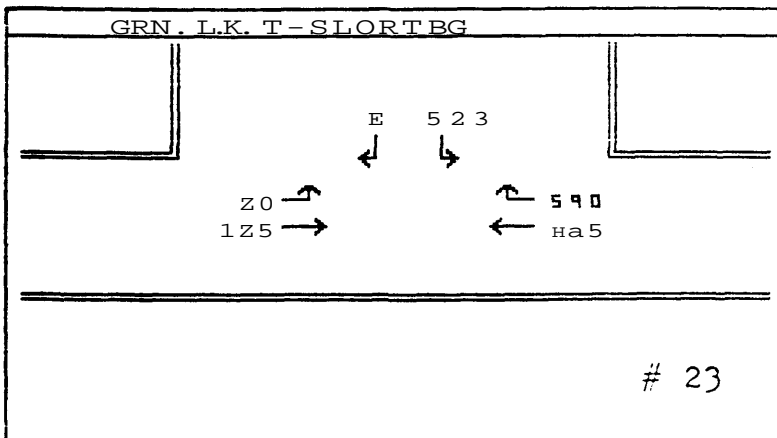
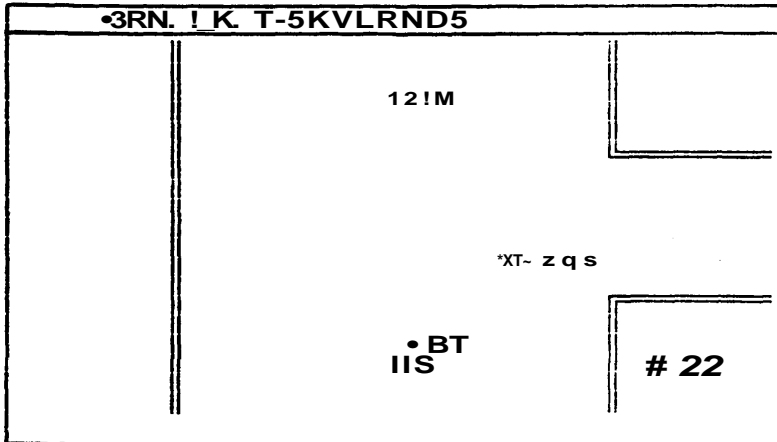
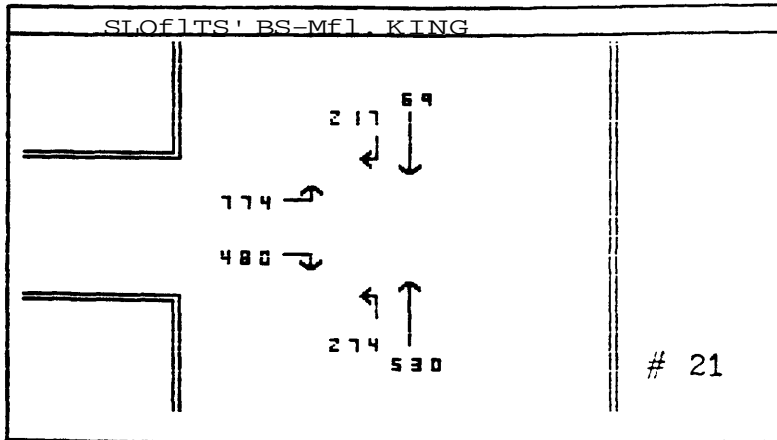


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PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS

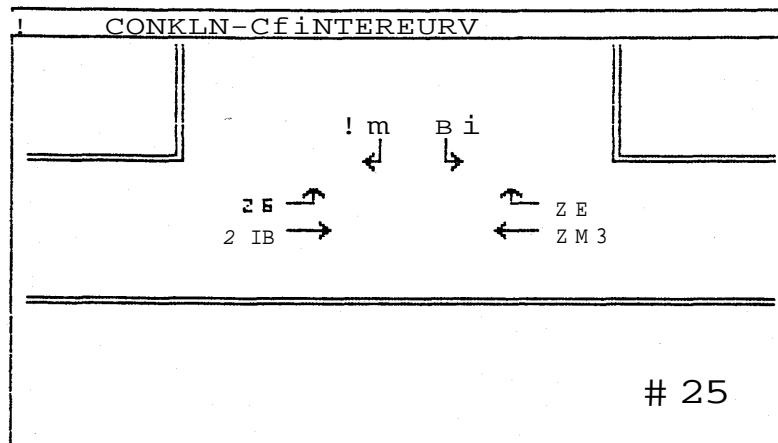
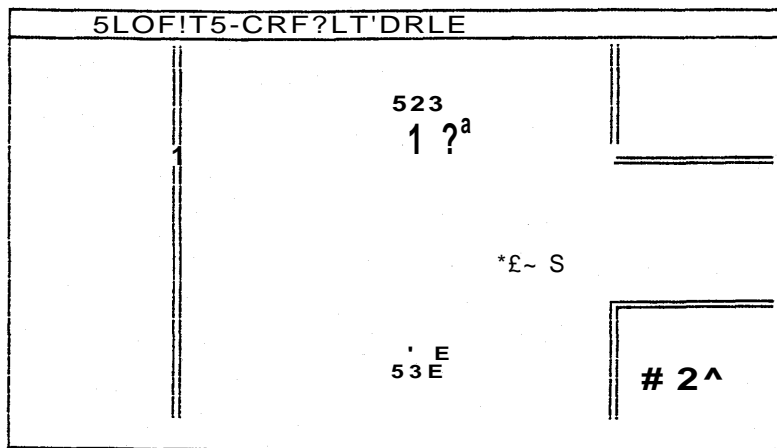
A.M. PEAK HOUR



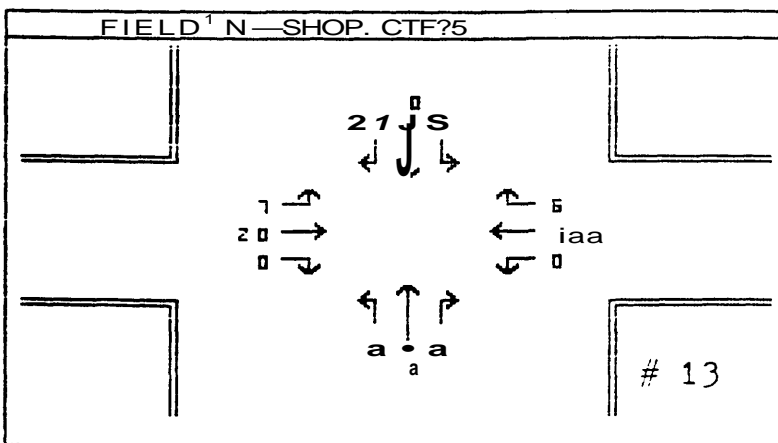
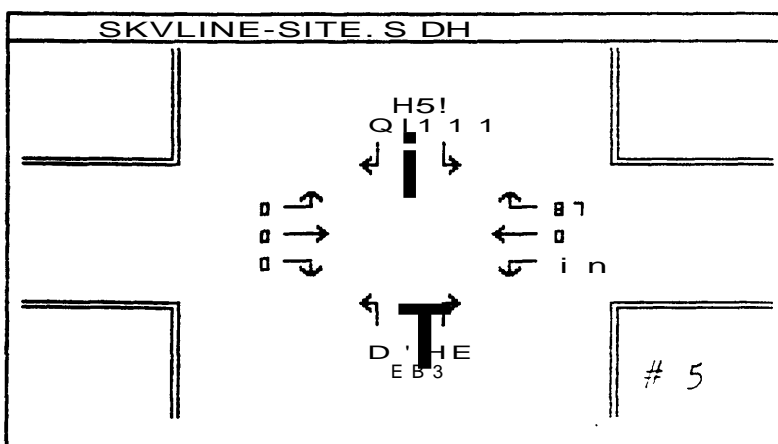
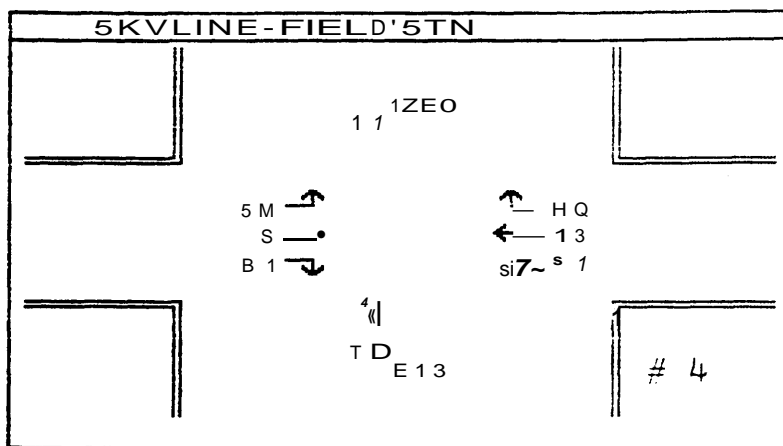
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS *
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3f*/YR FOR 10 YEARS
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
A.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR INR 10 YEARS "
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



1993 BACKGROUND TRAFFIC AND SITS TRAFFIC

P.M. RESULTING TRAFFIC VOLUMES

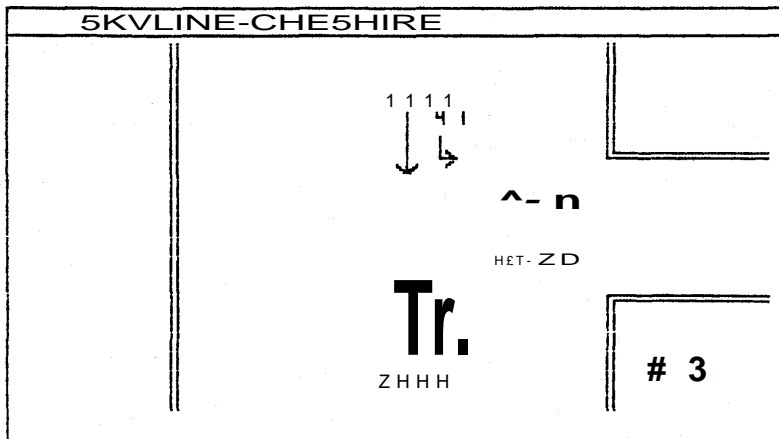
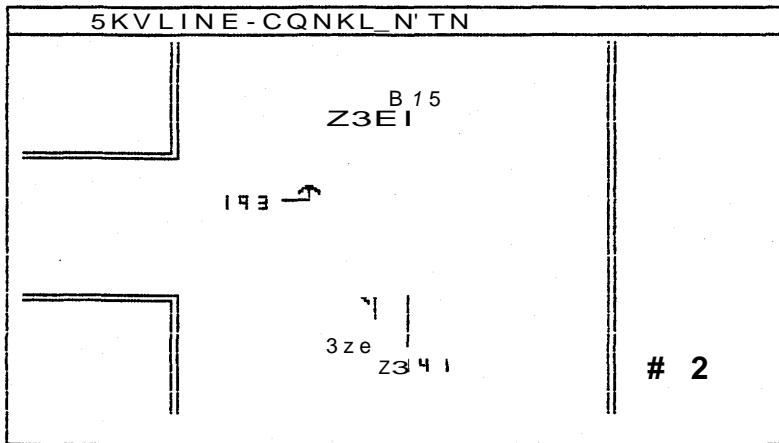
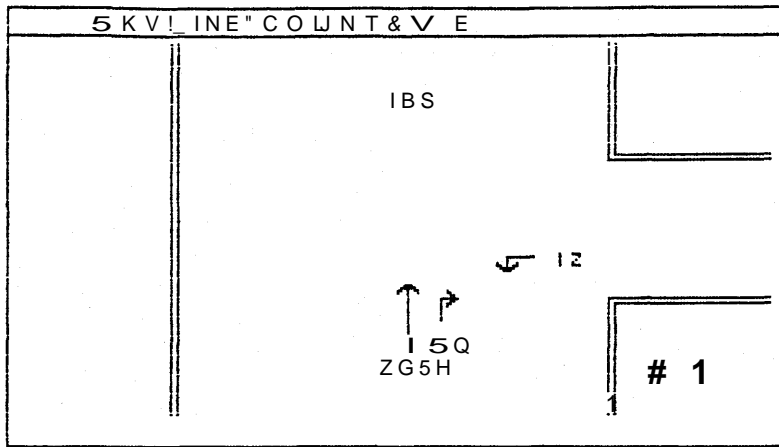
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STUDY SITES DEVELOPED AS PROPOSED BY OTHERS

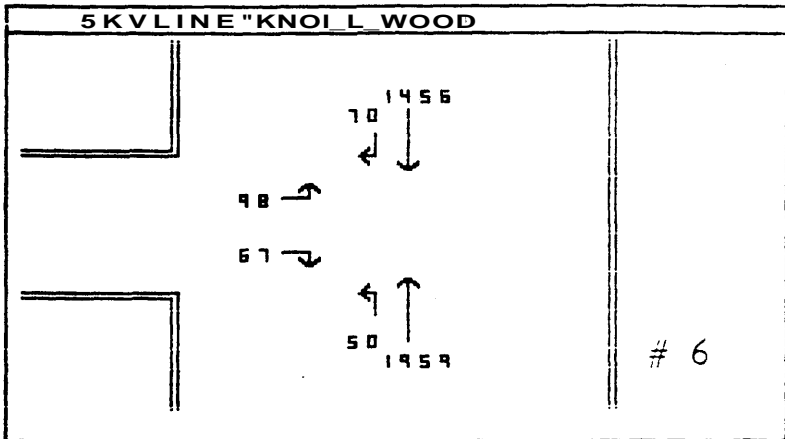
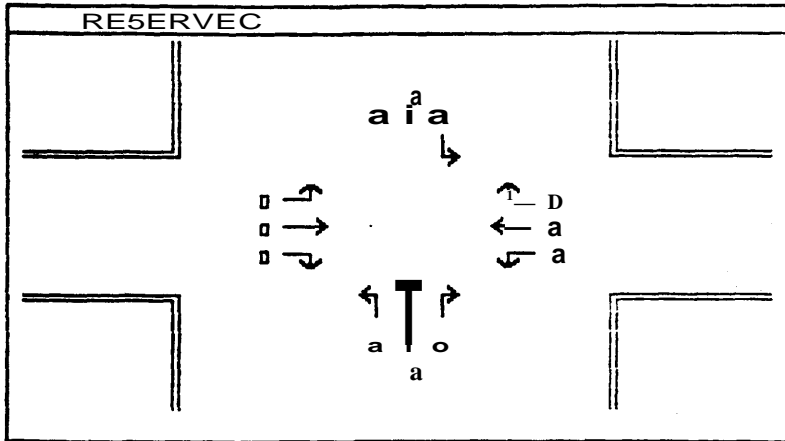
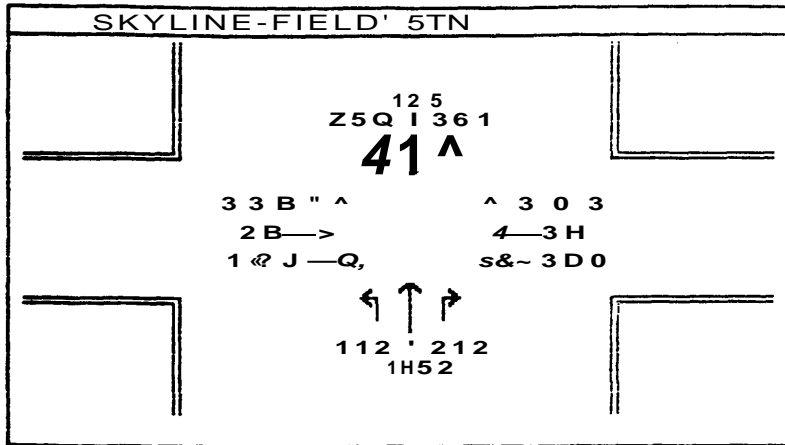
Access to Site 2 via Intersection 13
on Fieldstone Drive unless otherwise noted
(Last Sheet)

EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS

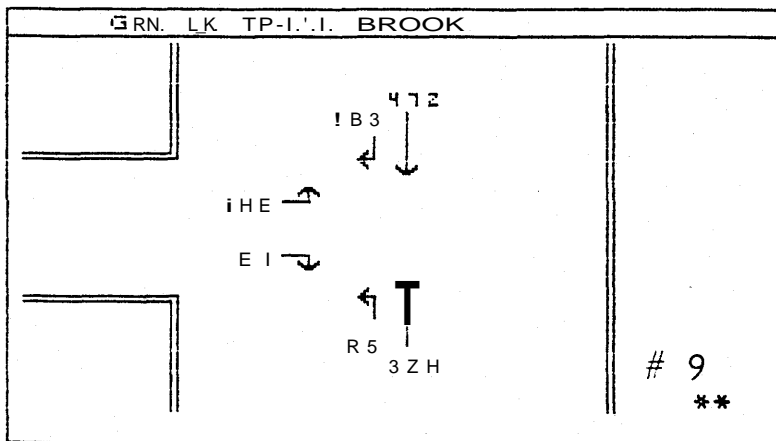
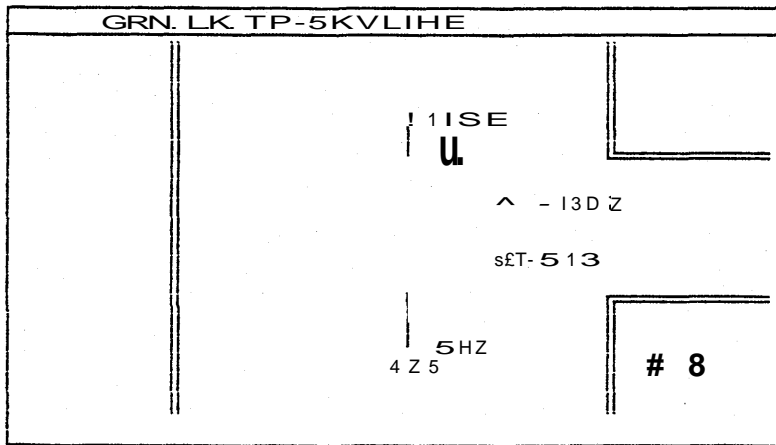
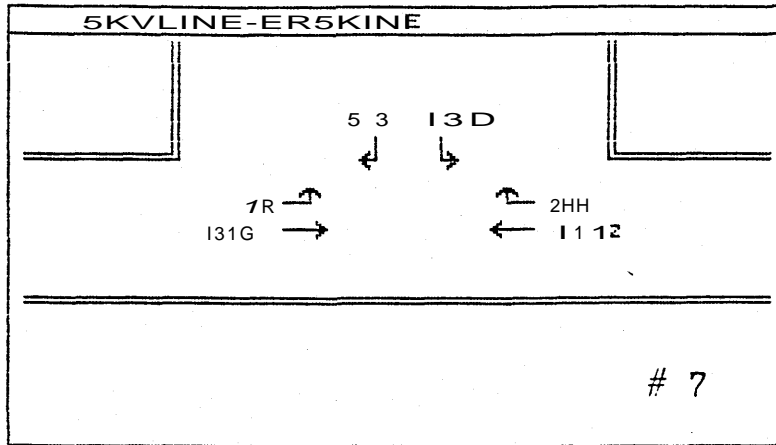
P.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3#/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR

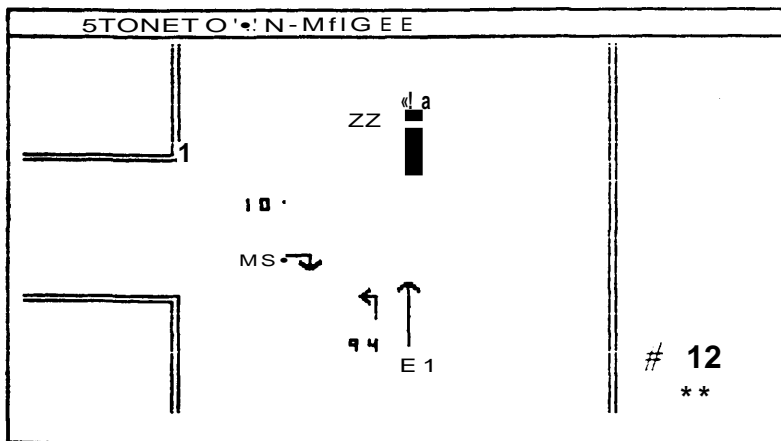
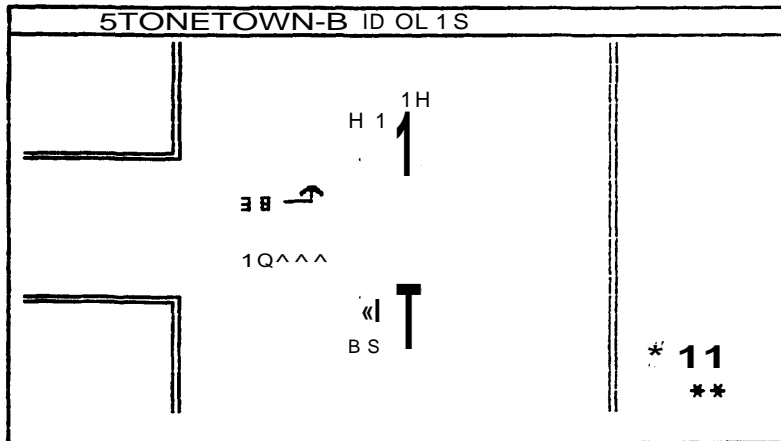
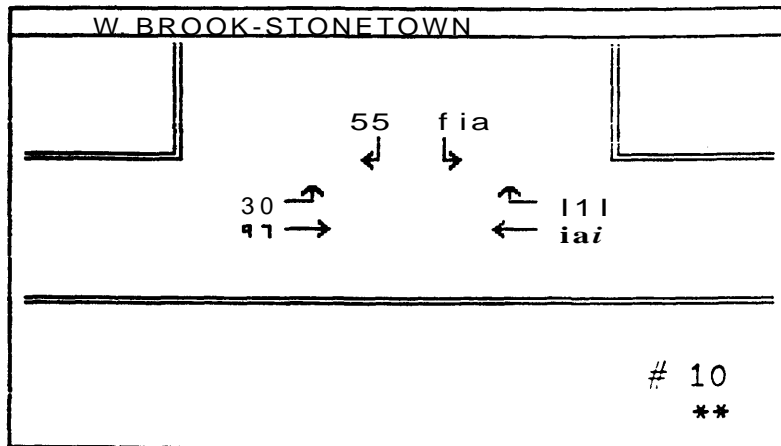


EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR



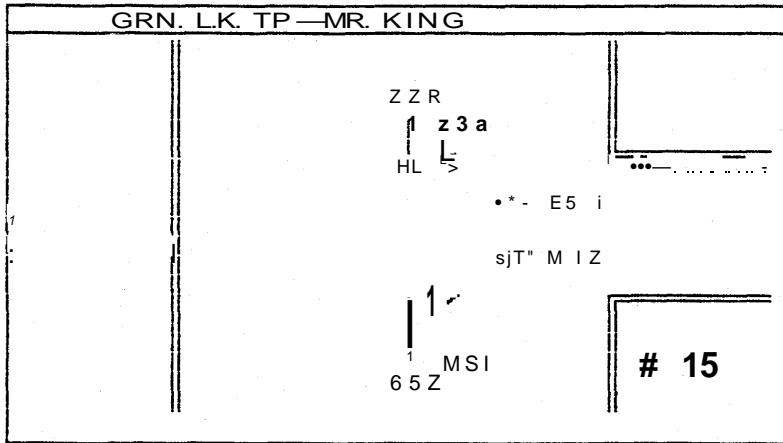
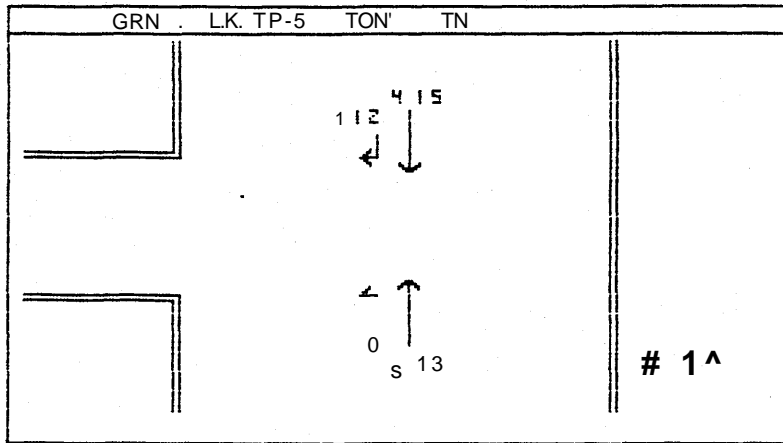
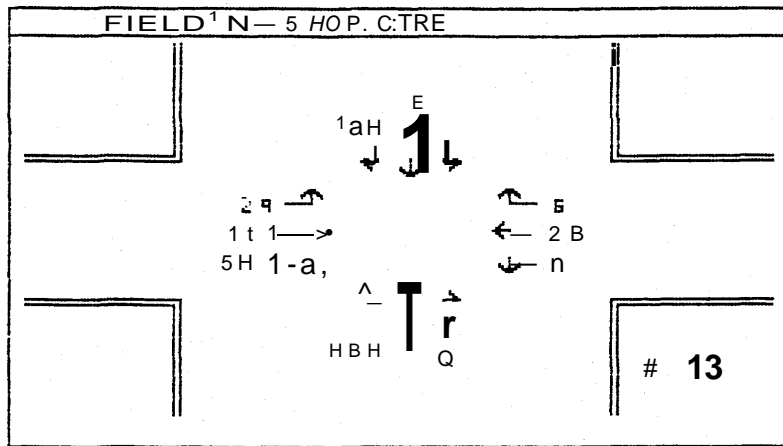
** NEW TRAFFIC ONLY

EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR



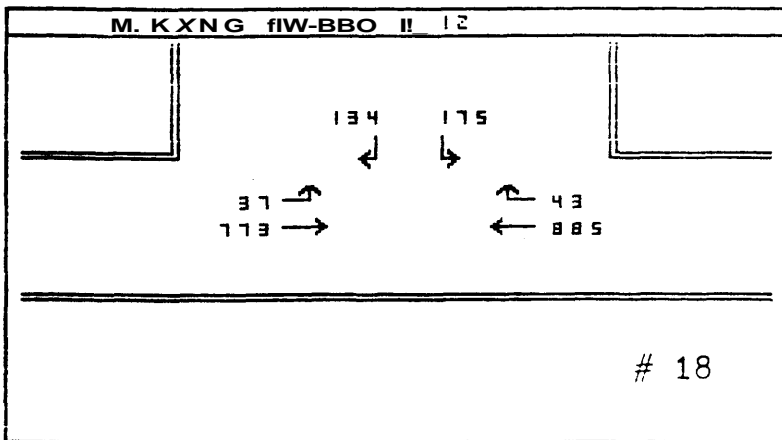
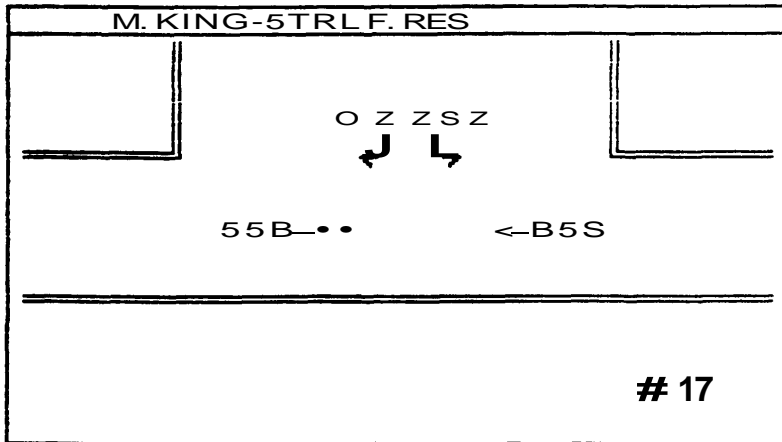
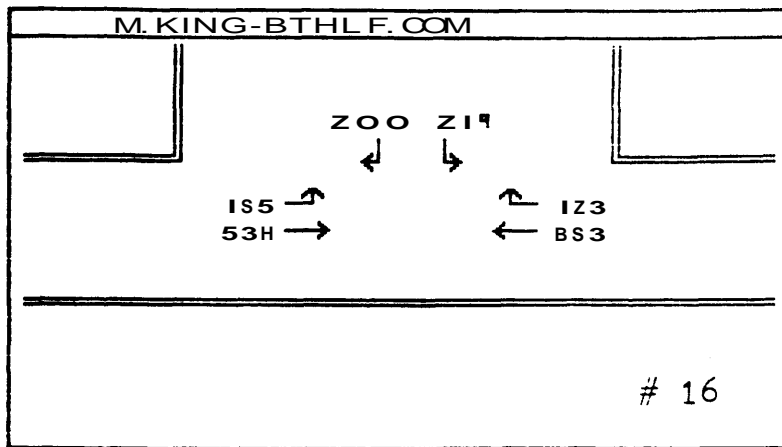
•• NSIP TRAFFIC ONLY

EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR

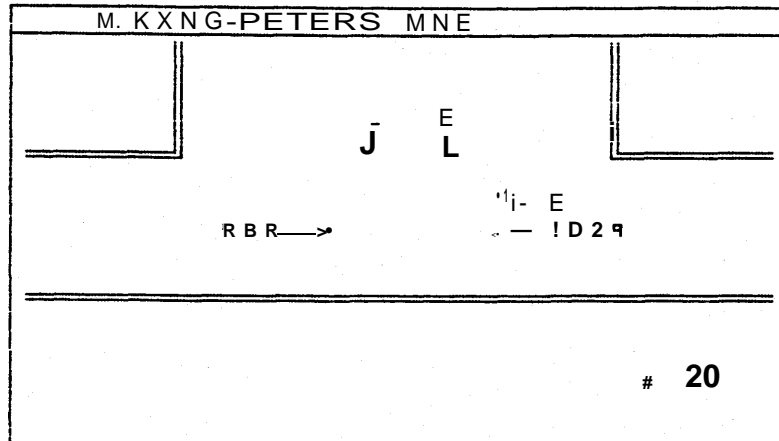
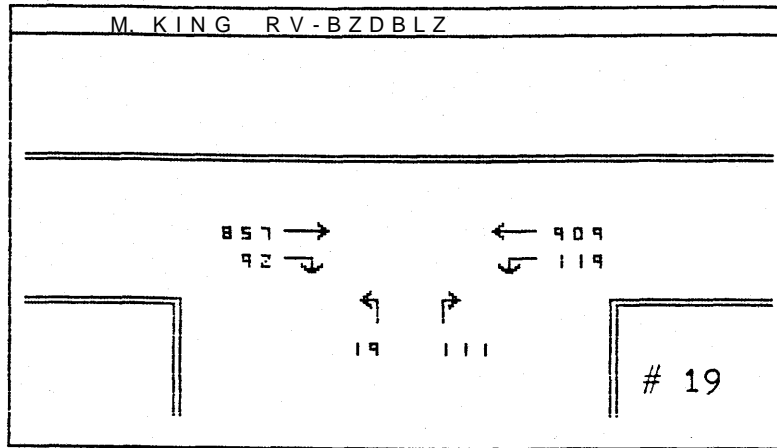


** NEW TRAFFIC ONLY

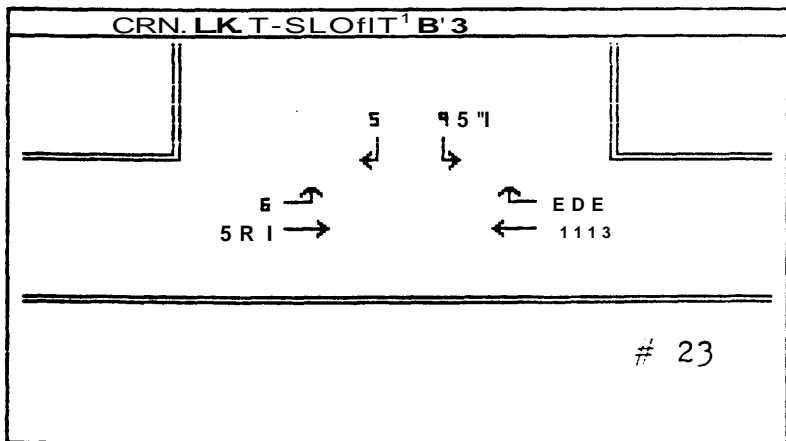
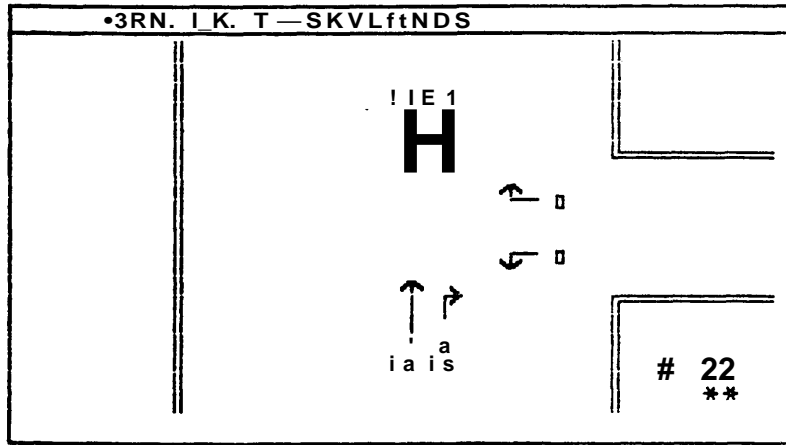
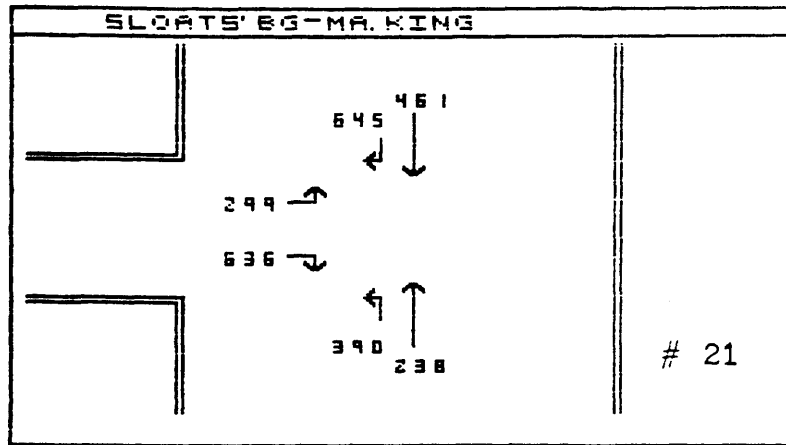
EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
P.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT *JfofiK* FOR 10 YEARS
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
P.M. PEAK HOUR

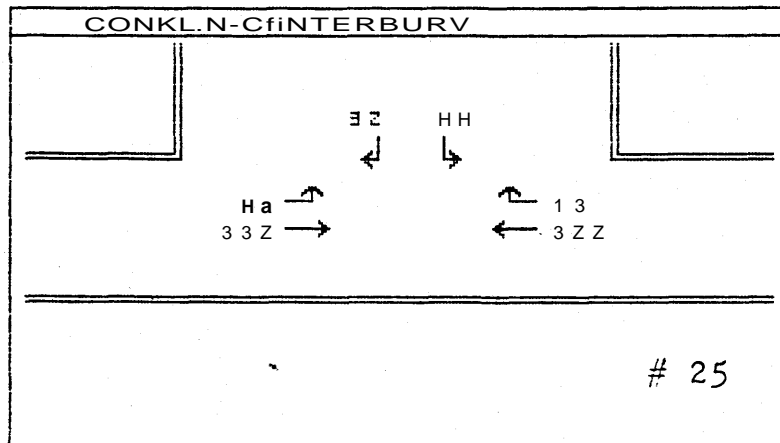
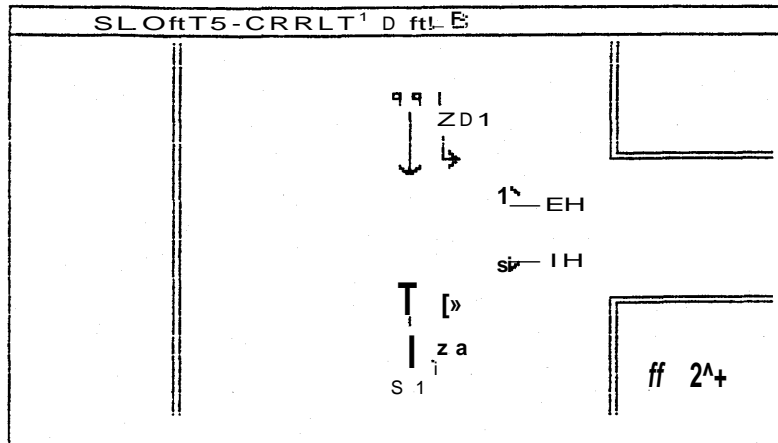


EXISTING INTERSECTION TRAFFIC EXPANDED AT 3fo/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR

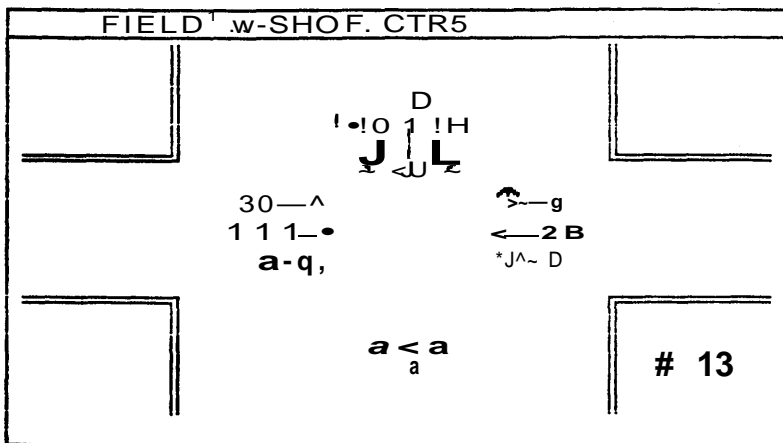
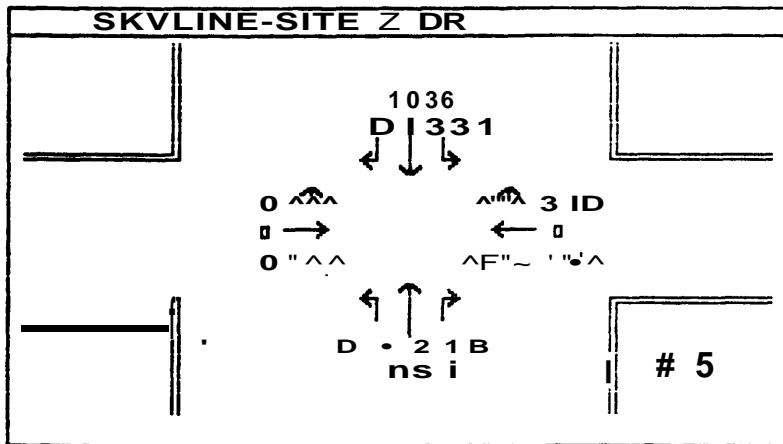
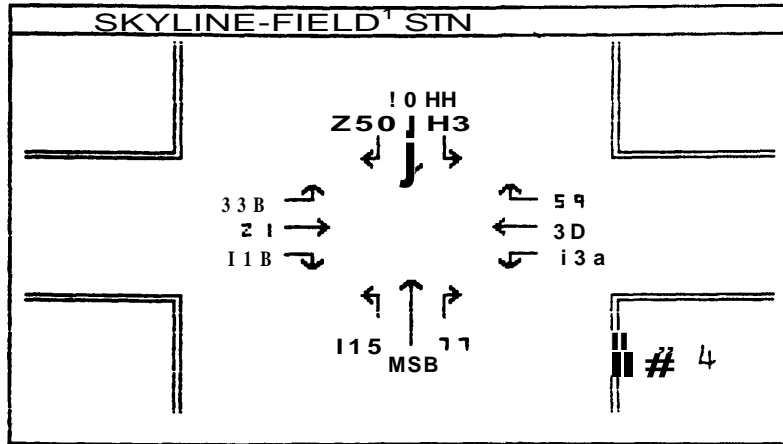


•• NEWJ TRAFFIC ONLY

EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC EXPANDED AT 3%/YR FOR 10 YEARS PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS WITH ACCESS TO SITE 2 FROM SKYLINE DRIVE
P.M. PEAK HOUR



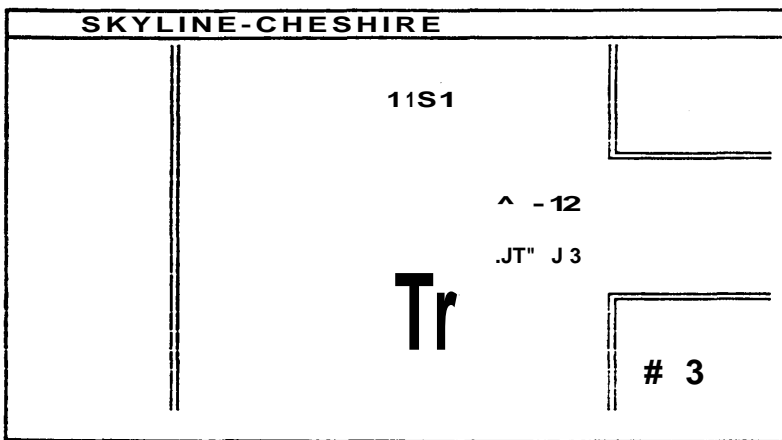
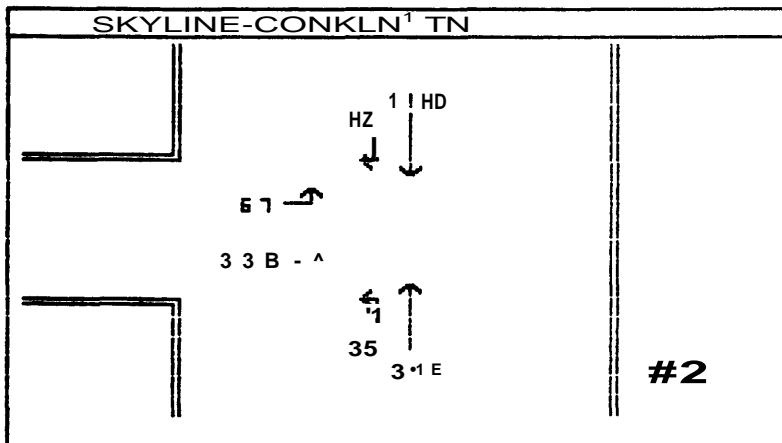
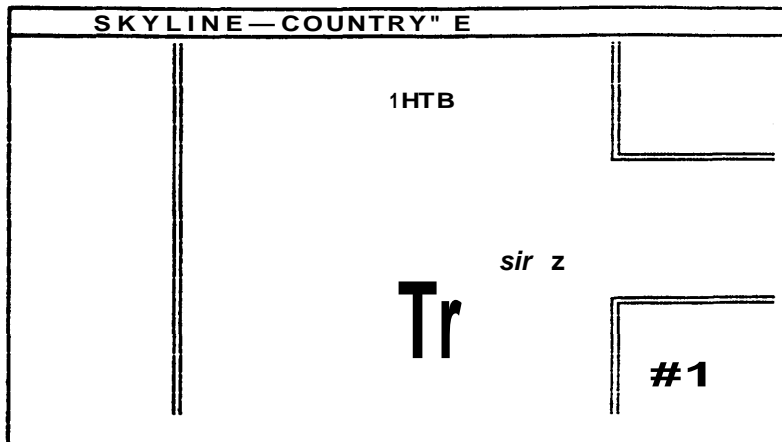
1983 BACKGROUND TRAFFIC AND SITE TRAFFIC

A.M. EXISTING TRAFFIC VOLUMES

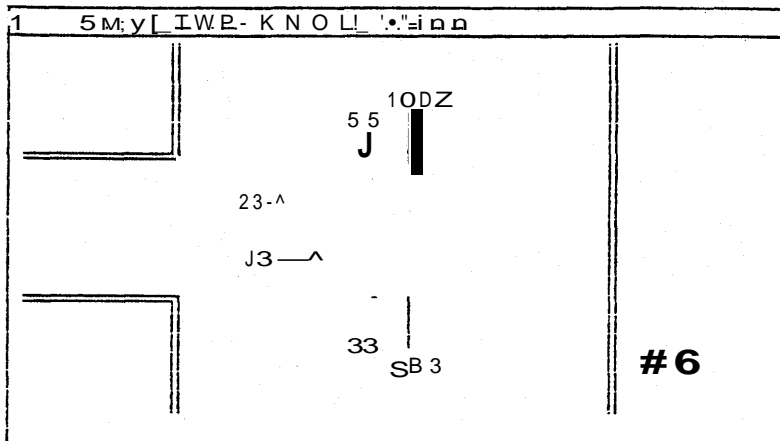
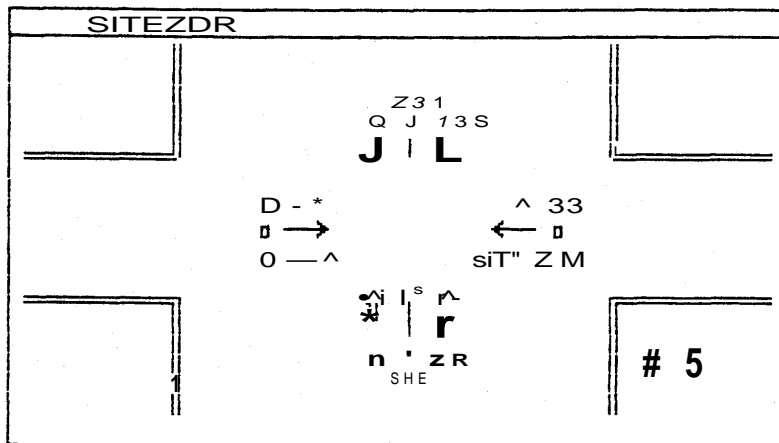
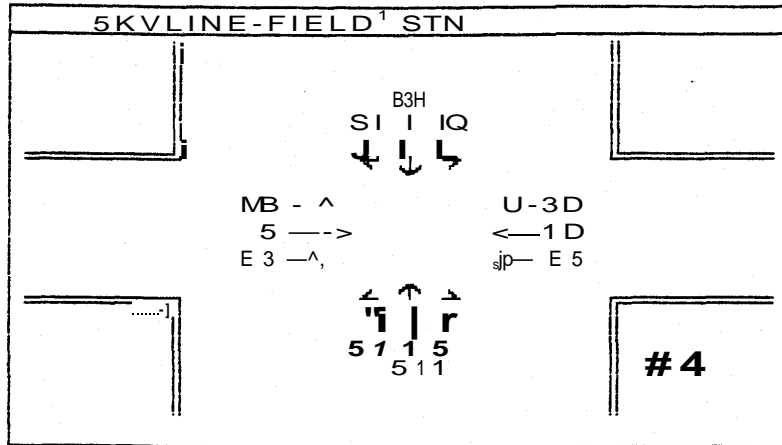
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STUDY SITES DEVELOPED AS ZONED

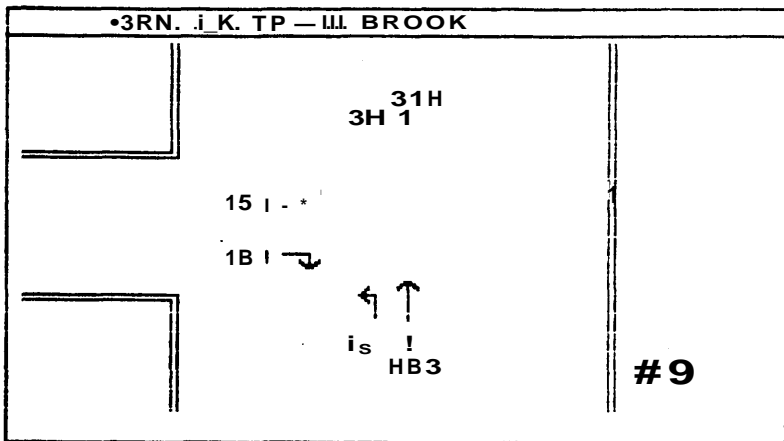
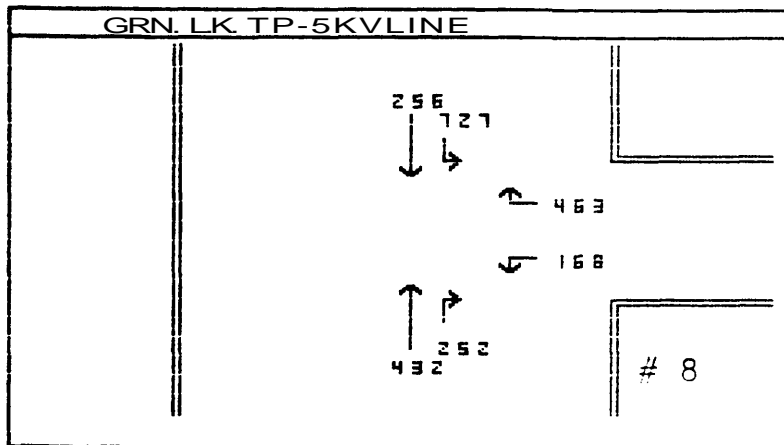
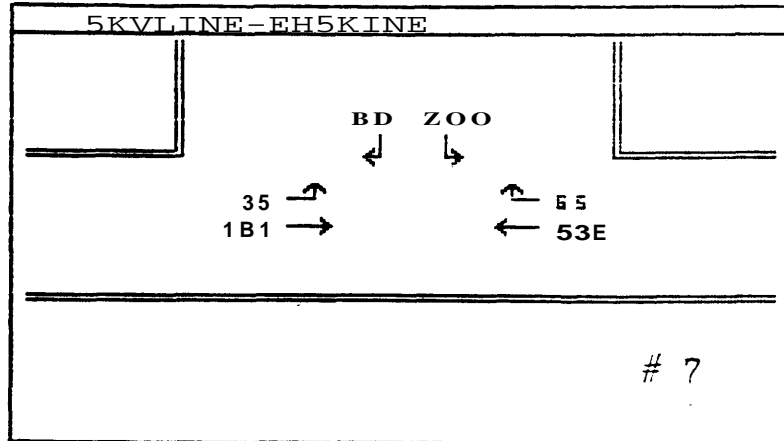
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 A.M. PEAK HOUR



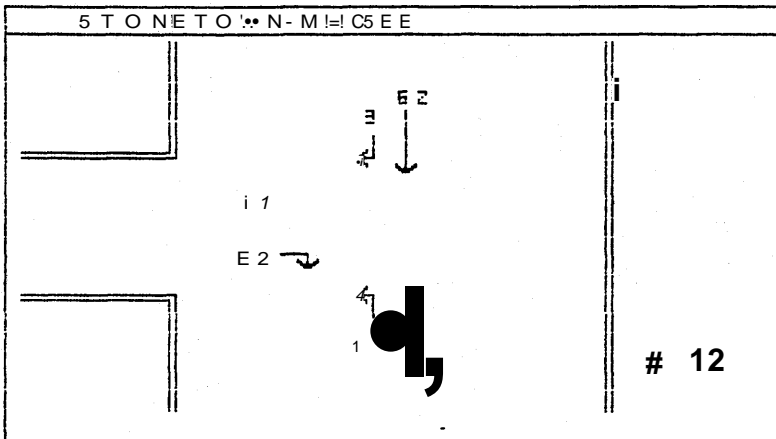
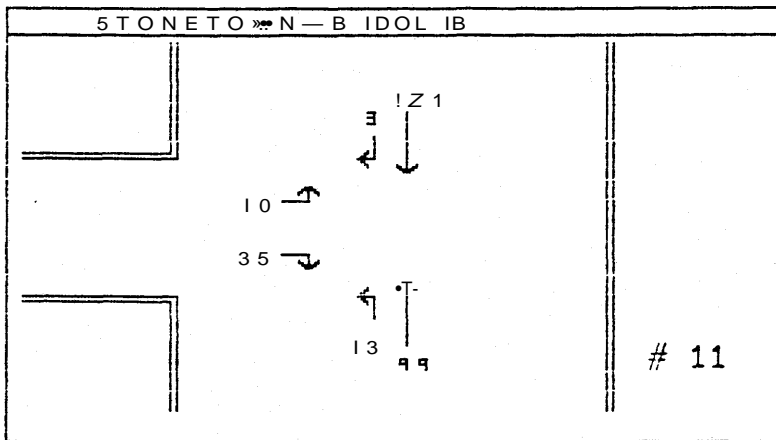
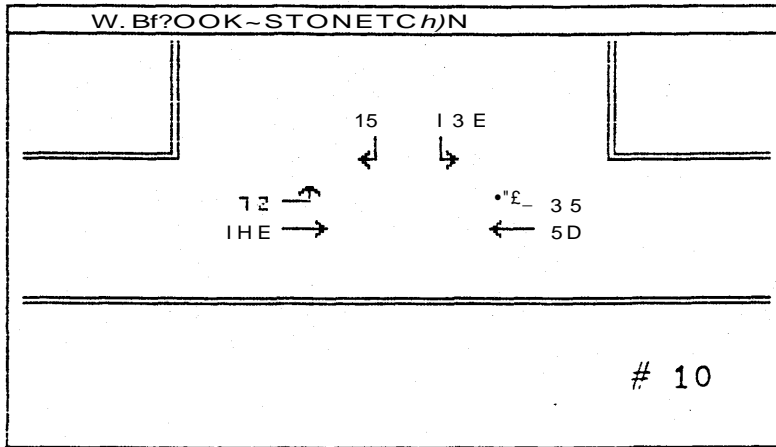
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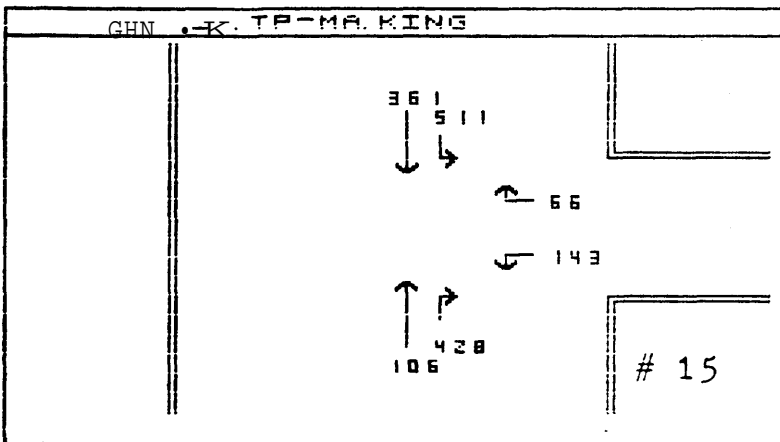
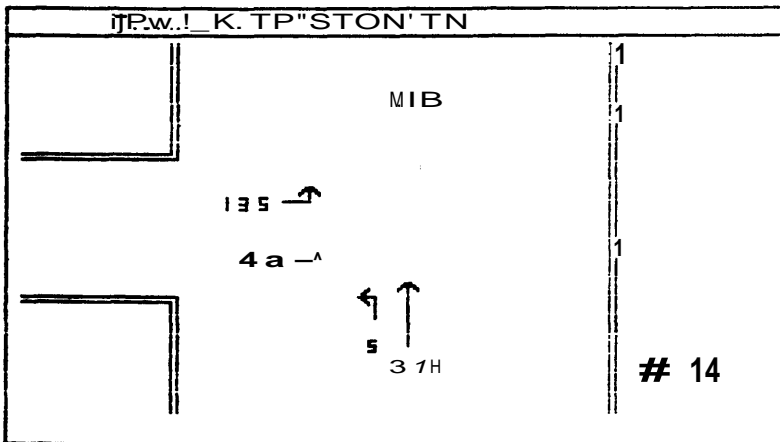
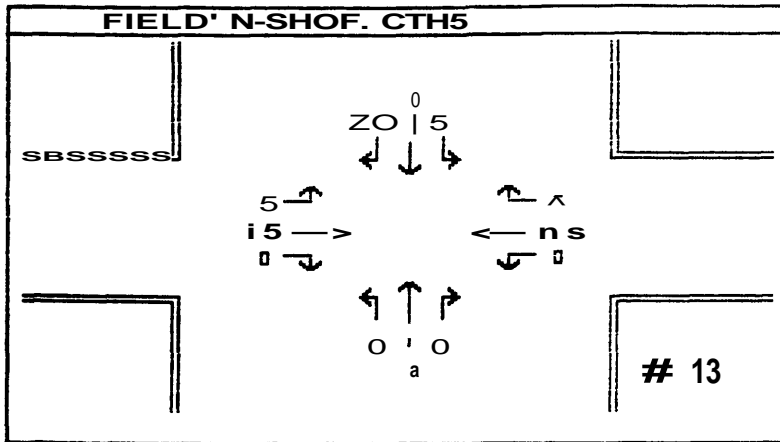
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 PUJS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



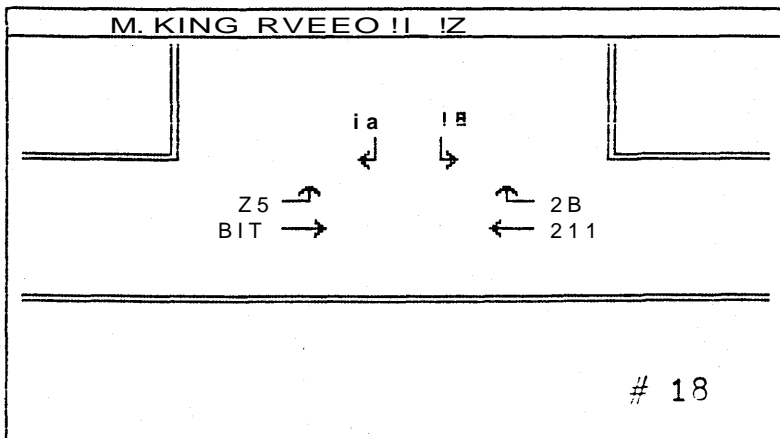
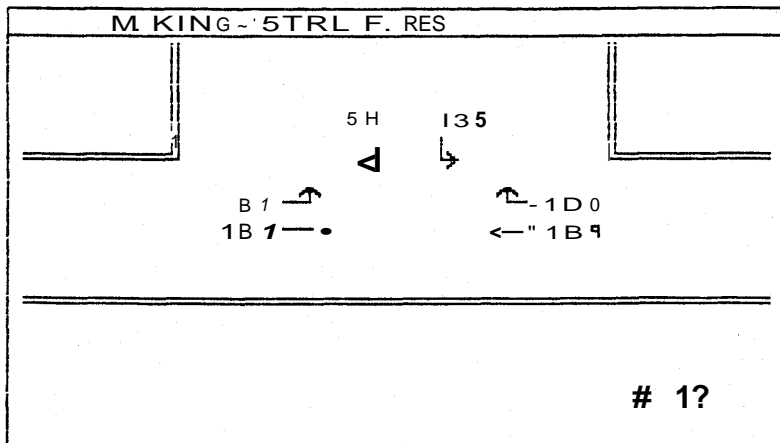
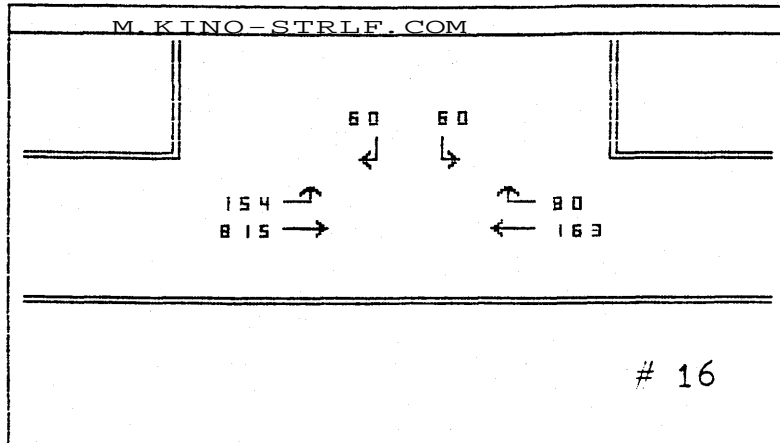
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PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
A.M. PEAK HOUR



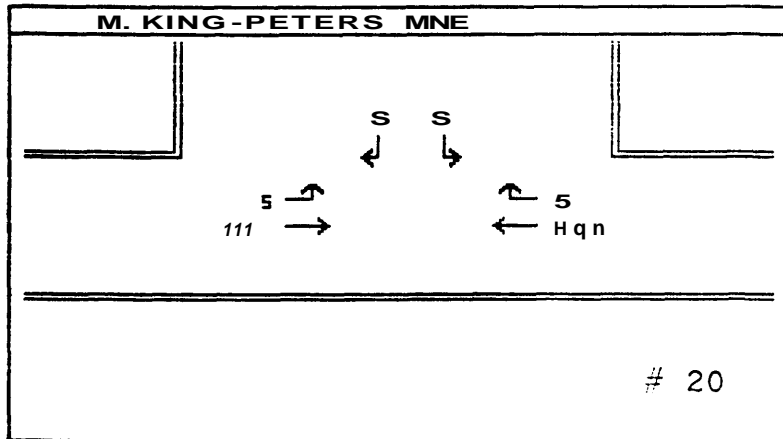
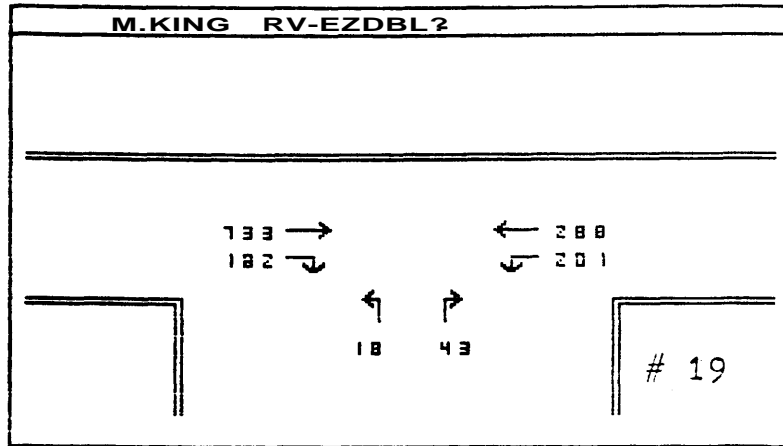
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 A.M. PEAK HOUR



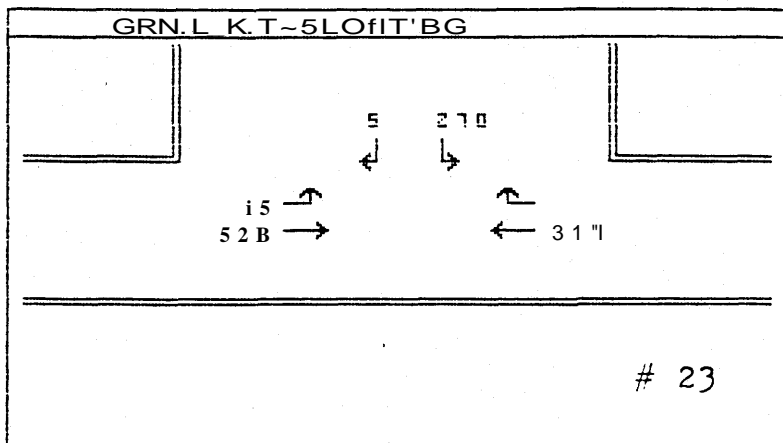
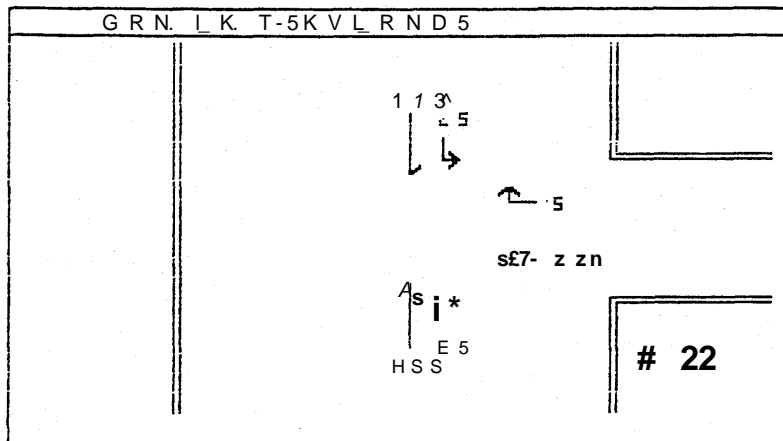
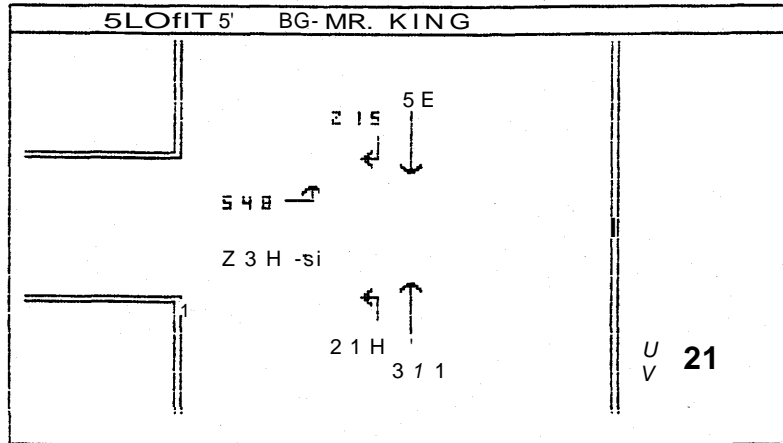
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PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
A.M. PEAK HOUR



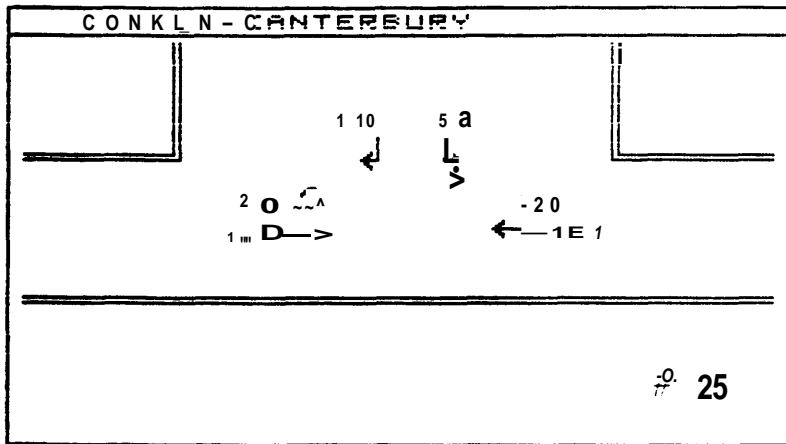
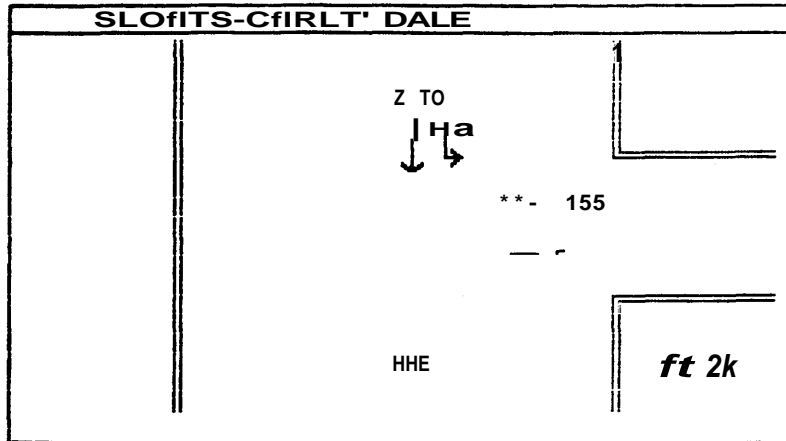
EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
A.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 A.M. PEAK HOUR



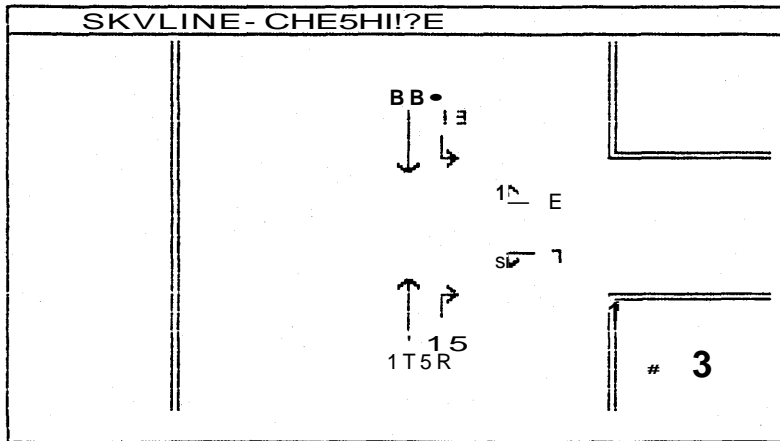
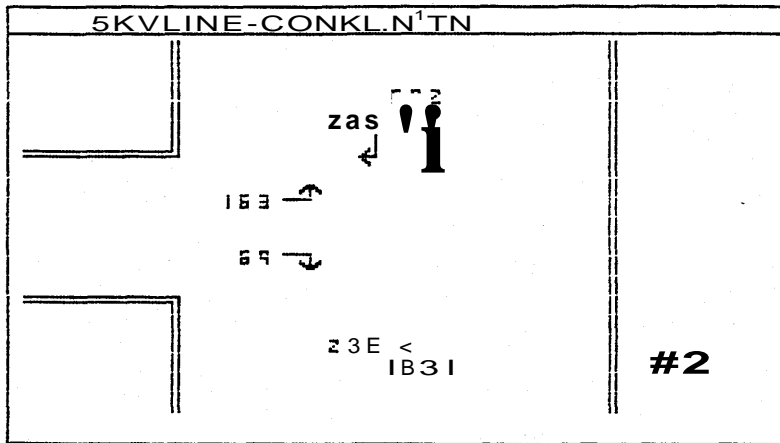
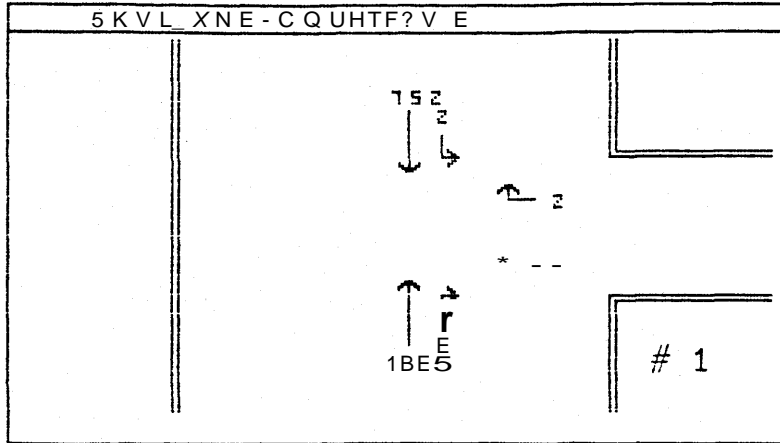
1983 BACKGROUND TRAFFIC AND SITE TRAFFIC

P.M. EXISTING TRAFFIC VOLUMES

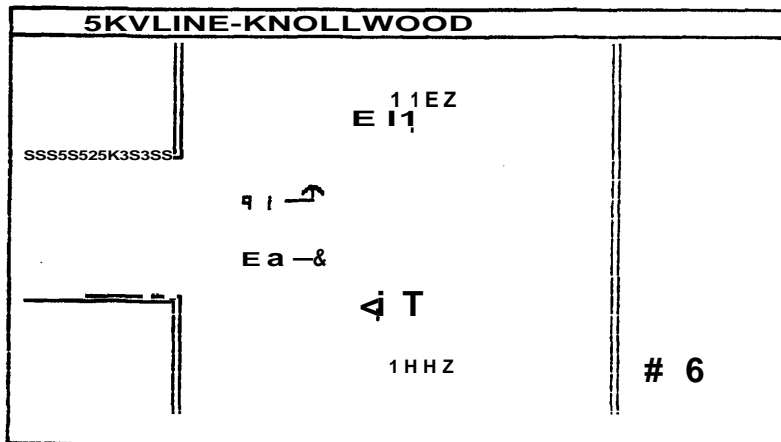
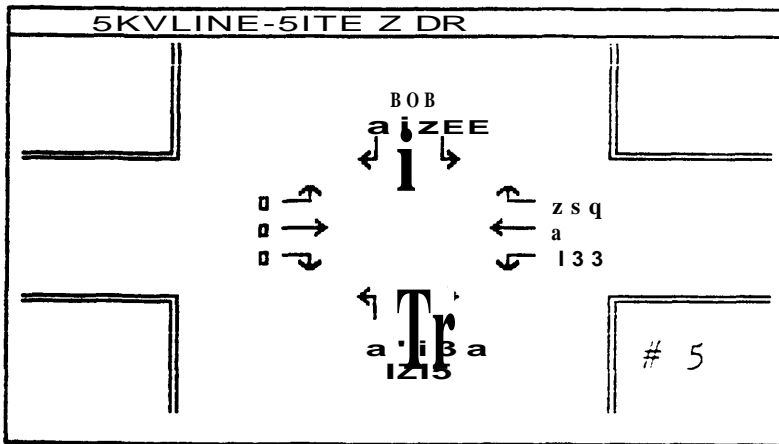
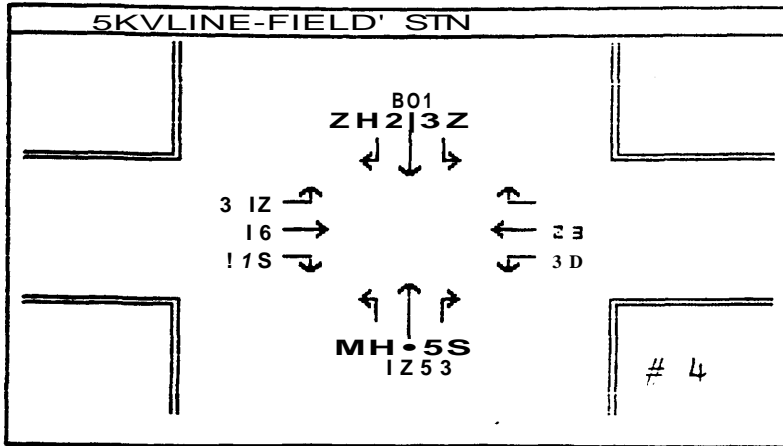
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STUDY SITES DEVELOPED AS ZONED

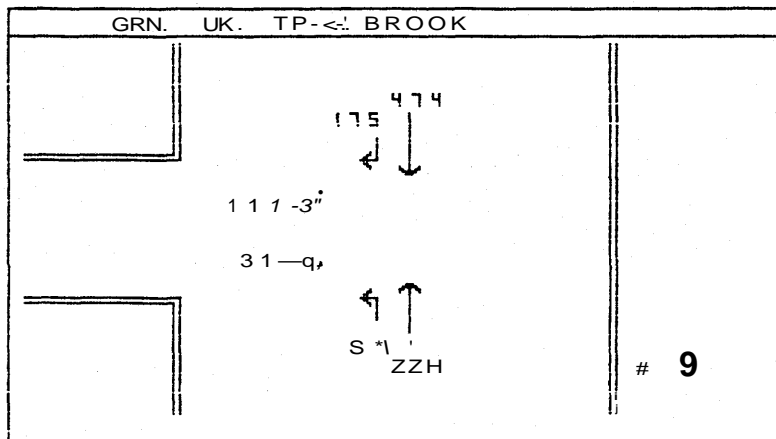
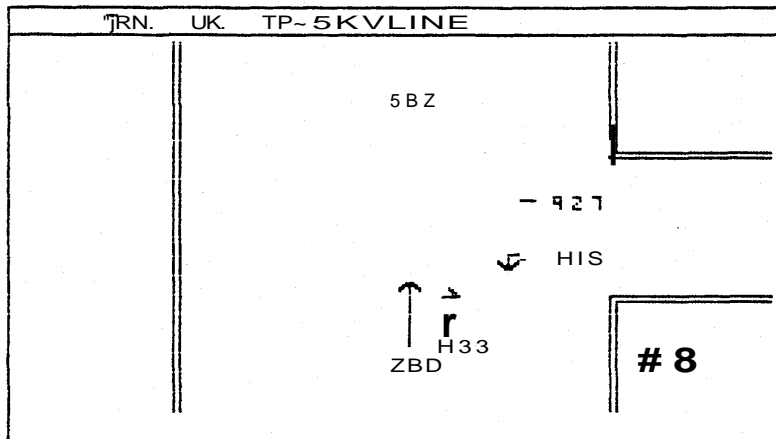
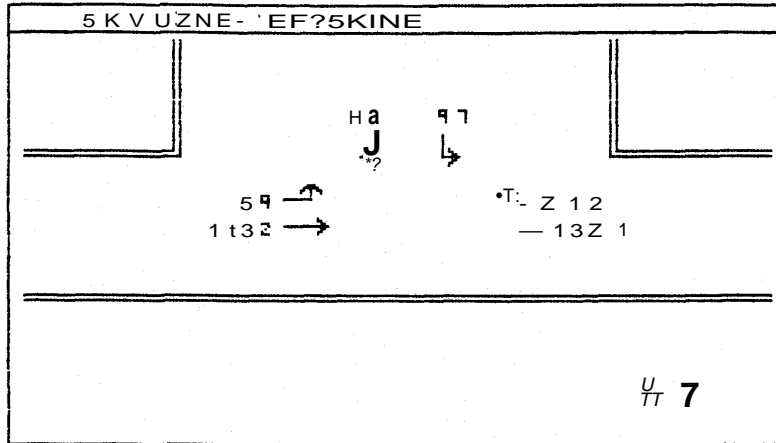
EXISTING INTERSECTION TRAFFIC
 PLUS ^TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR



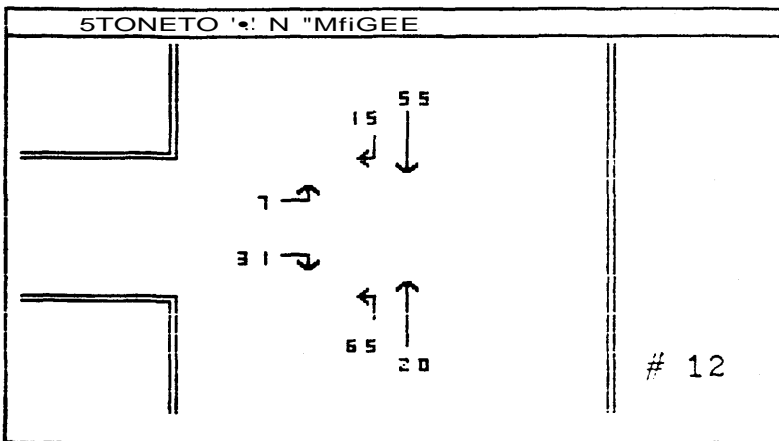
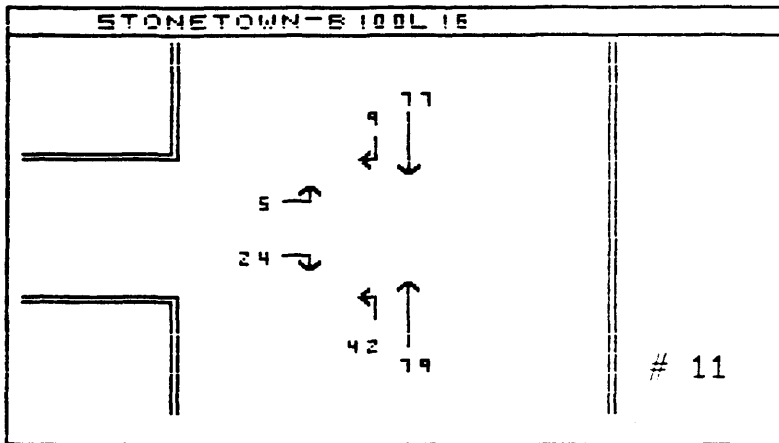
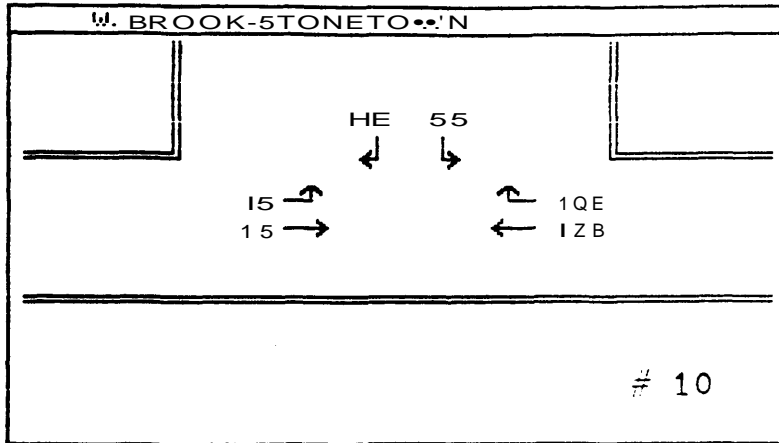
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 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR



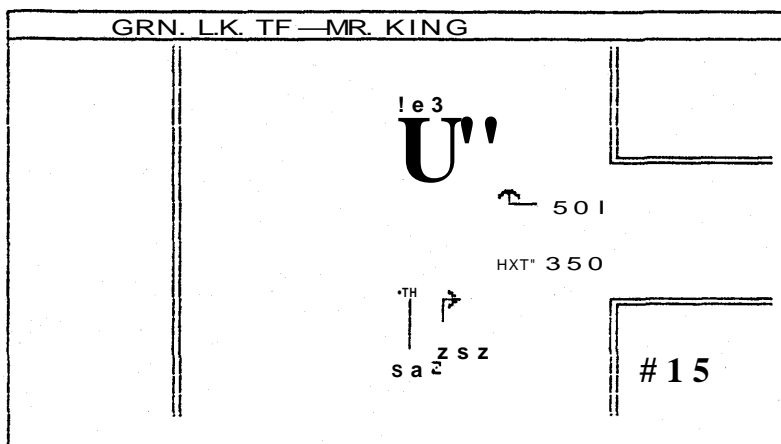
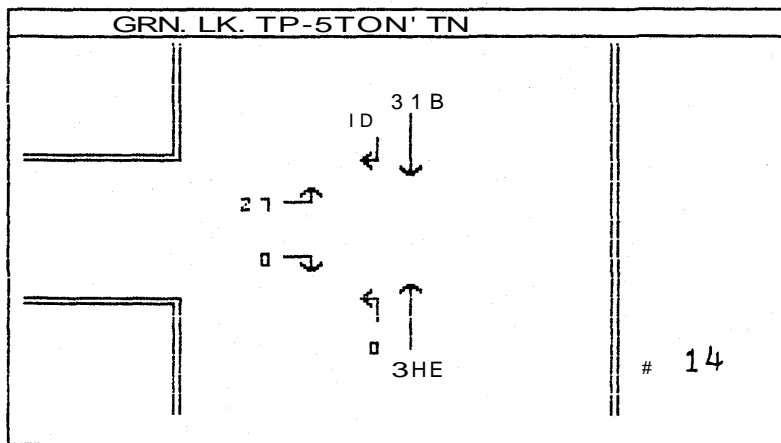
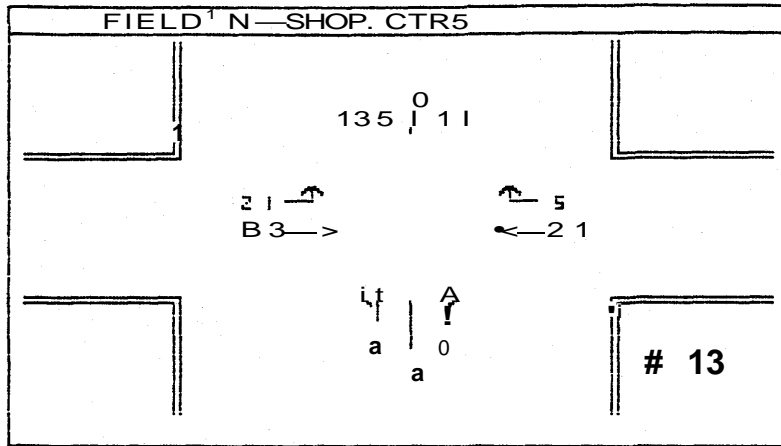
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PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
P.M. PEAK HOUR



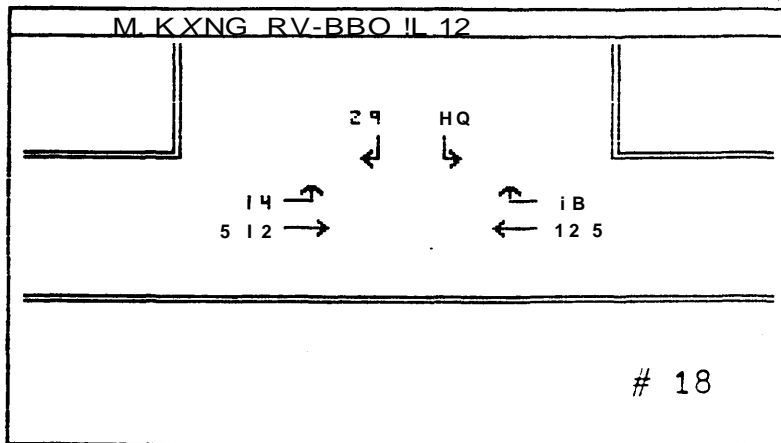
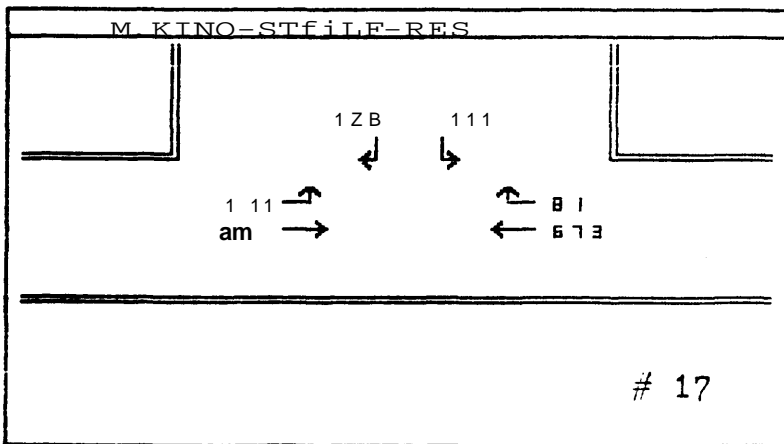
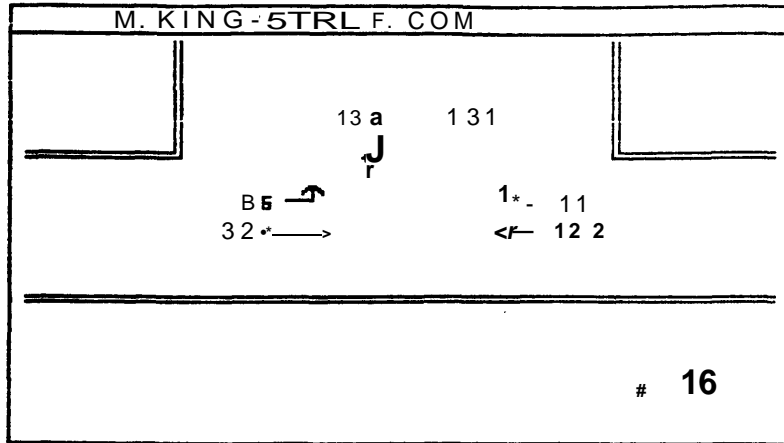
**EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
P.M. PEAK HOUR**



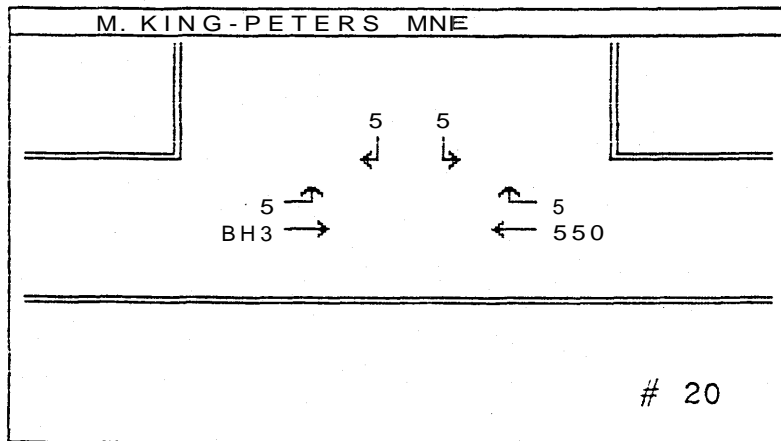
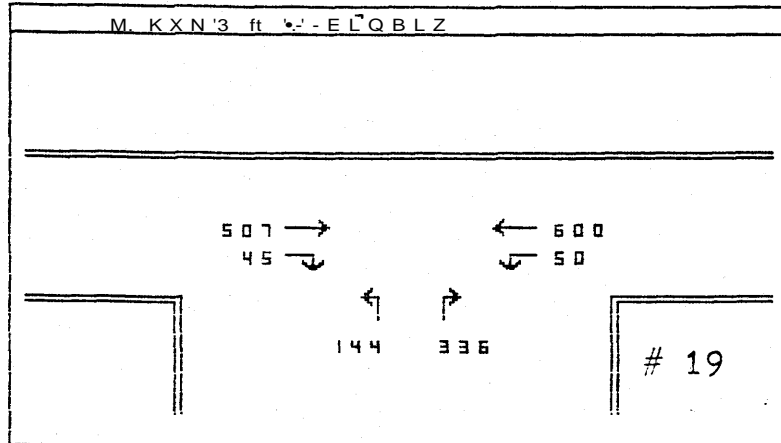
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 P.M. PEAK HOUR



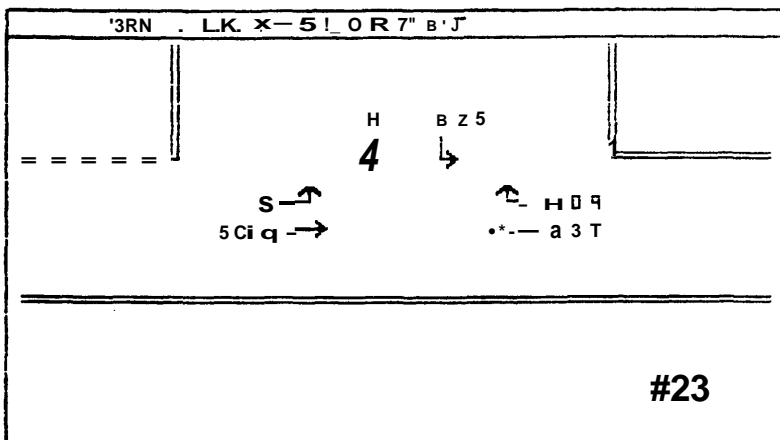
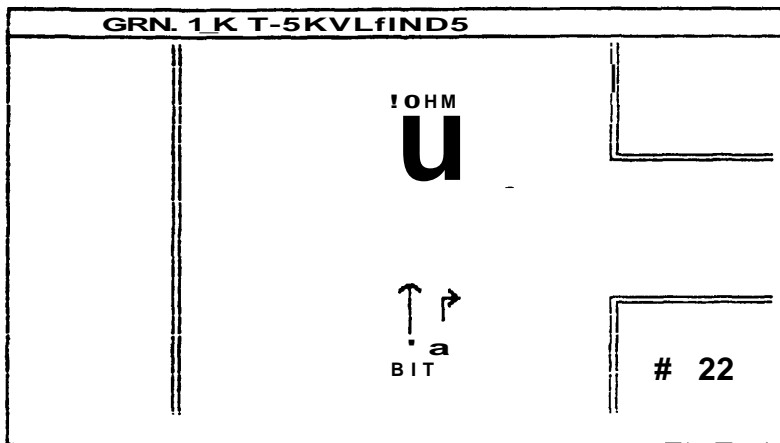
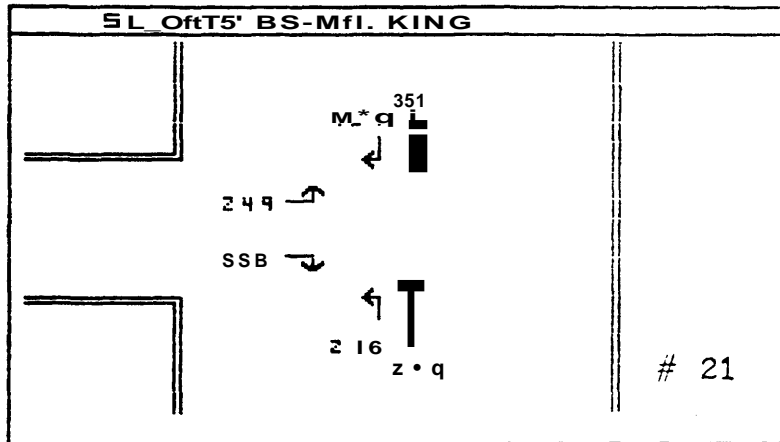
**EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
P.M. PEAK HOUR**



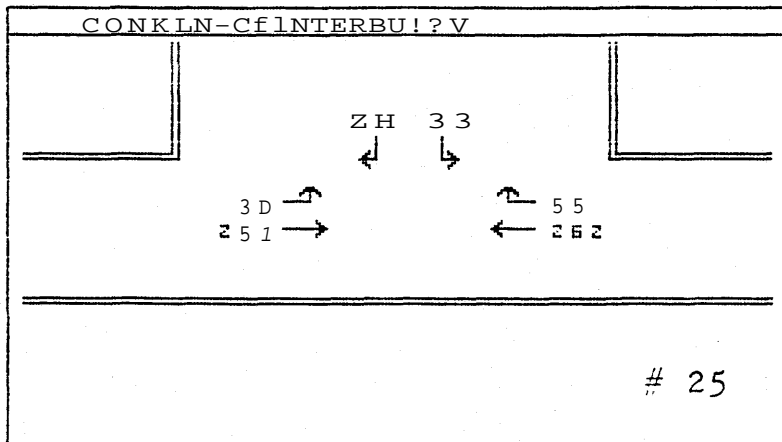
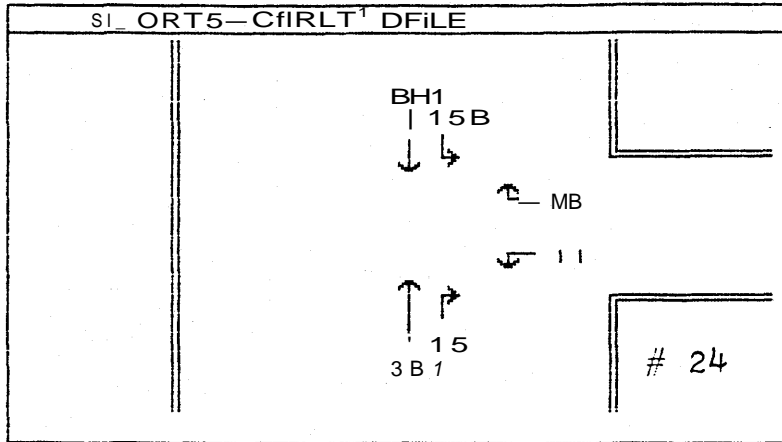
EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
P.M. PEAK HOUR



**EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
P.M. PEAK HOUR**



EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS ZONED
 P.M. PEAK HOUR



1983 BACKGROUND TRAFFIC AND SITE TRAFFIC

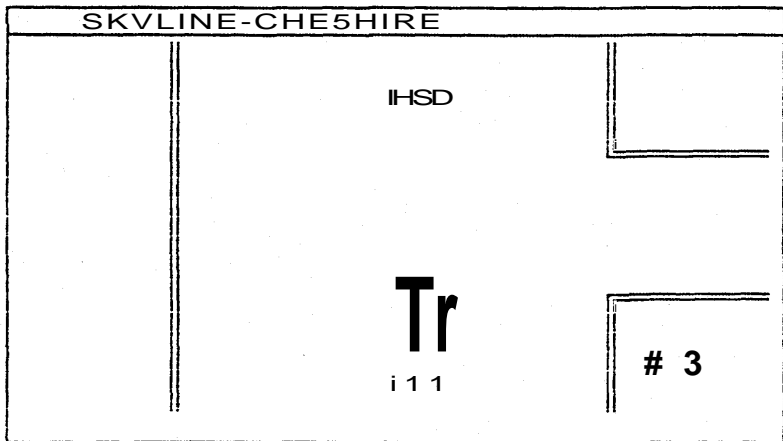
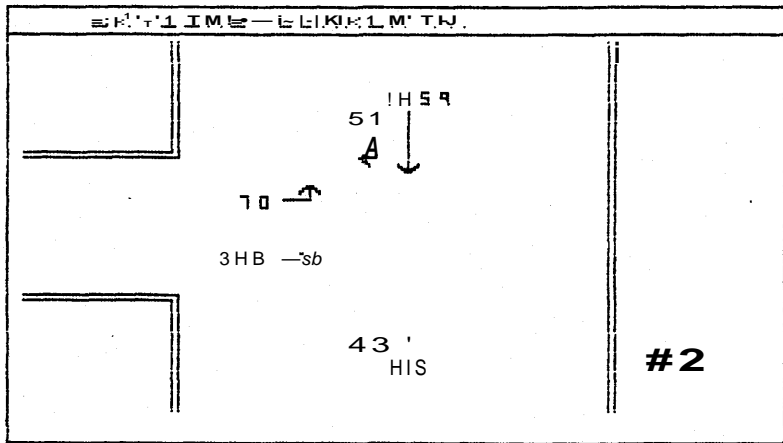
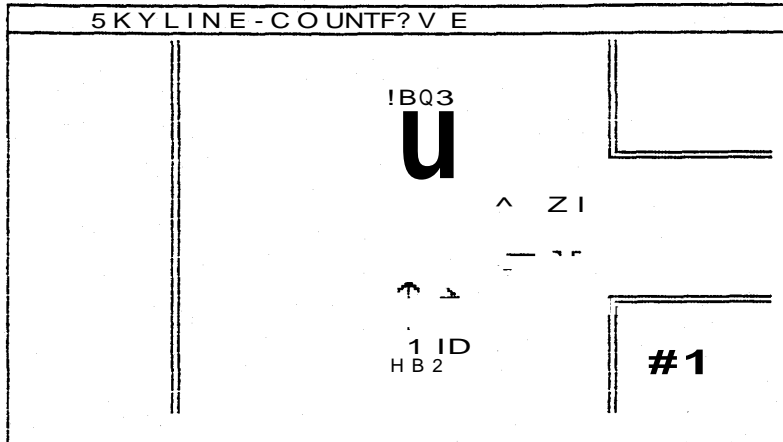
A.M. EXISTING TRAFFIC VOLUMES

WITH

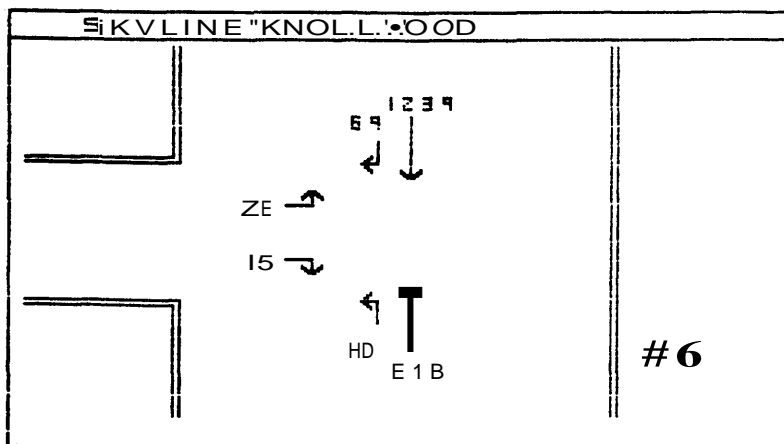
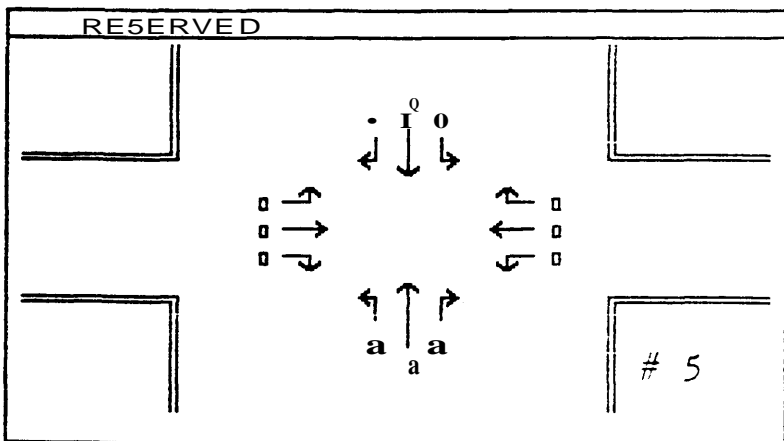
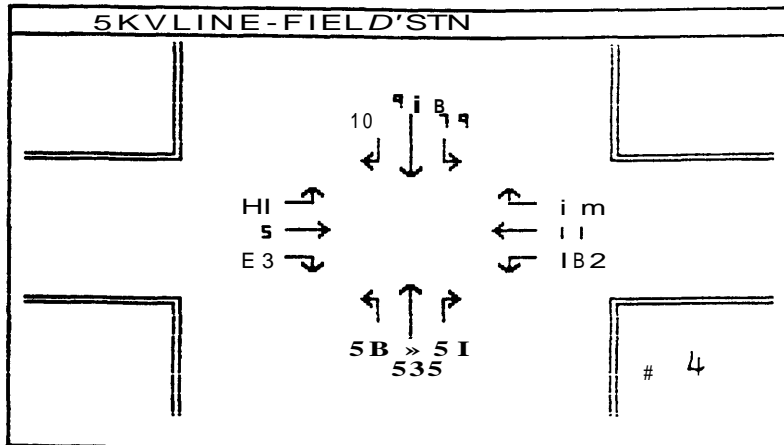
STUDY SITES DEVELOPED AS PROPOSED BY OTHERS

Access to Site 2 via Intersection 13
on Fieldstone Drive unless otherwise noted
(Last Sheet)

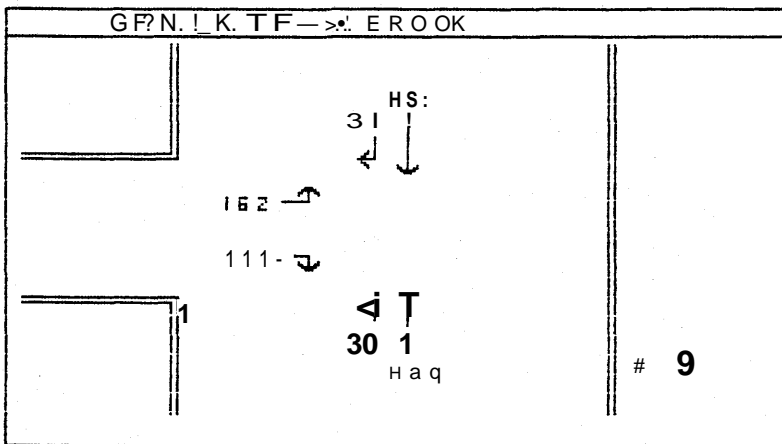
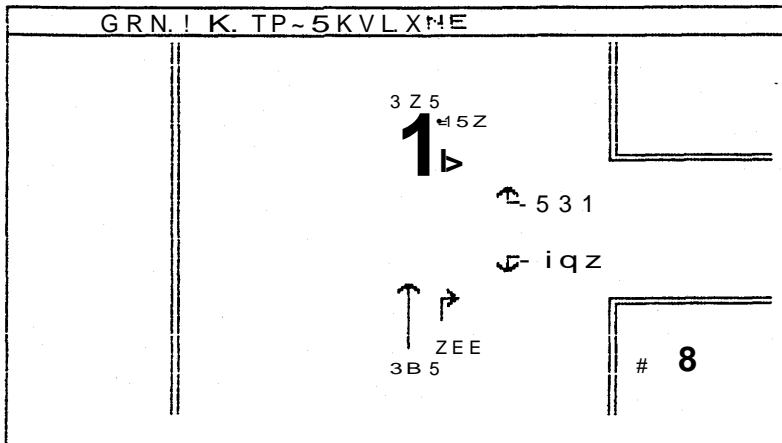
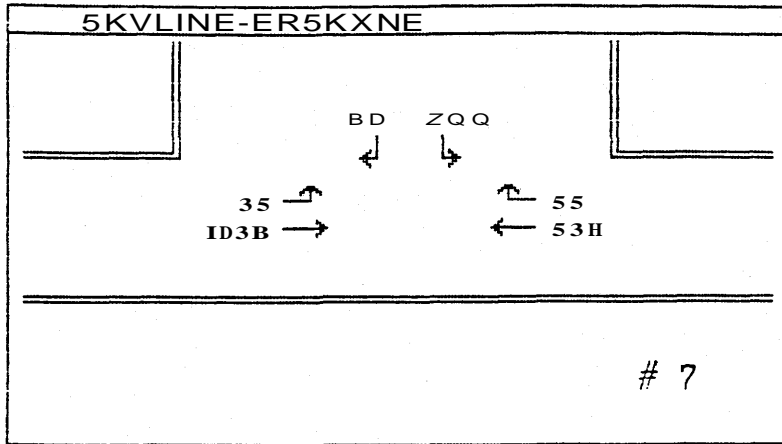
EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



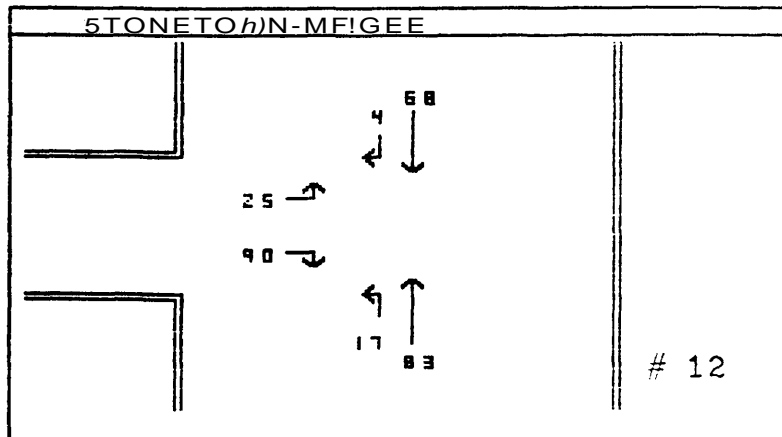
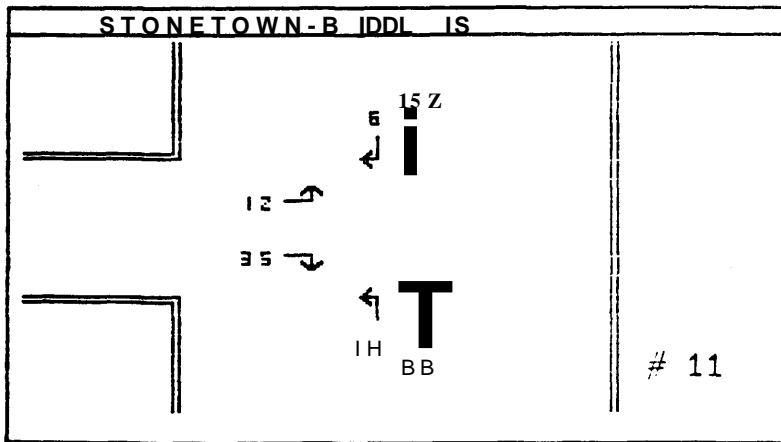
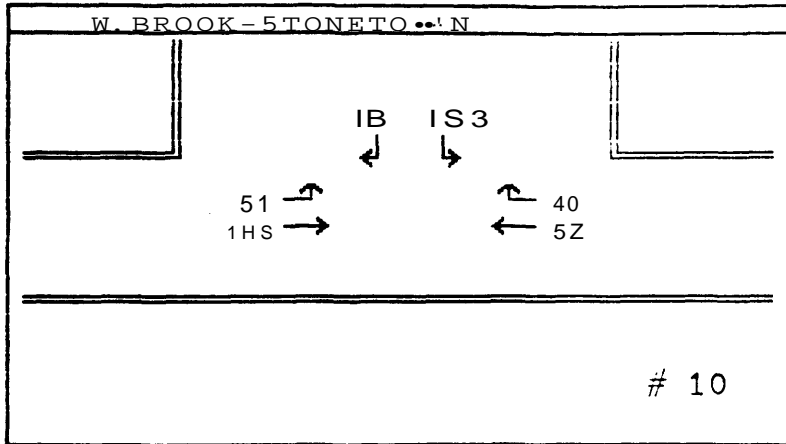
EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



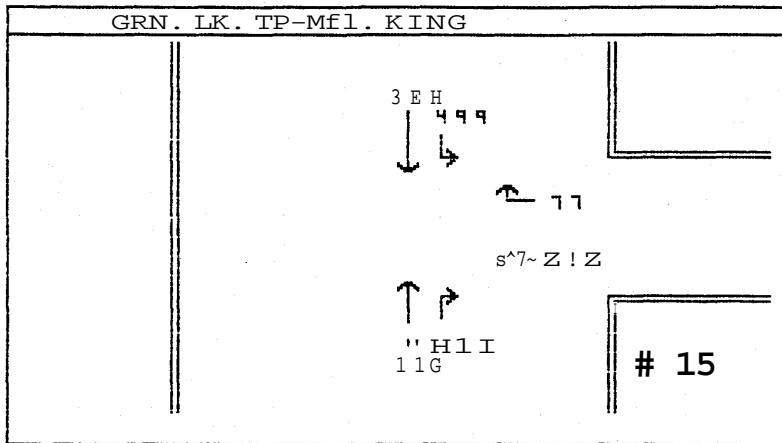
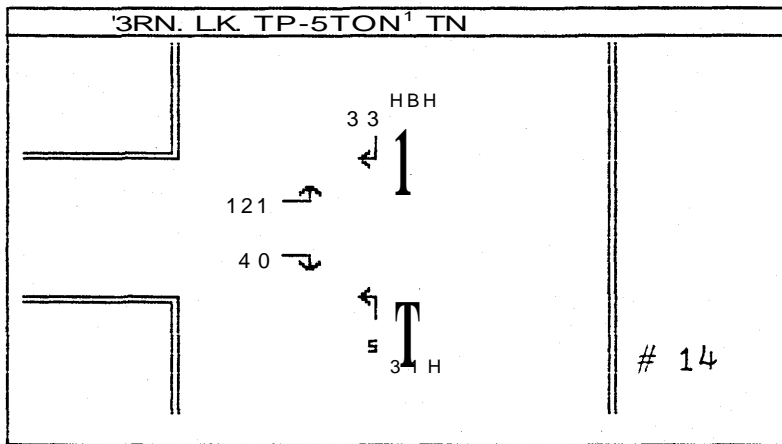
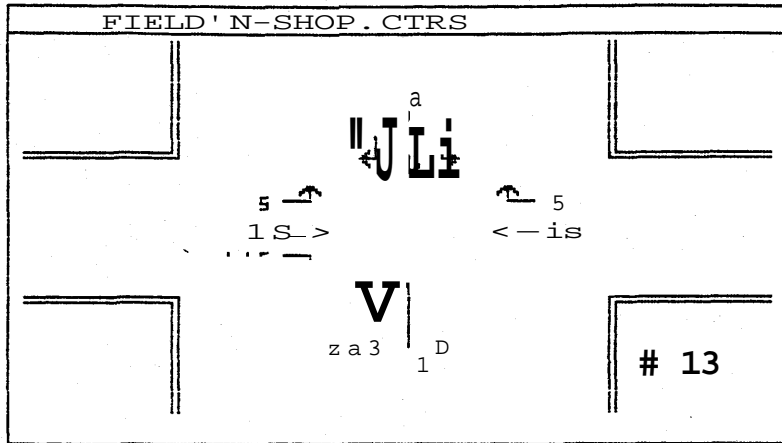
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 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



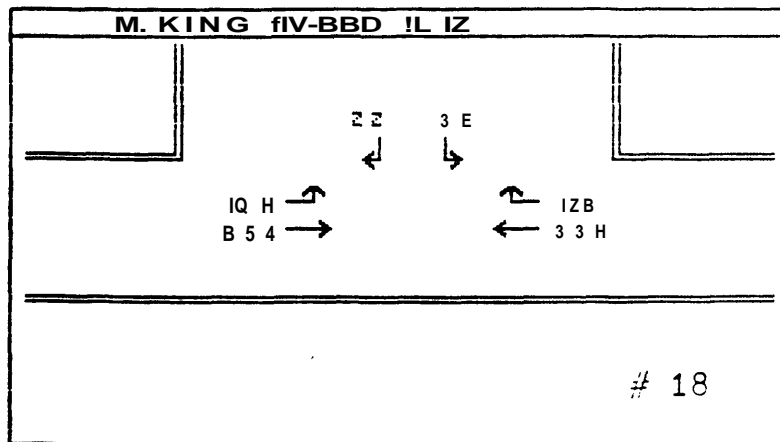
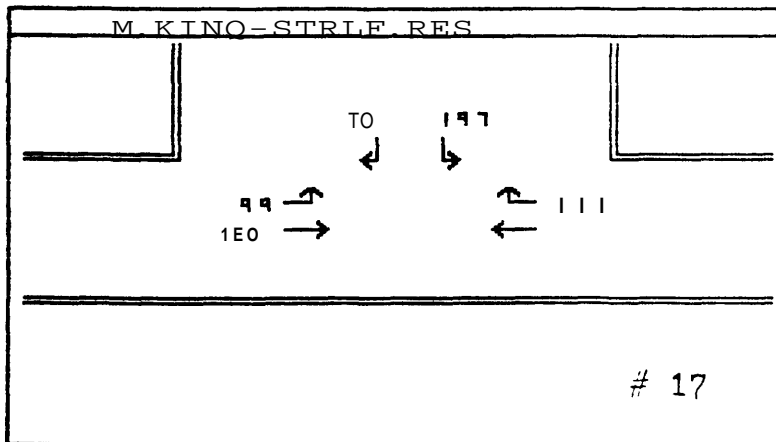
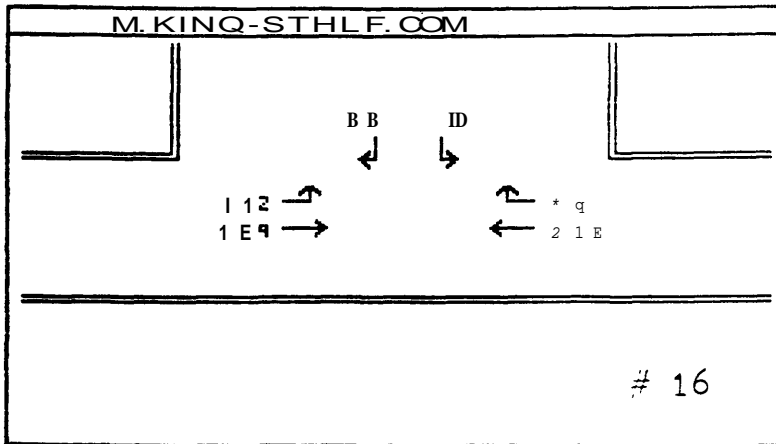
EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
A.M. PEAK HOUR



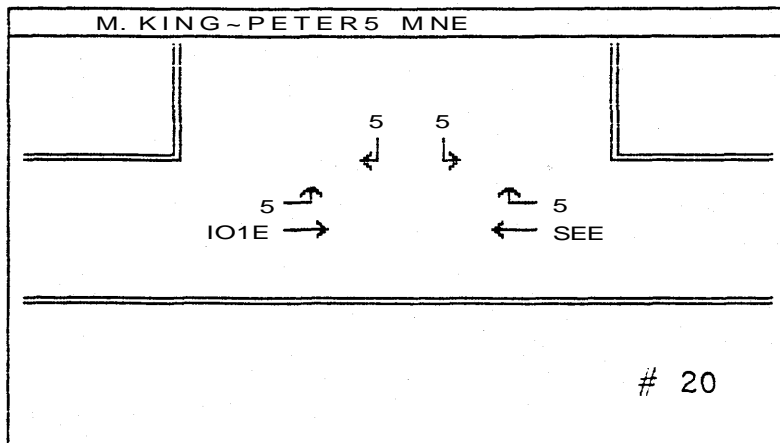
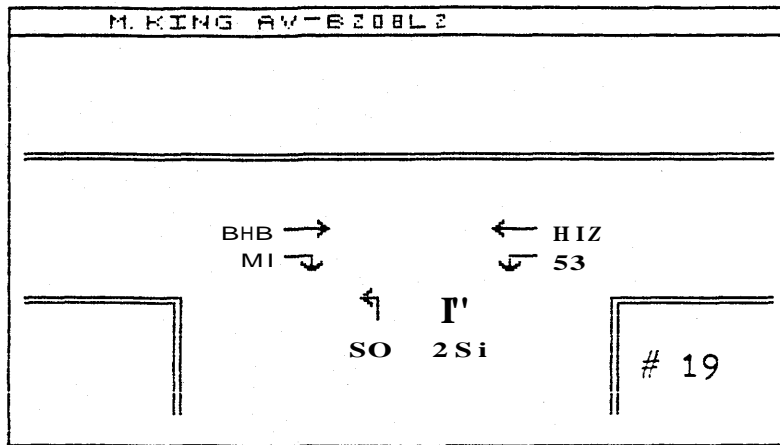
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 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



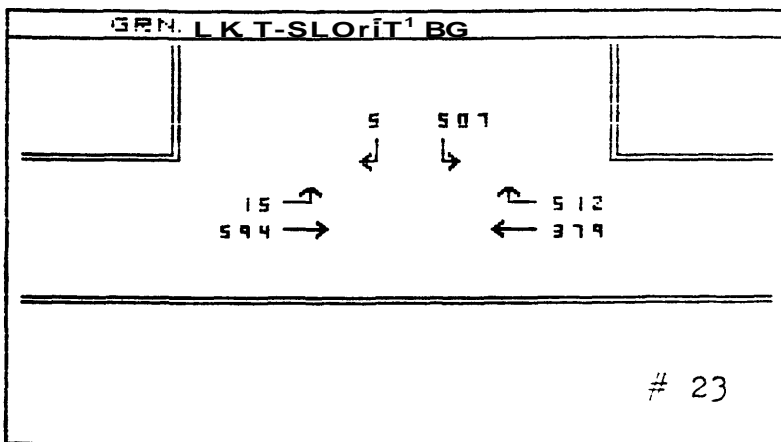
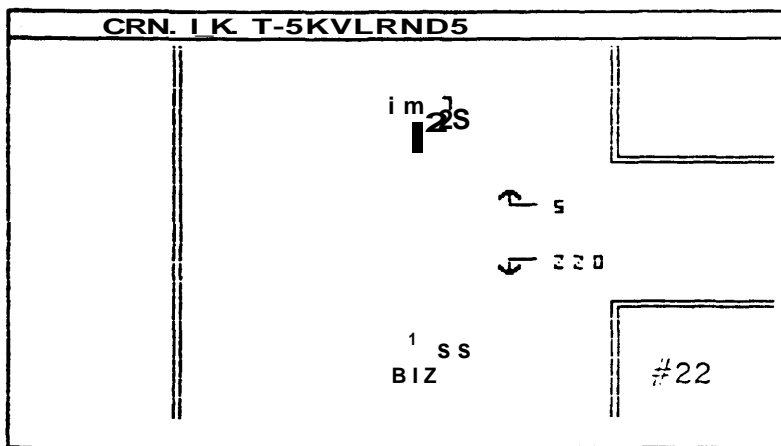
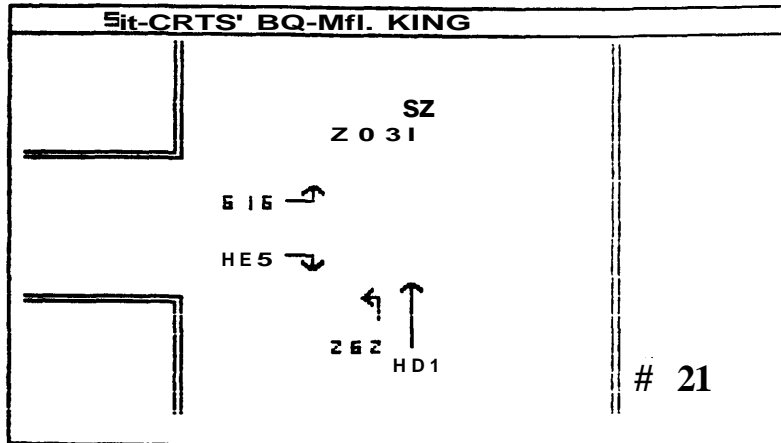
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 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



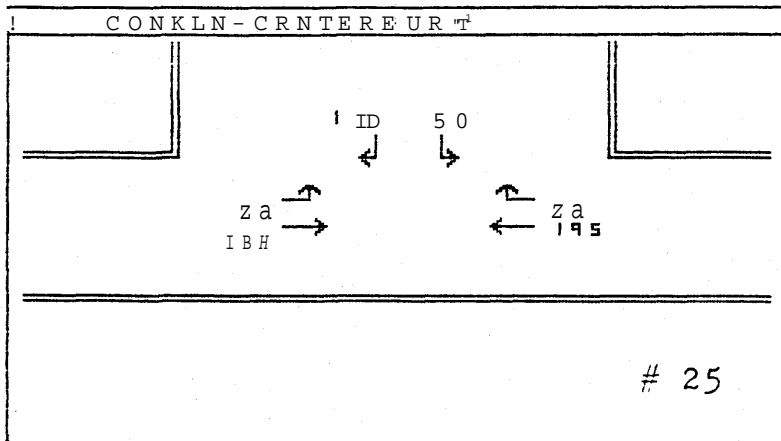
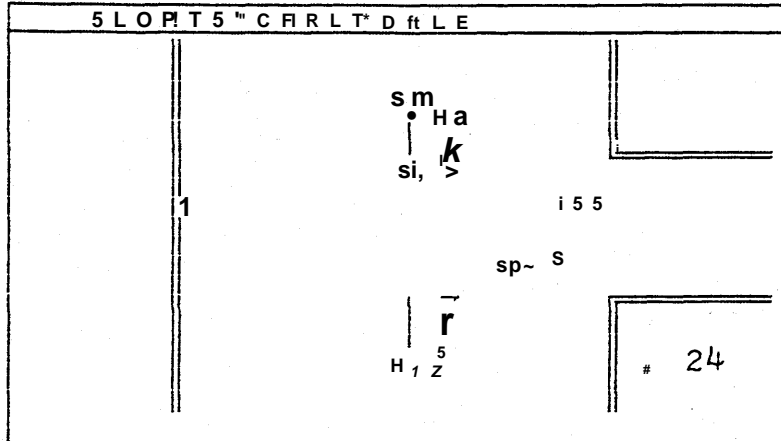
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PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
A.M. PEAK HOUR



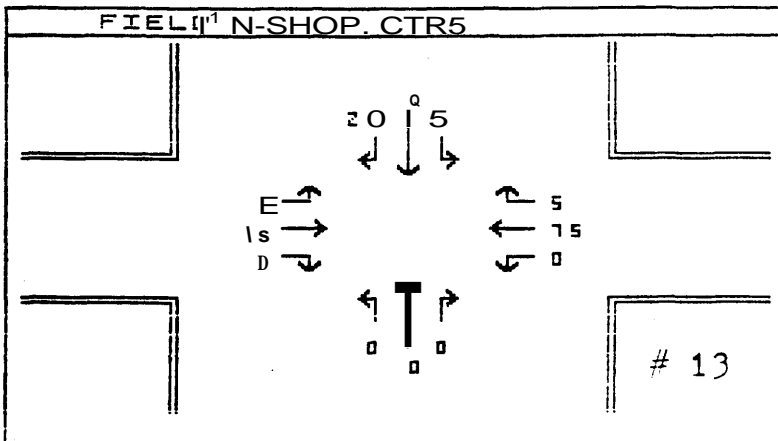
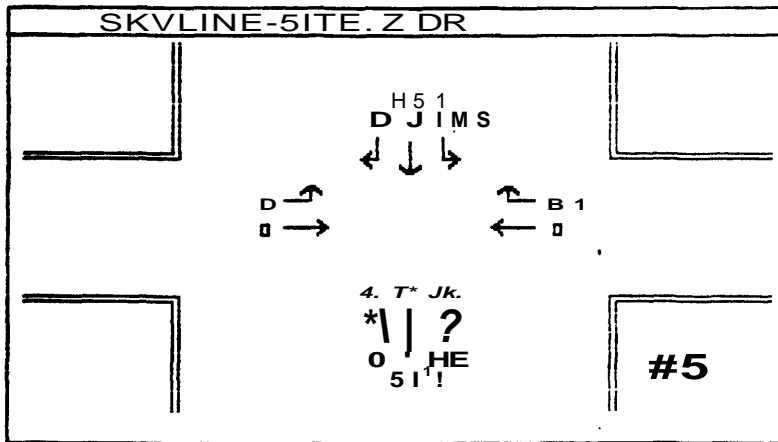
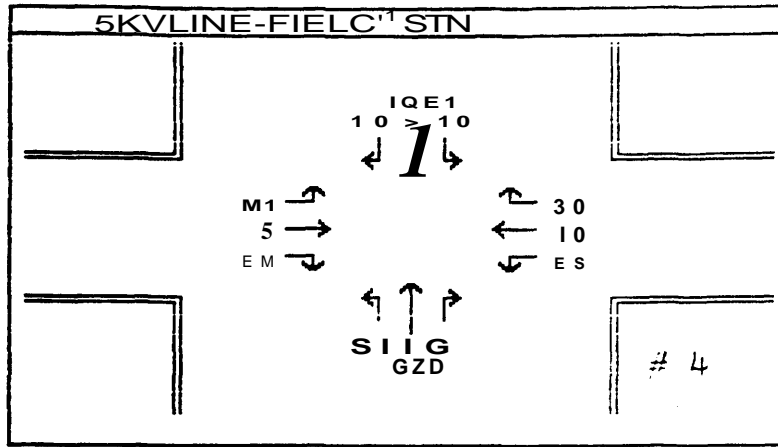
**EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
A.M. PEAK HOUR**



EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 A.M. PEAK HOUR



**EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
A.M. PEAK HOUR**



1983 BACKGROUND TRAFFIC AND SITS TRAFFIC

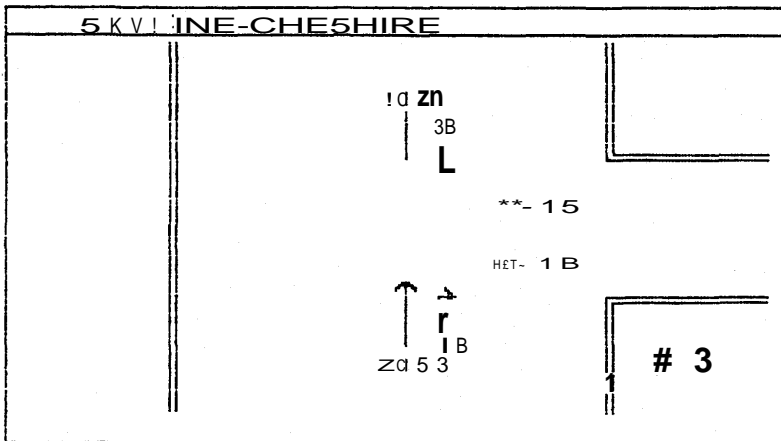
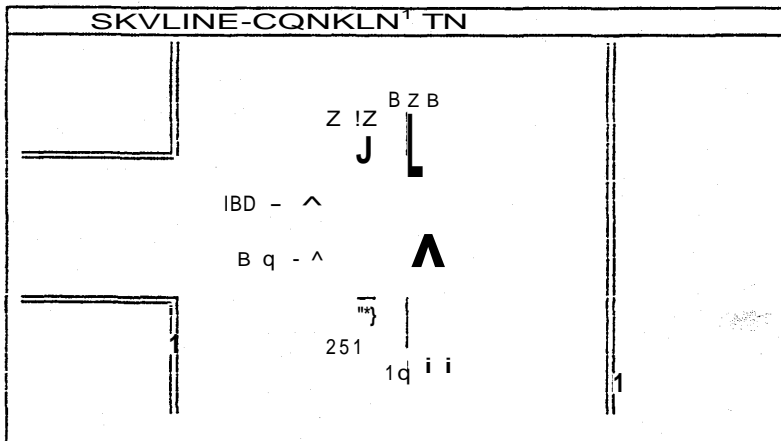
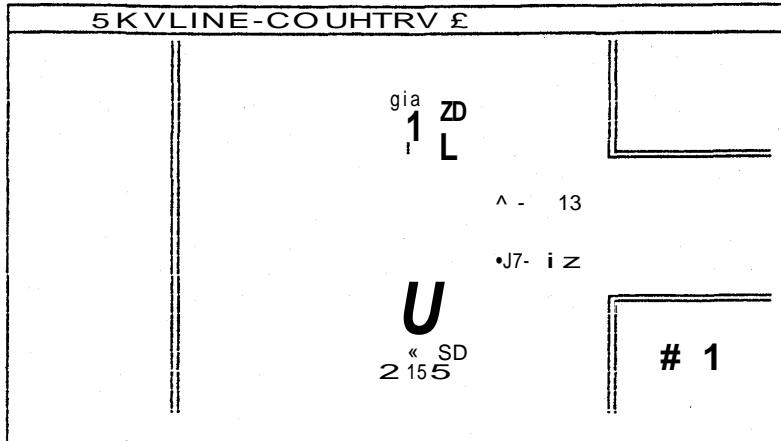
P.M. EXISTING TRAFFIC VOLUMES

WITH

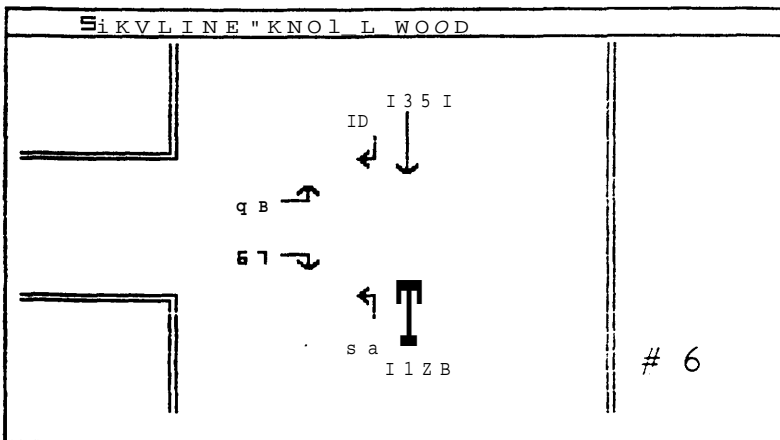
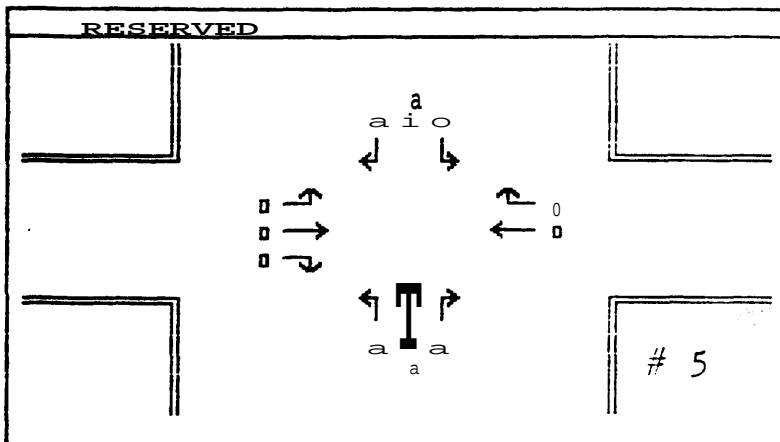
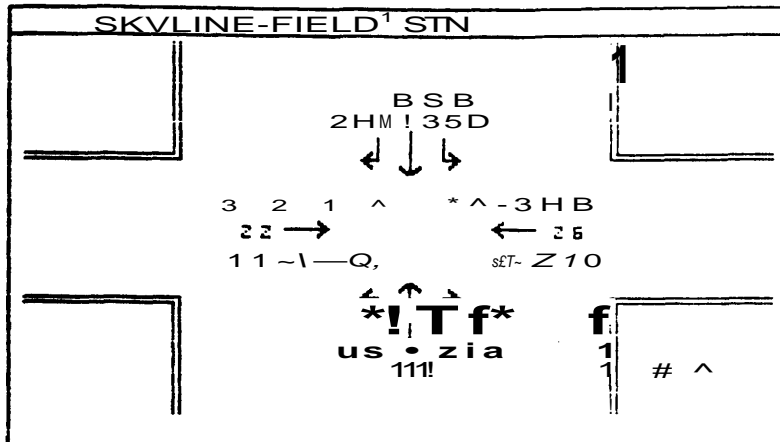
STUDY SITES DEVELOPED AS PROPOSED BY OTHERS

Access to Site 2 via Intersection 13
on Fieldstone Drive unless otherwise noted
(Last Sheet)

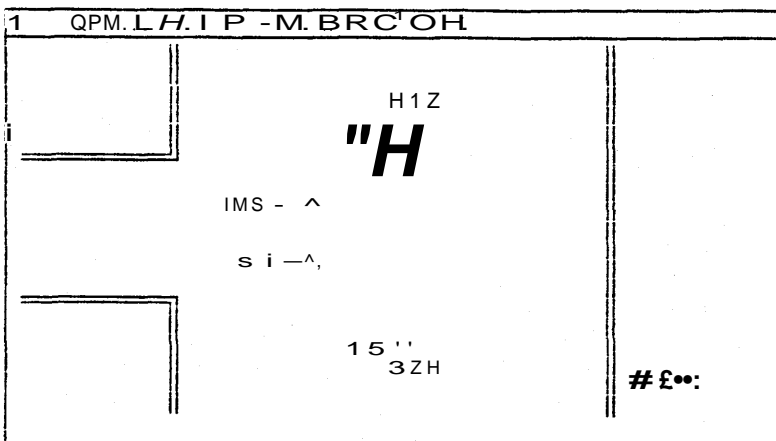
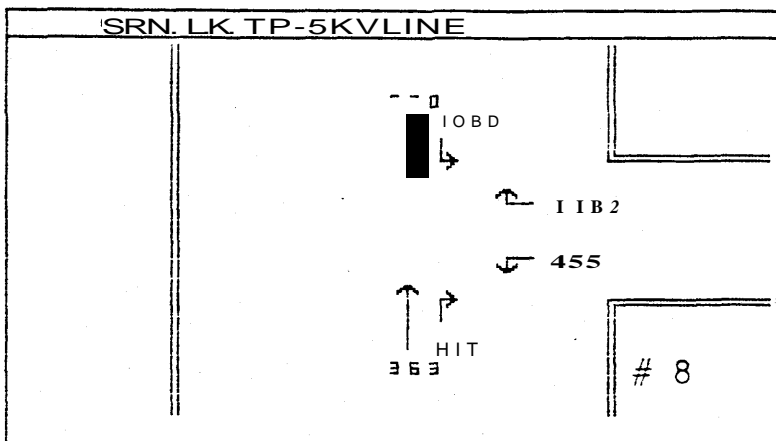
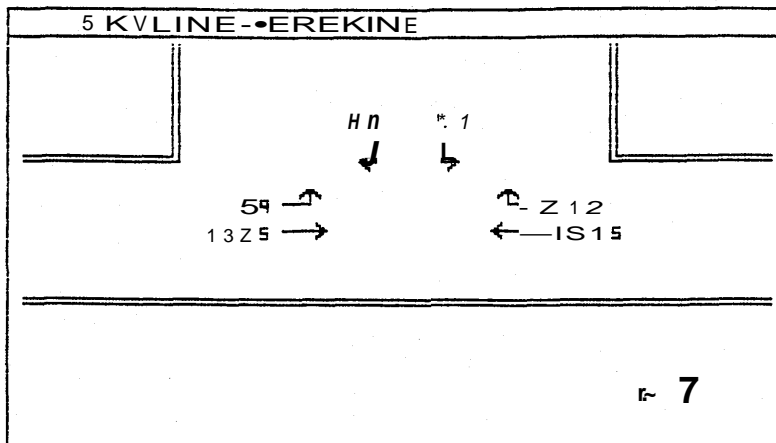
EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
P.M. PEAK HOUR

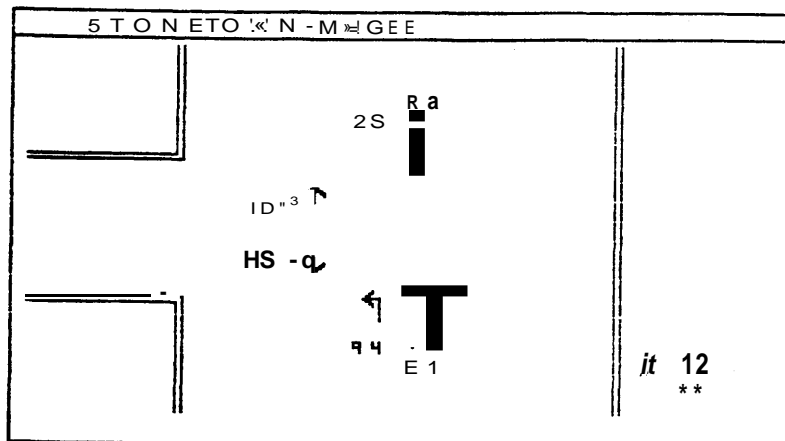
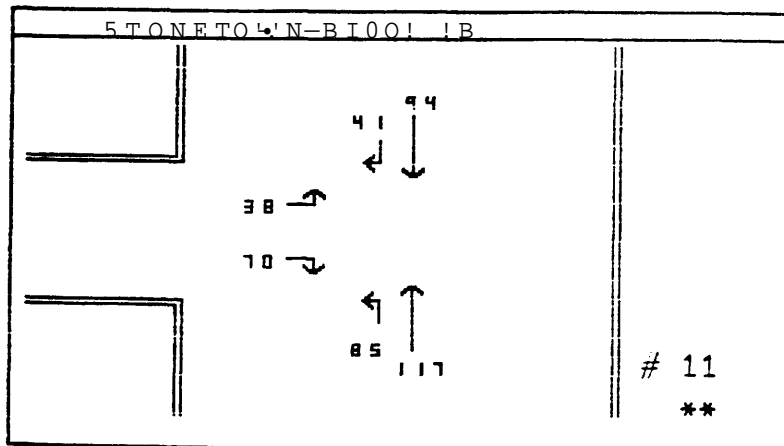
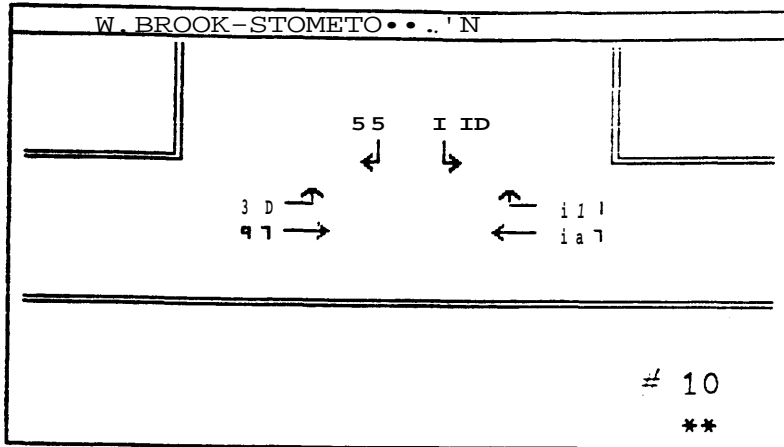


EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
P.M. PEAK HOUR



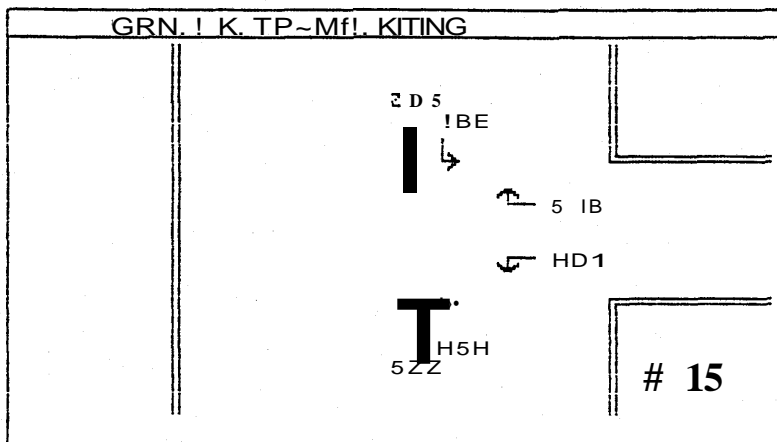
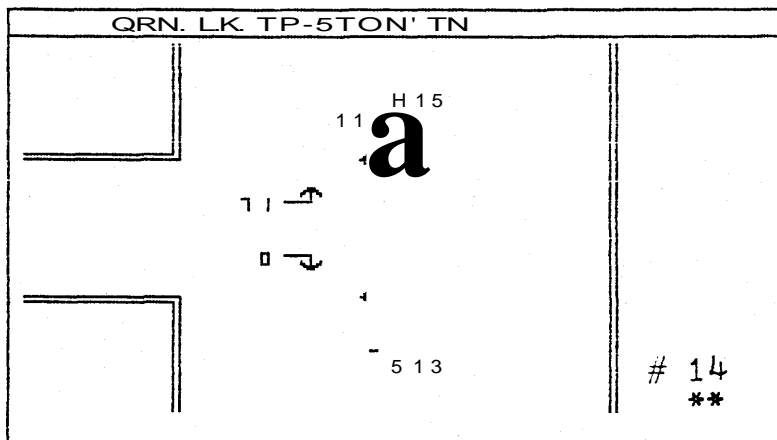
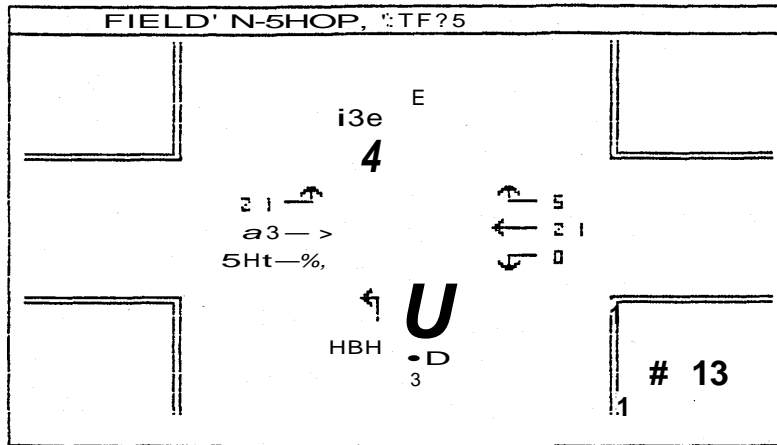
** NEW TRAFFIC ONLY

EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR



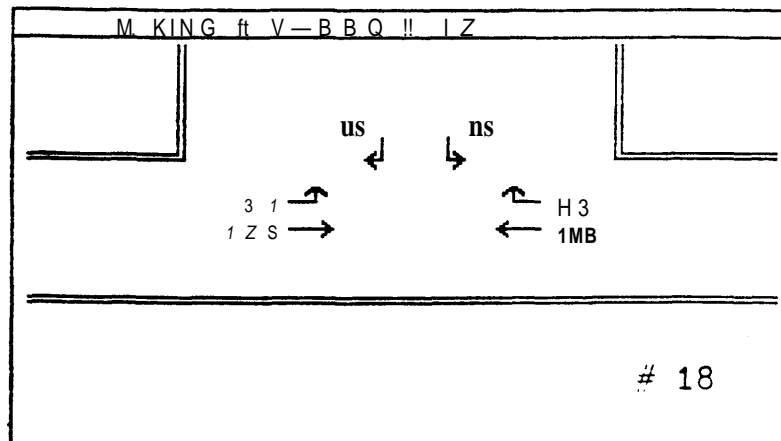
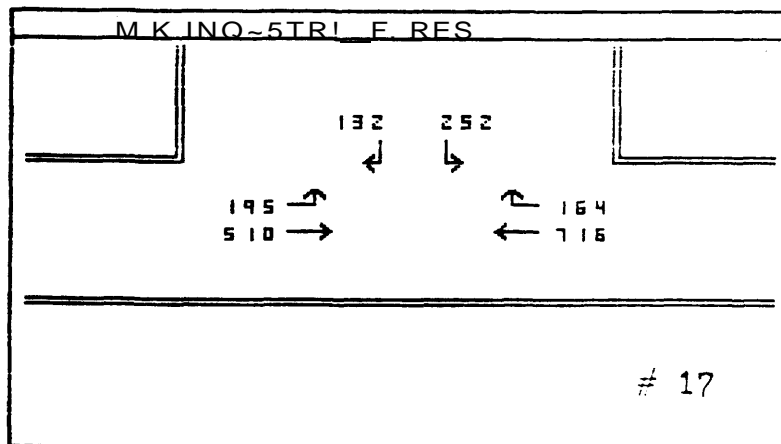
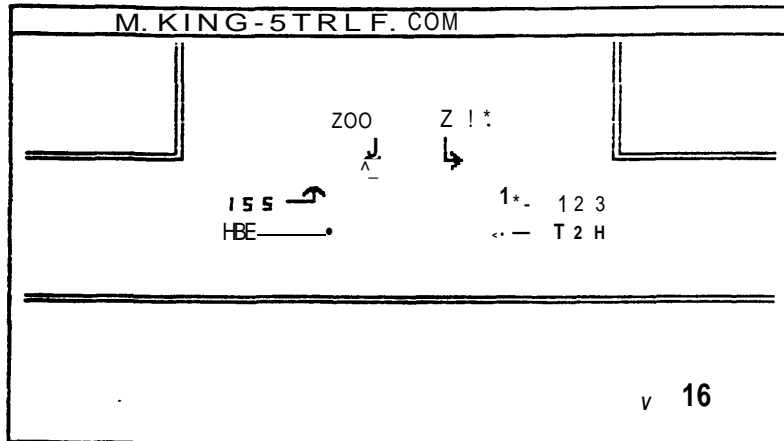
NEW TRAFFIC ONLY

EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
P.M. PEAK HOUR

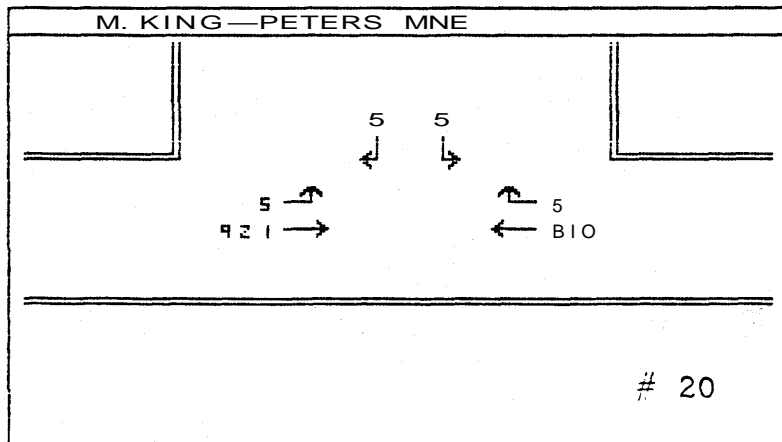
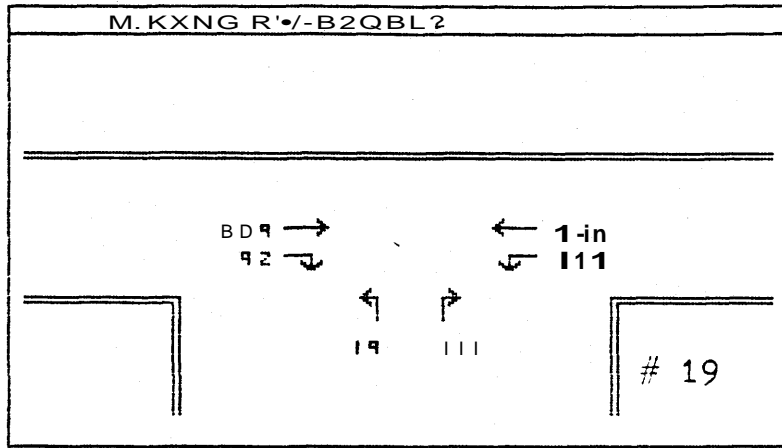


*• NEW TRAFFIC ONLY

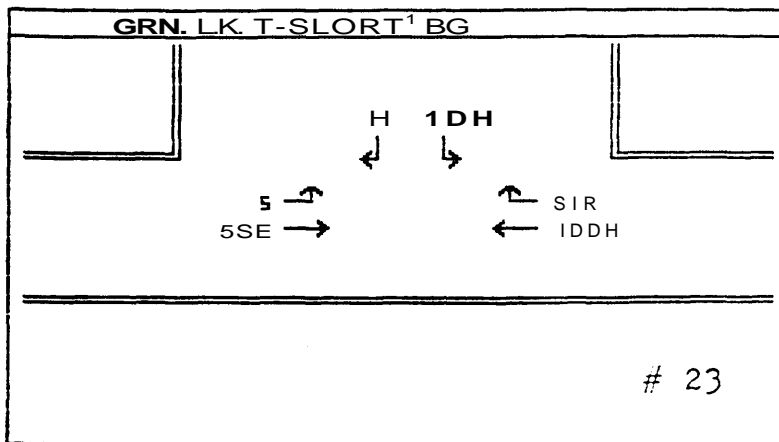
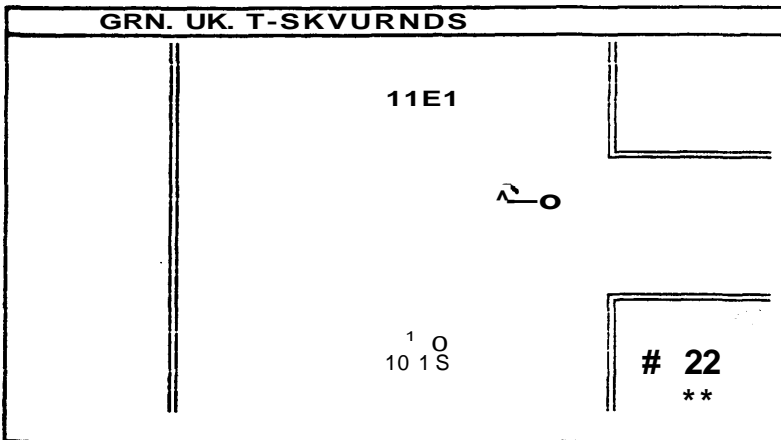
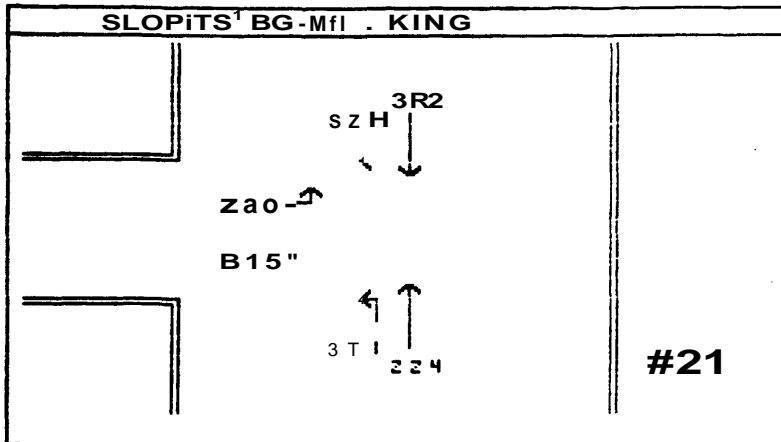
EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
P.M. PEAK HOUR



EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
P.M. PEAK HOUR

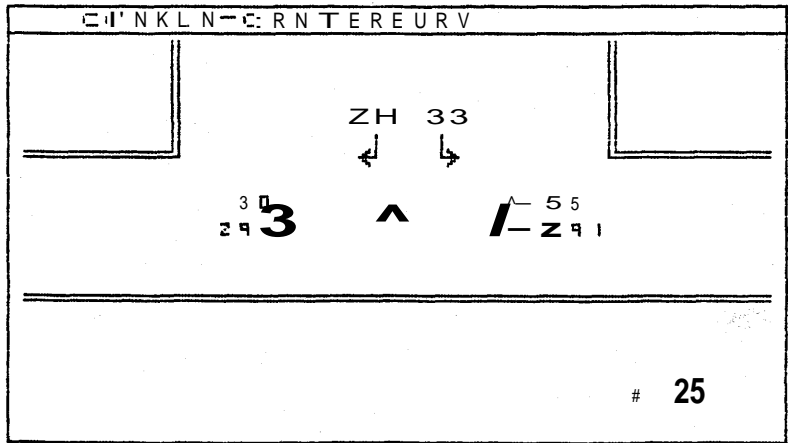
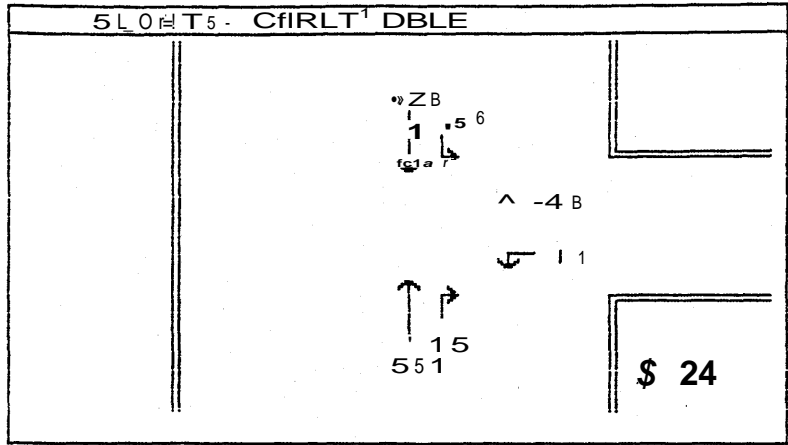


EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR



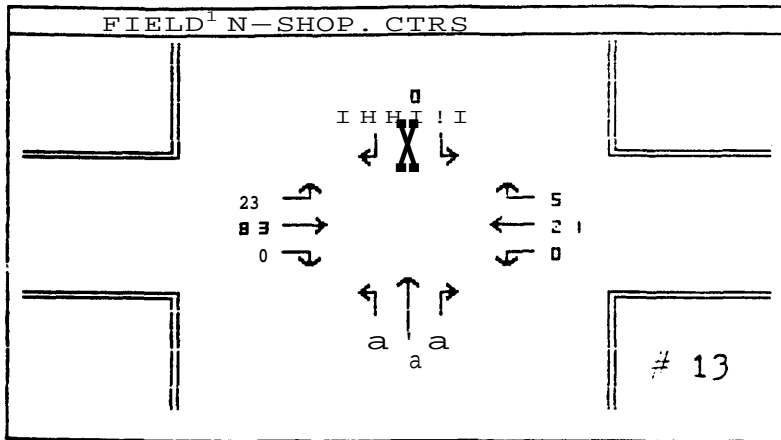
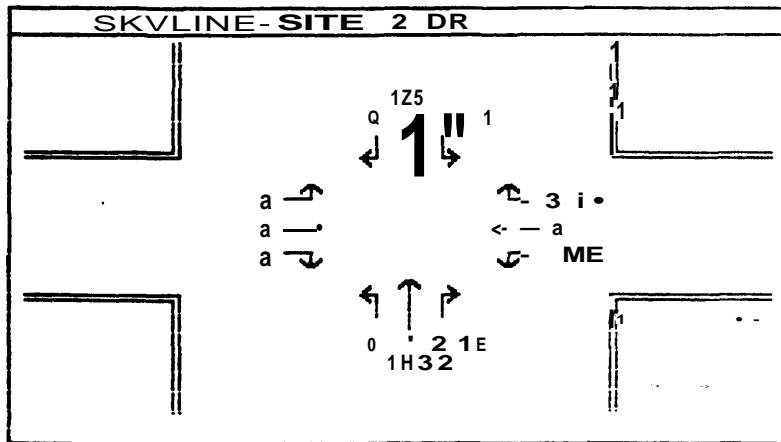
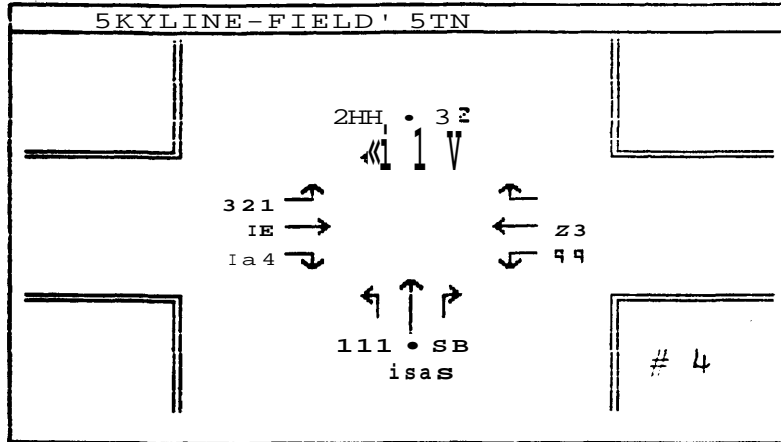
.. NEW TRAFFIC ONLY

EXISTING INTERSECTION TRAFFIC
 PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
 P.M. PEAK HOUR



** "

EXISTING INTERSECTION TRAFFIC
PLUS TRAFFIC FROM STUDY SITES DEVELOPED AS PROPOSED BY OTHERS
WITH ACCESS TO SITE 2 FROM SKYLINE DRIVE
P.M. PEAK HOUR



SUE PER APPROXIMATE TRAFFIC CONTROL MEASURES PRESENT

BAC> GROUND GROWTH: 37. PER YR
 YEARS = IP. GRTH FCTR 1.343916

TRIP GENERATION

INDEF VAR	UNITS	TRIP RATE		VEH. TRIPS	
		AM-IN	AM-OUT	AM-IN	AM-OUT
		FACTOR	FACTOR	VOLUME	VOLUME
BLOCK 752 LOT 1: SITE 1					
SINGLE FAM RES	20	.21	.55	4	11
TOWNHOUSE	0	.07	.37	0	0
RESERVED	0	0	0	0	0
TOTAL				4	11
BLOCK 877 LOT 16: SITE 2					
SINGLE FAM RES	34	.21	.55	7	19
TOWNHOUSE	0	.07	.37	0	0
COMMERCIAL	HO	.6	.3	84	42
RESERVED	0	0	0	0	0
TOTAL				91	61
BLOCK 800A LOT 3: SITE 3					
SINGLE FAM RES	0	.0	.0	0	0
TOWNHOUSE	0	.07	.37	0	0
APARTMENTS	0	.1	.4	0	0
COMMERCIAL	150	.5	.3	90	45
RESERVED	0	0	0	0	0
TOTAL				90	45
BLOCK 100 LOT 16: SITE 4					
SINGLE FAM RES	83	.21	.55	17	46
TOWNHOUSE	0	.07	.37	0	0
COMMERCIAL	0	.91	.8	0	0
RESERVED	0	0	0	0	0
TOTAL				17	46
BLOCK 201 LOT 1: SITE 5					
SINGLE FAM RES	0	.21	.55	0	0
TOWNHOUSE	217	.07	.37	15	80
COMMERCIAL	0	0	0	0	0
INDUSTRIAL	0	0	0	0	0
RESERVED	0	0	0	0	0
TOTAL				15	80
BLOCK 601 L12M3 SITE 6					
SINGLE FAM RES	0	.21	.55	0	0
TWO FAMILY RES	53	.1	.4	3	21
TOWNHOUSE	0	.1	.3	0	0
INDUSTRIAL	6	.8	1.3	48	8
RESERVED	0	0	0	0	0
TOTAL				53	29
BLOCK 508 LOT 2: SITE 7					
SINGLE FAM RES	0	0	0	0	0
INDUSTRIAL	48	.8	1.3	384	62
RESERVED	0	0	0	0	0
TOTAL				384	62
BLOCK 800 LOT 2: SITE 8					
APARTMENT-1 FAM	0	0	0	0	0
MUN.OFFICE-LIBR	30	.5	.05	15	2
MUN. D.P.W.	11	1	.5	11	6
PARK/RIDE LOT	60	1	.5	60	30
TOTAL				86	37
STERLING FOREST TR. SITE 9					
SINGLE FAM RES	483	.21	.55	101	266
TOWNHOUSE	0	.07	.37	0	0
APARTMENT	0	.1	.4	0	0
COMMERCIAL	0	.4	.2	0	0
OFFICE-LAB	250	1.79	.22	448	55
TOTAL				549	321

TRIP DISTRIBUTION PERCENT OF SITE TRAFFIC TO/FROM CORDON POINTS BY USE

COMPONENT	SKYLINE	CONKL'TN	BRN.LK.T	W.BROOK	GRH.LK.T	SLD'T'BG	FLD.SHOP	NEW SHOP	MUN.SITE	RING SHP	STRL FOR	TOTAL
	SOUTH-E	SOUTH	SOUTH	WEST	N-WEST	NORTH	EX IS N-E	S-E S 2	WEST	WEST NORTH CM		
BLOCK 752 LOT 1: SITE 1												
PERCENT:												
SINGLE FAM RES	52	11	8	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	11	8	1	3	16	1	1	3	1	3	100
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLTS:												
AM-IN	2	0	0	0	0	1	0	0	0	0	0	4
AM-OUT	6	1	1	0	0	2	0	0	0	0	0	11
BLOCK 877 LOT 16: SITE 2												
PERCENT:												
SINGLE FAM RES	52	11	8	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	11	8	1	3	16	1	1	3	1	3	100
COMMERCIAL	20	10	15	10	15	15	0	0	0	0	5	90
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLTS:												
AM-IN	21	9	13	8	13	14	0	0	0	0	4	83
AM-OUT	18	6	8	4	7	9	0	0	1	0	3	57
BLOCK 800A LOT 3: SITE 3												
PERCENT:												
SINGLE FAM RES	52	11	8	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	11	8	1	3	16	1	1	3	1	3	100
APARTMENTS	52	11	8	1	3	16	1	1	3	1	3	100
COMMERCIAL	20	10	15	10	15	15	0	0	0	0	5	70
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLTS:												
AM-IN	19	9	14	9	14	14	0	0	0	0	5	81
AM-OUT	9	5	7	5	7	7	0	0	0	0	2	41
BLOCK 100 LOT 16: SITE 4												
PERCENT:												
SINGLE FAM RES	22	30	19	1	3	16	1	1	3	1	3	100
TOWNHOUSE	22	30	19	1	3	16	1	1	3	1	3	100
COMMERCIAL	20	12	12	5	15	15	0	0	0	0	0	79
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLTS:												
AM-IN	4	5	3	0	1	3	0	0	1	0	1	17
AM-OUT	10	14	9	0	1	7	0	0	1	0	1	46
BLOCK 201 LOT 1: SITE 5												
PERCENT:												
SINGLE FAM RES	22	30	19	1	3	16	1	1	3	1	3	100
TOWNHOUSE	22	30	19	1	3	16	1	1	3	1	3	100
COMMERCIAL	0	0	0	0	0	0	0	0	0	0	0	0
INDUSTRIAL	0	0	0	0	0	0	0	0	0	0	0	0
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLTS:												
AM-IN	3	5	3	0	0	2	0	0	0	0	0	15
AM-OUT	18	24	15	1	2	13	1	1	2	1	2	80
BLOCK 601 L.12S.13 SITE 6												
PERCENT:												
SINGLE FAM RES	52	12	7	1	3	16	1	1	3	1	3	100
TWO FAMILY RES	52	12	7	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	12	7	1	3	16	1	1	3	1	3	100
INDUSTRIAL	25	20	20	5	10	20	0	0	0	0	0	100
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLTS:												
AM-IN	15	10	10	2	5	10	0	0	0	0	0	53
AM-OUT	13	4	3	1	1	5	0	0	1	0	1	29
BLOCK 508 LOT 2: SITE 7												
PERCENT:												
SINGLE FAM RES	52	12	7	1	3	16	1	1	3	1	3	100
MOBILE HOME PRK	25	20	20	5	10	20	0	0	0	0	0	100
INDUSTRIAL	25	20	20	5	10	20	0	0	0	0	0	100
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLTS:												
AM-IN	96	77	77	19	38	77	0	0	0	0	0	384
AM-OUT	16	12	12	3	6	12	0	0	0	0	0	62
BLOCK 800 LOT 2: SITE 8												
PERCENT:												
APARTMENT-1 FAM	52	11	8	1	3	16	1	1	3	1	3	100
COMMERCIAL	25	20	20	10	10	10	0	0	0	0	5	100
MUN.OFFICE-LIBR	25	20	20	10	10	10	0	0	0	0	5	100
MUN. D.P.W.	25	20	20	10	10	10	0	0	0	0	5	100
PARK/RIDE LOT	20	15	15	10	10	10	0	0	0	0	5	85
TRAFFIC VOLTS:												
AM-IN	19	14	14	9	9	9	0	0	0	0	4	77
AM-OUT	8	6	6	4	4	4	0	0	0	0	2	33
STERLING FOREST TR SITE 9												
PERCENT:												
SINGLE FAM RES	52	12	7	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	12	7	1	3	16	1	1	3	1	3	100
APARTMENT	52	12	7	1	3	16	1	1	3	1	3	100
COMMERCIAL	15	10	10	10	10	15	0	0	0	0	5	100
OFFICE-LAB	15	10	10	10	10	15	0	0	0	0	5	75
TRAFFIC VOLTS:												
AM-IN	120	57	52	46	48	83	1	1	3	1	25	437
AM-OUT	144	37	24	8	13	51	3	3	8	3	11	307

SUE BEJ. EL-ORHEAT-T4*
 SUE BEJ. EL-ORHEAT-T4*
 SUE BEJ. EL-ORHEAT-T4*

BACKGROUND GROWTH: 37 PER YR
 YEAR: 10 GRTR FCTR 1.343916

TRIP GENERATION

INDEX VAR	UNITS	TRIP RATE		VEH. TRIPS	
		PM-IN	PM-OUT	PM-IN	PM-OUT
		FACTOR	FACTOR	VOLUME	VOLUME
BLOCK 752 LOT 1: SITE 1					
SINGLE FAM RES	20	.63	.37	13	7
TOWNHOUSE	0	0	0	0	0
RESERVED	0	0	0	0	0
TOTAL				13	7
BLOCK 877 LOT 16: SITE 2					
SINGLE FAM RES	34	.63	.37	21	13
TOWNHOUSE	0	0	0	0	0
COMMERCIAL	140	2.9	3.1	406	434
RESERVED	0	0	0	0	0
TOTAL				427	447
BLOCK 800ft LOT 3: SITE 3					
SINGLE FAM RES	0	0	0	0	0
TOWNHOUSE	0	0	0	0	0
APARTMENTS	0	0	0	0	0
COMMERCIAL	150	2.9	3.1	435	465
RESERVED	0	0	0	0	0
TOTAL				435	465
BLOCK 100 LOT 16: SITE 4					
SINGLE FAM RES	83	.63	.37	52	31
TOWNHOUSE	0	0	0	0	0
COMMERCIAL	0	0	0	0	0
RESERVED	0	0	0	0	0
TOTAL				52	31
BLOCK 201 LOT 31: SITE 5					
SINGLE FAM RES	0	0	0	0	0
TOWNHOUSE	217	.37	.18	80	39
COMMERCIAL	0	0	0	0	0
INDUSTRIAL	0	0	0	0	0
RESERVED	0	0	0	0	0
TOTAL				80	39
BLOCK 601 L12&13 SITE 6					
SINGLE FAM RES	0	0	0	0	0
TWO FAMILY RES	53	.4	.2	21	11
TOWNHOUSE	0	0	0	0	0
INDUSTRIAL	6	2	10	12	60
RESERVED	0	0	0	0	0
TOTAL				33	71
BLOCK 508 LOT 2: SITE 7					
SINGLE FAM RES	0	0	0	0	0
MOBILE HOME PRK.	0	0	0	0	0
INDUSTRIAL	48	2	10	54	450
RESERVED	0	0	0	0	0
TOTAL				54	450
TOTAL: 96 480					
BLOCK 800 LOT 2: SITE 8					
SINGLE FAM RES	0	0	0	0	0
OFFICE-LAB	0	0	0	0	0
OFFICE-LIBR	30	2.5	2.5	75	75
UN. D.P.W.	11	.5	1	6	11
INDUSTRIAL LOT	60	.5	1	30	60
TOTAL				111	146
STERLING FOREST TR. SITE 9					
SINGLE FAM RES	483	.63	.37	304	179
TOWNHOUSE	0	0	0	0	0
APARTMENT	0	0	0	0	0
COMMERCIAL	0	0	0	0	0
OFFICE-LAB	250	.24	1.63	60	408
TOTAL				364	587

TRIP DISTRIBUTION PERCENT OF SITE TRAFFIC TO/FROM CORDON POINTS BY USE

COMPONENT	SKYLINE	CDNKL	TN GRN	LK.T	W. BROOK	GRN.LK.T	SLQAT'BG	FLD.SHOP	NEW SHOP	MUN.SITE	RING SHP	STRL FOR	TOTAL
	SOUTH-E	SOUTH	SOUTH	WEST	N-WEST	NORTH	EXIS N-E	S-E S 2	WEST	WEST	NORTH CH		
BLOCK 752 LOT 1: SITE 1													
PERCENT:													
SINGLE FAM RES	49	0	7	1	2	14	4	4	3	4	3	100	
TOWNHOUSE	0	0	0	0	0	0	0	0	0	0	0	0	
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0	
TRAFFIC VOLS:													
PM-IN	6	1	1	0	0	2	1	1	0	1	0	13	
PM-OUT	4	1	1	0	0	1	0	0	0	0	0	7	
BLOCK 877 LOT 16: SITE 2													
PERCENT:													
SINGLE FAM RES	49	9	7	1	2	14	4	4	3	4	3	100	
TOWNHOUSE	0	0	0	0	0	0	0	0	0	0	0	0	
COMMERCIAL	17	12	12	10	12	17	0	0	0	0	5	85	
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0	
TRAFFIC VOLS:													
PM-IN	51	51	50	41	49	75	1	1	1	1	21	367	
PM-OUT	30	32	33	41	52	75	1	1	1	1	22	31	
BLOCK 800 LOT 3: SITE 3													
PERCENT:													
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0	
TOWNHOUSE	0	0	0	0	0	0	0	0	0	0	0	0	
APARTMENTS	0	0	0	0	0	0	0	0	0	0	0	0	
COMMERCIAL	17	12	12	10	12	17	0	0	0	0	5	85	
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0	
TRAFFIC VOLS:													
PM-IN	74	52	52	44	52	74	0	0	0	0	22	379	
PM-OUT	79	56	56	47	51	79	0	0	0	0	23	395	
BLOCK 100 LOT 16: SITE 4													
PERCENT:													
SINGLE FAM RES	20	27	18	1	2	14	4	4	3	4	3	100	
TOWNHOUSE	0	0	0	0	0	0	0	0	0	0	0	0	
COMMERCIAL	0	0	0	0	0	0	0	0	0	0	0	0	
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0	
TRAFFIC VOLS:													
PM-IN	10	14	9	1	1	7	2	2	2	2	2	52	
PM-OUT	6	8	6	0	1	4	1	1	1	1	1	31	
BLOCK 201 LOT 31: SITE 5													
PERCENT:													
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0	
TOWNHOUSE	20	27	18	1	2	14	4	4	3	4	3	100	
COMMERCIAL	0	0	0	0	0	0	0	0	0	0	0	0	
INDUSTRIAL	0	0	0	0	0	0	0	0	0	0	0	0	
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0	
TRAFFIC VOLS:													
PM-IN	16	22	14	1	2	11	3	3	2	3	2	86	
PM-OUT	11	11	7	0	1	5	2	2	1	2	1	39	
BLOCK 601 L.12M3 SITE 6													
PERCENT:													
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0	
TWO FAMILY RES	49	10	6	1	2	14	4	4	3	4	3	100	
TOWNHOUSE	0	0	0	0	0	0	0	0	0	0	0	0	
INDUSTRIAL	25	20	20	5	10	20	0	0	0	0	0	100	
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0	
TRAFFIC VOLS:													
PM-IN	13	5	4	1	2	5	1	1	1	1	1	33	
PM-OUT	20	13	13	3	6	13	0	0	0	0	0	71	
BLOCK SOB LOT 2: SITE 7													
PERCENT:													
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0	
MOBILE HOME PRK	0	0	0	0	0	0	0	0	0	0	0	0	
INDUSTRIAL	25	20	20	5	10	20	0	0	0	0	0	100	
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0	
TRAFFIC VOLS:													
PM-IN	24	19	19	5	10	19	0	0	0	0	0	96	
PM-OUT	120	96	96	24	48	96	0	0	0	0	0	480	
STERLING FOREST TR. SITE 9													
PERCENT:													
SINGLE FAM RES	42	8	5	1	2	11	4	4	3	4	3	87	
TOWNHOUSE	0	0	0	0	0	0	0	0	0	0	0	0	
APARTMENT	0	0	0	0	0	0	0	0	0	0	0	0	
COMMERCIAL	0	0	0	0	0	0	0	0	0	0	0	0	
OFFICE-LAB	14	10	14	10	14	14	5	5	0	5	5	96	
TRAFFIC VOLS:													
PM-IN	136	30	24	9	14	42	15	15	9	15	12	322	
PM-OUT	132	55	46	43	61	77	28	28	5	28	26	517	

Table with columns: NETWORK ASSIGNMENT, MOVEMENT, EXISTING (GRND CNT, BLOCK 75, BLOCK 87, BLOCK 80, BLOCK 10, BLOCK 20, BLOCK 40, BLOCK 50, BLOCK 80, STERLING), FUTURE (TOT VOL). Rows include various intersection and movement combinations like 1. SKYLINE-COUNTRY'E, 2. SKYLINE-CONKLN'TN, 3. SKYLINE-CHESHIRE, etc.

* NEW TRAFFIC ONLY

SHE DEVELOPMENT TRAFFIC ESTIMATION SPREAD SHEET

BACKGROUND GROWTH: 3% PER YR
 YEARS = 10 3RTH FCTR 1.343914

TRIP GENERATION

INDEP USE	UNITS	TRIP RATE		VEH. TRIPS	
		AM-IN	AM-OUT	AM-IN	AM-OUT
		FACTOR	FACTOR	VOLUME	VOLUME
BLOCK 752 LOT 1: SITE 1					
SINGLE FAM RES	0	.21	.55	0	0
TOWNHOUSE	230	.07	.37	20	104
RESERVED	0	0	0	0	0
TOTAL				20	104
BLOCK 877 LOT 16: SITE 2					
SINGLE FAM RES	0	.21	.55	0	0
TOWNHOUSE	450	.07	.37	32	167
COMMERCIAL	140	.6	.3	84	42
RESERVED	0	0	0	0	0
TOTAL				116	209
BLOCK 800A LOT 3: SITE 3					
SINGLE FAM RES	0	0	0	0	0
TOWNHOUSE	0	0	0	0	0
APARTMENTS	0	0	0	0	0
COMMERCIAL	150	.6	.3	90	45
RESERVED	0	0	0	0	0
TOTAL				90	45
BLOCK 100 LOT 16: SITE 4					
SINGLE FAM RES	0	.21	.55	0	0
TOWNHOUSE	95	.07	.37	7	35
COMMERCIAL	20	.91	.18	18	16
RESERVED	0	0	0	0	0
TOTAL				25	51
BLOCK 201 LOT 31: SITE 5					
SINGLE FAM RES	0	.21	.55	0	0
TOWNHOUSE	314	.07	.37	22	116
COMMERCIAL	0	0	0	0	0
INDUSTRIAL	0	0	0	0	0
RESERVED	0	0	0	0	0
TOTAL				22	116
BLOCK 601 L12U3: SITE 6					
SINGLE FAM RES	0	.21	.55	0	0
TKO FAMILY RES	53	.1	.4	5	21
TOWNHOUSE	0	.07	.37	0	0
INDUSTRIAL	30	.8	.37	240	39
RESERVED	0	0	1.3	0	0
TOTAL				245	60
BLOCK 503 LOT 1: SITE 7					
SINGLE FAM RES	0	0	0	0	0
MOBILE HOME PRK	272	.13	.39	95	278
INDUSTRIAL	0	0	1.3	0	0
RESERVED	0	0	0	0	0
TOTAL				95	278
BLOCK 800 LOT 2: SITE B					
APARTMENT-1 FAM	0	0	0	0	0
COMMERCIAL	0	0	0	0	0
MUN.OFFICE-LIBR	30	.5	.05	15	2
MUN. D.P.W.	11	1	.5	11	6
PARK/RIDE LOT	60	1	.5	60	30
TOTAL				86	37
STERLING FOREST TR. SITE 9					
SINGLE FAM RES	350	.21	.55	74	193
TOWNHOUSE	220	.07	.37	15	81
APARTMENT	300	.1	.4	30	120
COMMERCIAL	100	.4	.2	40	20
OFFICE-LIBR	250	1.79	.22	448	55
TOTAL				606	469

TRIP DISTRIBUTION PERCENT OF SITE TRAFFIC TO/FROM CORDON POINTS BY USE

COMPONENT	SKYLINE CONCL. TR. N. BROOK BR. HILKTSLOAT BR. LIN. SHOP NEW SHOP MUN. SITE RING SHP STR. TOR											TOTAL
	SOUTH-E	SOUTH	SOUTH	WEST	N-WEST	NORTH	EXIS N-E	S-E S 2	WEST	WEST	NORTH	
BLOCK 752 LOT 1: SITE 1												
PERCENT:												
SINGLE FAM RES	52	11	8	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	11	8	1	3	16	1	1	3	1	3	100
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLLS:												
AM-IN	10	2	2	0	1	3	0	0	1	0	1	20
AM-OUT	54	11	8	1	3	17	1	1	3	1	3	104
BLOCK 877 LOT 16: SITE 2												
PERCENT:												
SINGLE FAM RES	52	11	8	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	11	8	1	3	16	1	1	3	1	3	100
COMMERCIAL	20	10	15	10	15	15	0	0	0	0	5	90
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLLS:												
AM-IN	33	12	15	9	14	18	0	0	1	0	5	107
AM-OUT	95	23	15	11	33	33	2	2	5	2	7	204
BLOCK 800A LOT 3: SITE 3												
PERCENT:												
SINGLE FAM RES	52	11	8	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	11	8	1	3	16	1	1	3	1	3	100
APARTMENTS	52	11	8	1	3	16	1	1	3	1	3	100
COMMERCIAL	20	10	15	10	15	15	0	0	0	0	0	85
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLLS:												
AM-IN	7	7	7	5	7	14	0	0	0	0	0	77
AM-OUT	9	5	7	5	7	7	0	0	0	0	0	73
BLOCK 100 LOT 16: SITE 4												
PERCENT:												
SINGLE FAM RES	22	30	19	1	3	16	1	1	3	1	3	100
TOWNHOUSE	22	30	19	1	3	16	1	1	3	1	3	100
COMMERCIAL	20	12	12	5	15	15	0	0	0	0	0	79
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLLS:												
AM-IN	5	4	3	1	3	4	0	0	0	0	0	21
AM-OUT	11	12	9	1	3	8	0	0	1	0	1	48
BLOCK 201 LOT 31: SITE 5												
PERCENT:												
SINGLE FAM RES	22	30	19	1	3	16	1	1	3	1	3	100
TOWNHOUSE	22	30	19	1	3	16	1	1	3	1	3	100
COMMERCIAL	0	0	0	0	0	0	0	0	0	0	0	0
INDUSTRIAL	0	0	0	0	0	6	0	0	0	0	0	6
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLLS:												
AM-IN	5	7	4	0	1	4	0	0	1	0	1	22
AM-OUT	26	35	22	1	3	19	1	1	3	1	3	116
BLOCK 601 L.12M3 SITE 6												
PERCENT:												
SINGLE FAM RES	52	12	7	1	3	16	1	1	3	1	3	100
TWO FAMILY RES	52	12	7	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	12	7	1	3	16	1	1	3	1	3	100
INDUSTRIAL	25	20	20	0	10	20	0	0	0	0	0	95
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLLS:												
AM-IN	63	49	48	0	24	49	0	0	0	0	0	233
AM-OUT	21	10	9	0	5	11	0	0	1	0	1	59
BLOCK 508 LOT 2: SITE 7												
PERCENT:												
SINGLE FAM RES	52	12	7	1	3	16	1	1	3	1	3	100
MOBILE HOME PRK	52	12	7	1	3	16	1	1	3	1	3	100
INDUSTRIAL	25	20	20	5	10	20	0	0	0	0	0	100
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLLS:												
AM-IN	49	11	7	1	3	15	1	1	3	1	3	95
AM-OUT	145	33	19	3	8	45	3	3	8	3	8	278
BLOCK 800 LOT 2: SITE 8												
PERCENT:												
APARTMENT-1 FAM	52	11	8	1	3	16	1	1	3	1	3	100
COMMERCIAL	25	20	20	10	10	10	0	0	0	0	5	166
MUN.OFFICE-LIBR	25	20	20	10	10	10	0	0	0	0	5	100
MUN. D.P.W.	25	20	20	10	10	10	0	0	0	0	5	100
PARK/RIDE LOT	20	15	15	10	10	10	0	0	0	0	8	35
TRAFFIC VOLLS:												
AM-IN	19	14	14	9	9	9	0	0	0	0	4	78
AM-OUT	8	6	6	4	4	4	0	0	0	0	2	33
SITE 1												
PERCENT:												
SINGLE FAM RES	52	12	7	1	3	16	1	1	3	1	3	100
TOWNHOUSE	52	12	7	1	3	16	1	1	3	1	3	100
APARTMENT	52	12	7	1	3	16	1	1	3	1	3	100
COMMERCIAL	15	10	10	10	10	15	0	0	0	0	5	75
OFFICE-LIBR	15	10	10	10	10	15	0	0	0	0	5	75
TRAFFIC VOLLS:												
AM-IN	135	63	57	50	52	92	1	1	4	1	28	485
AM-OUT	214	55	35	11	19	74	4	4	12	4	14	450

SITE DEVELOPMENT TRAFFIC ESTIMATION SPREAD SHEET

BACKGROUND GROWTH: 3% PER YR
 YEARS = 10 GRTH FCTR 1.343916

TRIP GENERATION

INDEX VEH	UNITS	TRIP RATE		VEH. TRIPS	
		PM-IN	PM-OUT	PM-IN	PM-OUT
		FACTOR	FACIOP?	VOLUME	VOLUME
BLOCK 752 LOT 1:					
SINGLE FAM RES	0	0	0	0	0
TOWNHOUSE	280	.17	.18	104	50
RESERVED	0	0	0	0	0
TOTAL				104	50
BLOCK 877 LOT 16:					
SINGLE FAM RES	0	0	0	0	0
TOWNHOUSE	150	.37	.18	147	81
COMMERCIAL	140	2.9	3.1	406	434
RESERVED	0	0	0	0	0
TOTAL				573	515
BLOCK 800A LOT 3:					
SINGLE FAM RES	0	0	0	0	0
TOWNHOUSE	0	0	0	0	0
APARTMENTS	0	0	0	0	0
COMMERCIAL	150	2.9	3.1	435	465
RESERVED	0	0	0	0	0
TOTAL				435	445
BLOCK 100 LOT U:					
SINGLE FAM RES	0	0	0	0	0
TOWNHOUSE	95	.37	.18	35	17
COMMERCIAL	20	5.77	5.81	115	116
RESERVED	0	0	0	0	0
TOTAL				151	133
BLOCK 201 LOT 31:					
SINGLE FAM RES	0	0	0	0	0
TOWNHOUSE	314	.37	.18	116	57
COMMERCIAL	0	0	0	0	0
INDUSTRIAL	0	0	0	0	0
RESERVED	0	0	0	0	0
TOTAL				116	57
BLOCK 601 L. 12&13:					
SINGLE FAM RES	0	0	0	0	0
TWO FAMILY RES	53	.4	.2	21	11
TOWNHOUSE	0	0	0	0	0
INDUSTRIAL	30	2	10	60	300
RESERVED	0	0	0	0	0
TOTAL				81	311
BLOCK 508 LOT 2:					
SINGLE FAM RES	0	0	0	0	0
MOBILE HOME PRK	732	.29	.18	212	132
RESERVED	0	0	0	0	0
TOTAL				212	132
BLOCK 800 LOT 2:					
APARTMENT-1 FAM	0	0	0	0	0
COMMERCIAL	0	0	0	0	0
MUN. OFFICE-LIBR	30	2.5	2.5	75	75
HUN. D.P.W.	11	.5	1	6	11
PARK/RIDE LOT	60	.5	1	30	60
TOTAL				111	146
STERLING FOREST TR					
SINGLE FAM RES	350	.63	.37	221	130
TOWNHOUSE	220	.37	.18	81	40
APARTMENT	300	.4	.2	120	60
COMMERCIAL	100	2.1	2.2	210	220
OFFICE-LAB	250	.24	1.63	60	408
TOTAL				692	857

TRIP DISTRIBUTION PERCENT OF SITE TRAFFIC TO/FROM CORDON POINTS BY USE

COMPONENT	SKYLINE	CONKL'TN	GRN.LK.T	H.BROOK	GRN.LK.T	SLOAT'BG	FLD.SHOP	NEW SHOP	MUN.SITF	RING SHP	STRL FOR	TOTAL
	SOUTH-E	SOUTH	SOUTH	WEST	N-WEST	NORTH	EXIS N-E	S-E S 2	WEST	WEST NORTH	CM	
BLOCK 752 LOT 1:												
SITE 1 PERCENT:												
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0
TOWNHOUSE	49	9	7	1	2	14	4	4	3	4	3	100
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLs:												
PM-IN	51	9	7	1	2	15	4	4	3	4	3	104
PM-OUT	25	5	4	1	1	7	2	2	2	2	2	50
BLOCK 877 LOT 16:												
SITE 2 PERCENT:												
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0
TOWNHOUSE	49	9	7	1	2	14	4	4	3	4	3	100
COMMERCIAL	17	12	12	10	12	17	0	0	0	0	3	83
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLs:												
PM-IN	151	64	60	42	52	92	7	7	5	7	17	503
PM-OUT	113	59	58	44	54	83	3	3	2	3	15	441
BLOCK 800A LOT 3:												
SITE 2 PERCENT:												
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0
TOWNHOUSE	0	0	0	0	0	0	0	0	0	0	0	0
APARTMENTS	0	0	0	0	0	0	0	0	0	0	0	0
COMMERCIAL	17	12	12	10	12	17	0	0	0	0	3	83
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLs:												
PM-IN	74	52	52	44	52	74	0	0	0	0	13	361
PM-OUT	79	56	56	47	56	79	0	0	0	0	14	386
BLOCK 100 LOT 16:												
SITE 4 PERCENT:												
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0
TOWNHOUSE	20	27	18	1	2	14	4	4	3	4	3	100
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLs:												
PM-IN	30	23	20	6	18	22	1	1	1	1	1	126
PM-OUT	27	19	17	6	18	20	1	1	1	1	1	109
BLOCK 201 LOT 31:												
SITE 5 PERCENT:												
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0
TOWNHOUSE	20	27	18	1	2	14	4	4	3	4	3	100
COMMERCIAL	0	0	0	0	0	0	0	0	0	0	0	0
INDUSTRIAL	0	0	0	0	0	0	0	0	0	0	0	0
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLs:												
PM-IN	23	31	21	1	2	16	5	5	3	5	3	116
PM-OUT	11	15	10	1	1	8	2	2	2	2	2	57
BLOCK 601 L. 12&13:												
SITE 6 PERCENT:												
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0
TWO FAMILY RES	49	10	6	1	2	14	4	4	3	4	3	100
TOWNHOUSE	0	0	0	0	0	0	0	0	0	0	0	0
INDUSTRIAL	25	20	20	5	10	20	0	0	0	0	0	0
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLs:												
PM-IN	25	14	13	3	6	15	1	1	1	1	1	81
PM-OUT	80	61	61	15	30	61	0	0	0	0	0	311
BLOCK 508 LOT 2:												
SITE 7 PERCENT:												
SINGLE FAM RES	0	0	0	0	0	0	0	0	0	0	0	0
MOBILE HOME PRK	49	10	6	1	2	14	4	4	3	4	3	100
INDUSTRIAL	0	0	0	0	0	0	0	0	0	0	0	0
RESERVED	0	0	0	0	0	0	0	0	0	0	0	0
TRAFFIC VOLs:												
PM-IN	104	71	13	2	4	30	8	8	6	8	6	212
PM-OUT	63	13	8	1	3	18	3	5	4	5	4	132
BLOCK 800 LOT 2:												
SITE 9 PERCENT:												
APARTMENT-1 FAM	0	0	0	0	0	0	0	0	0	0	0	0
COMMERCIAL	0	0	0	0	0	0	0	0	0	0	0	0
MUN. OFFICE-LIBR	25	20	20	10	10	10	0	0	0	0	3	98
HUN. D.P.W.	25	70	20	10	10	10	0	0	0	0	3	98
PARK/RIDE LOT	20	15	15	10	10	10	0	0	0	0	3	83
TRAFFIC VOLs:												
PM-IN	26	21	21	11	11	11	0	0	0	0	3	104
PM-OUT	34	26	26	15	15	15	0	0	0	0	4	134
STERLING FOREST TR												
PERCENT:												
SINGLE FAM RES	42	8	5	1	2	11	4	4	3	4	3	87
TOWNHOUSE	42	8	5	1	2	11	4	4	3	4	3	87
APARTMENT	42	8	5	1	2	11	4	4	3	4	3	87
COMMERCIAL	15	10	15	5	15	15	5	5	0	5	5	95
OFFICE-LAB	15	10	15	5	15	15	5	5	0	5	5	95
TRAFFIC VOLs:												
PM-IN	218	61	62	18	49	87	30	30	13	30	26	624
PM-OUT	190	111	106	34	99	119	41	41	7	41	39	707

1997 EXISTING BACKGROUND TRAFFIC EXPANDED AT 37. PER YEAR TO 1993 BACKGROUND TRAFFIC
S.I.A.GROUND TRAFFIC PLUS TRAFFIC GENERATED BY SITE DEVELOPMENT PROPOSED BY OTHERS

EXISTING
SITE 1 SITE 2 SITE 3 SITE 4 SITE 5 SITE 6 SITE 7 SITE 8 SITE 9

FUTURE
GRND CNT BLOCK 75 BLOCK 80 BLOCK 10 BLOCK 20 BLOCK 60 BLOCK 50 BLOCK 80 STERLING TOT VOL
PM DATA SITE 1 SITE 2 SITE 3 SITE 4 SITE 5 SITE 6 SITE 7 SITE 8 SITE 9

Table with columns: LINE-COUNTRY, NB-THRU, SB-LEFT, WB-LEFT, SB-THRU, EB-LEFT, EB-THRU, WB-THRU, SB-RGHT, EB-RGHT, WB-RGHT, and TOT VOL. Rows include sections 1 through 26, listing various traffic lines and their associated vehicle counts.

* NEW TRAFFIC ONLY